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USER'S GUIDE FOR A SYSTEM OF COMPUTER PROGRAMS TO PREDICT FLOWS--ETC(U)  
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**User's Guide For A System Of  
Computer Programs To Predict Flows  
Over And In The Near Wake Behind  
Axisymmetric, Self-Propelled Bodies**

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by

**M. C. Hyman, S. C. Houlihan, J. A. Hill,  
D. L. Dwoyer and C. H. Lewis**

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November 1978

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USER'S GUIDE FOR A SYSTEM OF COMPUTER PROGRAMS  
TO PREDICT FLOWS OVER AND IN THE NEAR WAKE BEHIND  
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## ABSTRACT

↓  
A system of computer programs has been developed to predict flows around and in the near wake behind an axisymmetric body including a propeller at the tail of the vehicle. The system is capable of calculating laminar and/or turbulent, attached and separated flows. Interactive boundary-layer theory is used to predict the flow on the nonseparating region over the body and the full Navier-Stokes equations are solved for the separated, propeller and near wake flow regions.

Details of the theory and results are included in a separate engineering report. The programs, subroutines, variables in common and input and output data are described. Listings of the program code, input and output data for a sample case are included.

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# FORWARD

The following system of computer programs has been developed for use on the IBM 370, model 158 computer, for CMS under VM. For this reason the exec procedures required to execute this system have also been included to aid in the conversion of the system in its present form to a form compatible with that in use at a receiving facility.

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## INTRODUCTION

The purpose of this system of programs is the prediction of viscous flow over and in the near wake behind axisymmetric bodies, particularly submarine-like bodies. The effects of an operating propeller and separated flow have been included in the procedure. The system procedure is basically the execution of four segments. The first is the development of a transformed or nonseparating body which allows a boundary-layer solution to be calculated. The second segment is the solution of the interactive boundary-layer over the body. The third segment is the development of the perturbed flowfield, used in the fourth and final segment, the solution of the afterbody and near wake with the propeller.

## DESCRIPTION OF SYSTEM

The system is composed of a number of programs which serve not only to obtain a solution, but to as great a degree as possible automate the calculation of the solution. The first segment of the system is composed of support programs included specifically to perform this task. The general body coordinates are input and these programs calculate a transformed set of coordinates that allow a nonseparating boundary-layer solution to be obtained. The basis of the transformation is in the nature of the flow over the afterbody. The original coordinates are tested to determine if the flow separates over the afterbody. The test is based on the inviscid pressure distribution over the body and was empirically developed from repeated trials on a number of test configurations. From these trials it was determined that the boundary layer on the afterbody would not remain attached if the inviscid pressure coefficient exceeded a value of 0.2. Therefore, an inviscid calculation is performed to give the pressures over the afterbody and, if the criterion for separation is met, the body is modified until a nonseparating configuration is found.

The next segment of the system is an interactive boundary-layer solution about the transformed body. The interactive solution employs the VPI&SU Incompressible Boundary-Layer Program and the Hess Potential Flow Program to obtain a viscous/inviscid iterated solution. The iteration procedure is as follows: A boundary-layer solution is first obtained by matching the boundary-layer edge pressure with a "first guess" inviscid pressure distribution. Coordinates of the displacement body

that result from the boundary-layer solution are placed in a separate coordinate data set. The inviscid pressure distribution is then found about the displaced body by the potential flow program and becomes the next guess for the pressure distribution. This guess is then used by the boundary-layer program to yield another, corresponding displaced body and the sequence is continued. The iterative process that is developed is continued for several iterations, the number of which is dependent on the shape of the afterbody and the accuracy of the initial guess. With the current system, the first guess is the inviscid pressure distribution about the original body obtained from the potential flow code. It has been found that the use of this initial guess requires that only one iteration was needed when solving for the flows about bodies with straight tails and from 4-6 iterations were needed for straight-tapered or curved tails.

The elliptic nature of the Navier-Stokes equations requires that full (surrounding), boundary conditions be supplied, as well as a first guess of the flowfield in the region treated. The downstream boundary lies in the wake of the body and the corresponding boundary conditions are that  $\partial^2 \xi / \partial x^2$  and  $\partial^2 \psi / \partial x^2$  go to zero. Since the region that is treated in the Navier-Stokes program, in this case a "box" of grid points, encompasses a much greater area than that of the viscous region alone, the full viscous-inviscid velocity profile is required at the upstream edge. The interactive boundary-layer solution provides conditions for the viscous region of the upstream boundary, and conditions in the inviscid region are obtained by employing the potential flow program to calculate the outer flowfield about the final displaced body. At the



joining of the two velocity profiles, the viscous and inviscid regions, a composite expansion is used to ensure a continuous transition. The initial flowfield is thus an inviscid velocity field and is used inside the Navier-Stokes program to generate the initial stream function throughout the Navier-Stokes region. The upper boundary conditions are simply the inviscid velocities obtained from the perturbed flowfield.

The final segment of the system is the solution of the propeller, separated and near wake regions of the flow which is accomplished through the use of the APLNS program. The Navier-Stokes program iterates on the stream function, which, on the first iteration, is the stream function about the inviscid, perturbed body described above. An Alternating Difference Implicit method (ADI) is used for calculating new stream functions in the Navier-Stokes (N-S) region. After NTS time steps, the solution is assumed to reach convergence and the results are printed. For many high speed problems the time step ( $\Delta t$ ) must be particularly small, and hence the number of time steps required for convergence may be considerable.

There is no final convergence criterion other than the specified total number of time steps (NTS).

The logical flow of the system may be followed in Fig. 1. Figure 2 shows the corresponding sequence of program usage in the system. This user's guide contains a brief overview of the system augmented by a more complete and detailed description of the system and its component programs. The system is tied together by WAKE EXEC, an exec procedure which executes the segment procedures. See Appendix A, Table 1.1 for a listing of WAKE EXEC.

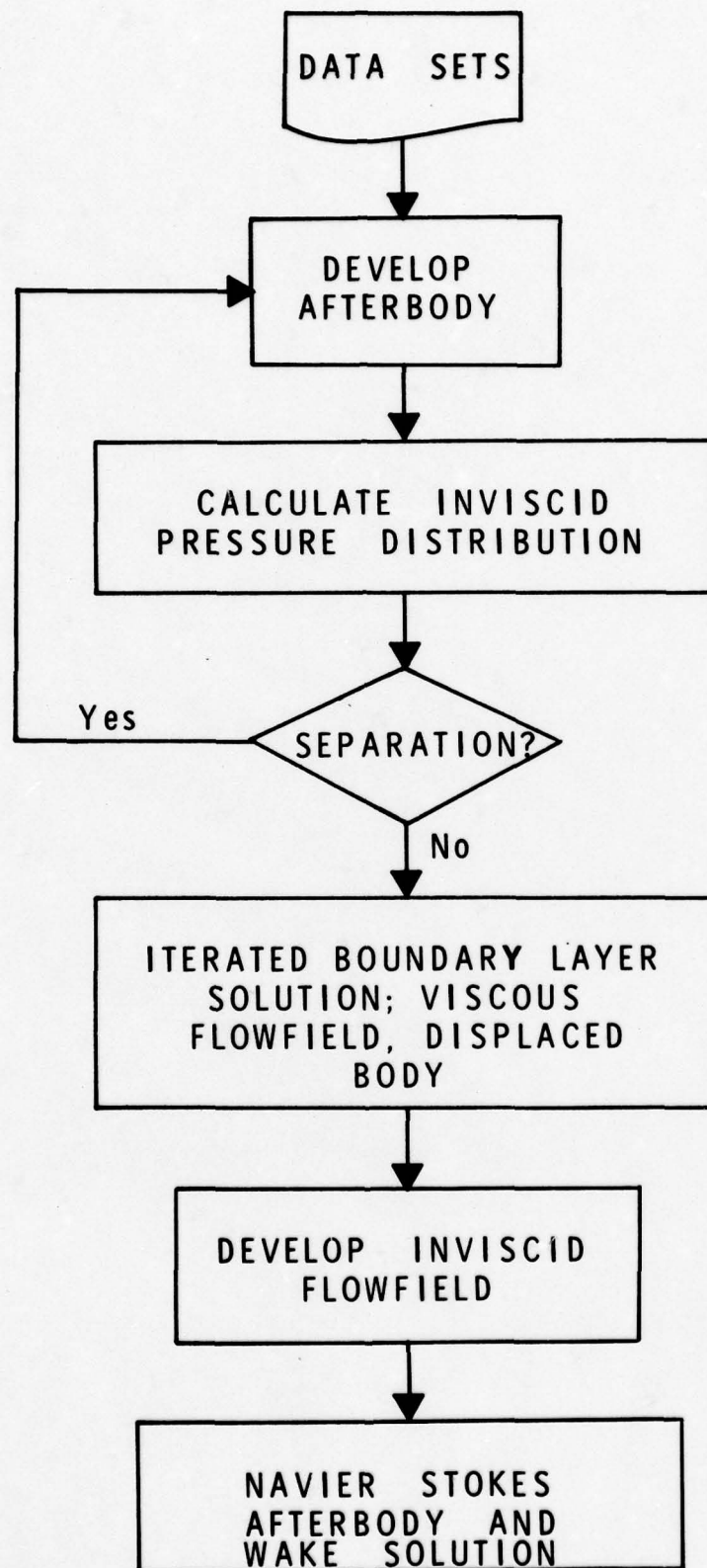


Figure 1. LOGICAL FLOW OF SYSTEM



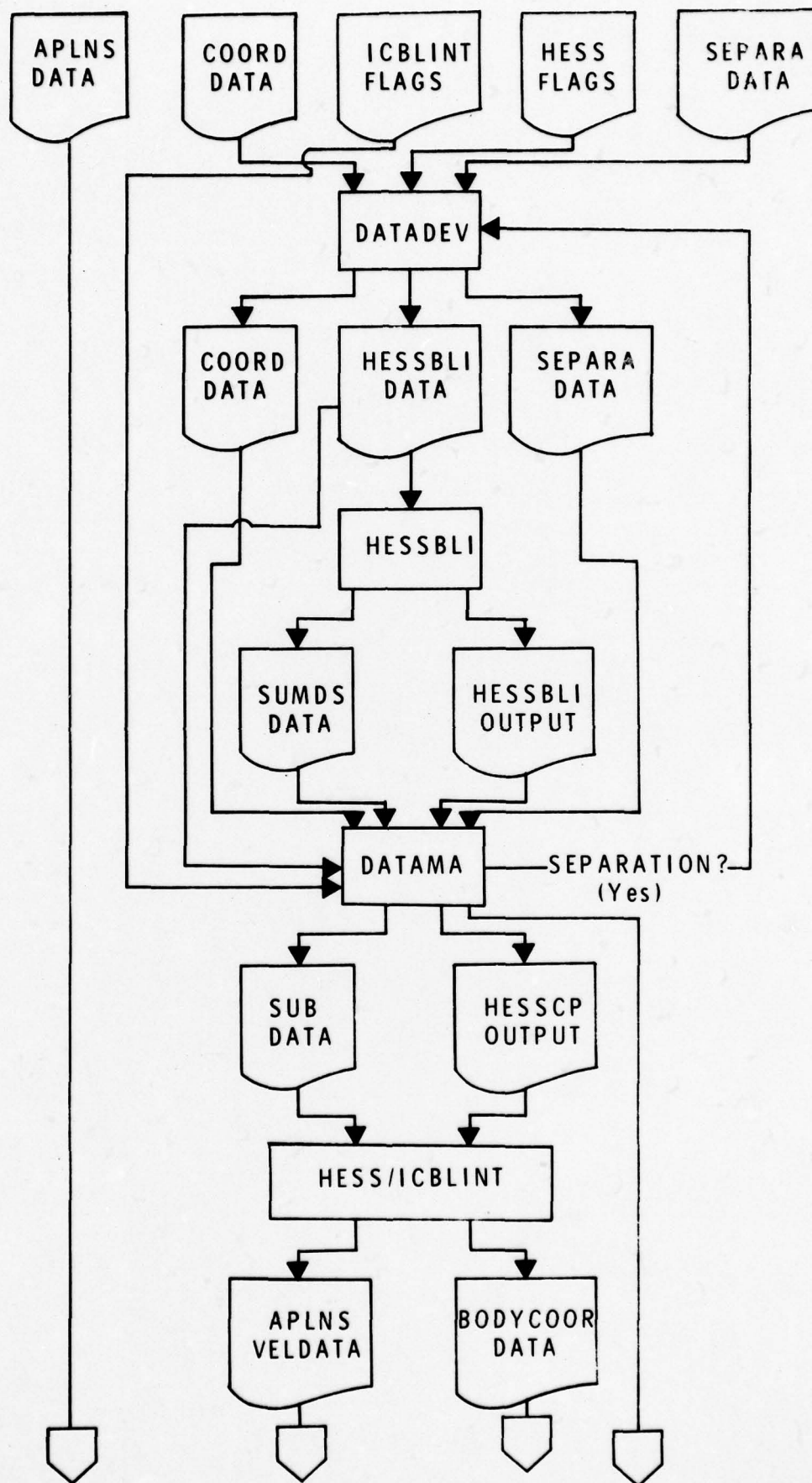


Figure 2. MECHANICAL FLOW OF SYSTEM

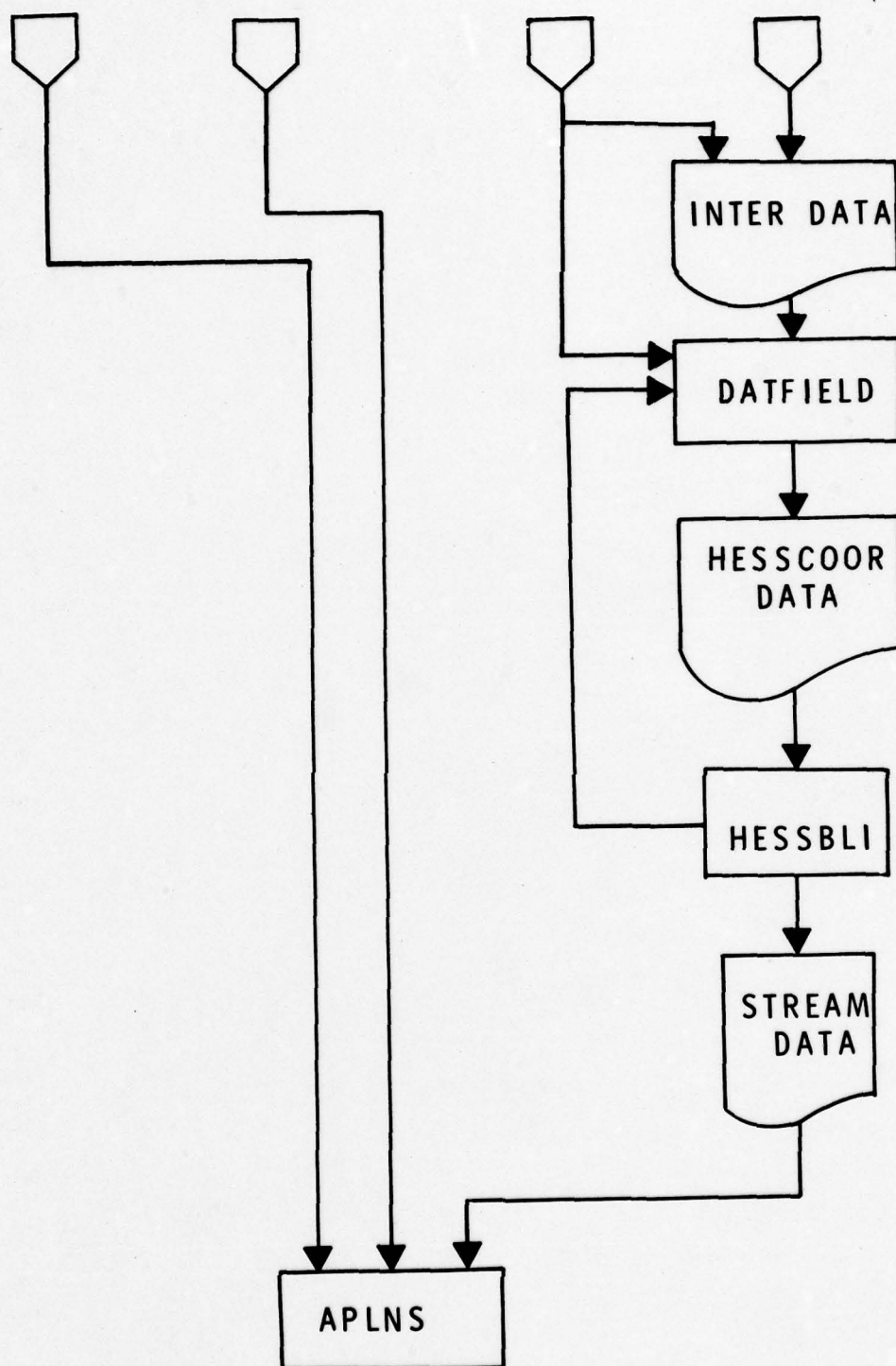


Figure 2. MECHANICAL FLOW OF SYSTEM (continued)

## DESCRIPTION OF PROCEDURE CDCP

CDCP EXEC is an exec procedure which ties together the operation of the support programs: DATADEV, DATAMA, and HESS.

Programs DATADEV and DATAMA, controlled by CDCP EXEC, generate a complete set of data files with which the iterative procedure can be executed. The procedure includes the development and the checking of body geometries until a nonseparating flow is found. The development of the nonseparating flow involves: (1) the incremental extension of a trailing edge fairing into the wake (performed in DATADEV), (2) the testing of that fairing in HESS, and (3) the check of that fairing in DATAMA. CDCP EXEC first executes DATADEV, then HESSBLI and then DATAMA execs. When DATAMA has completed executing, the data file SEPARA DATA is checked and the flag ICP is evaluated. IF ICP is 0, a successful afterbody has been found; if 1, the iterative procedure is continued. If a nonseparating fairing has been found, data sets are written and control shifts to BLINT EXEC, but if not, the fairing is extended further into the wake, and the result is retested. This sequence is continued until a successful afterbody is generated or an iteration limit is reached. Because of imperfections in the fitting of the faired afterbody to the original body, as stated above, it is suggested that the user carefully examine the coordinate sets and  $C_p$  distribution that are output by CDCP and smooth where needed, especially in the trailing edge region and near the body/fairing joint.

### Use of CDCP EXEC (ARGUMENT)

(ARGUMENT) is the maximum number of iterations that the sequence



will complete to find a satisfactory fairing. This is put in as a safety feature to prevent execution from continuing indefinitely due to some unforeseen body characteristic. A listing of CDCP EXEC can be found in Appendix A, Table 2.1.

#### Program DATADEV

Description of Program DATADEV. DATADEV EXEC is the EXEC program which executes DATADEV FORTRAN. DATADEV FORTRAN generates data sets for the HESS potential flow code. On the first pass DATADEV simply writes out a full HESS data set using the original body coordinates. On successive passes, DATADEV generates the afterbody which extends into the wake and further up the body. The extension up the body has been found to hasten afterbody development. The fairing is concave upward, beginning at the point where  $C_p$  changes sign from negative to positive (see Fig. 3 ). After developing the afterbody, new HESS data sets are written out, and a new data set with iteration information is written. A flow chart of DATADEV is found in Fig. 4 .

See Appendix A, Tables 2.2 and 2.3 for listings of DATADEV EXEC and DATAMA FORTRAN.

#### Description of Variables in Common.

BLOCK	VARIABLE	DESCRIPTION OF USE
CORFIT	C	Slope of body at the beginning of the Navier-Stokes region.
CORFIT	DX	Constant stepsize used in re-positioning afterbody coordinates.

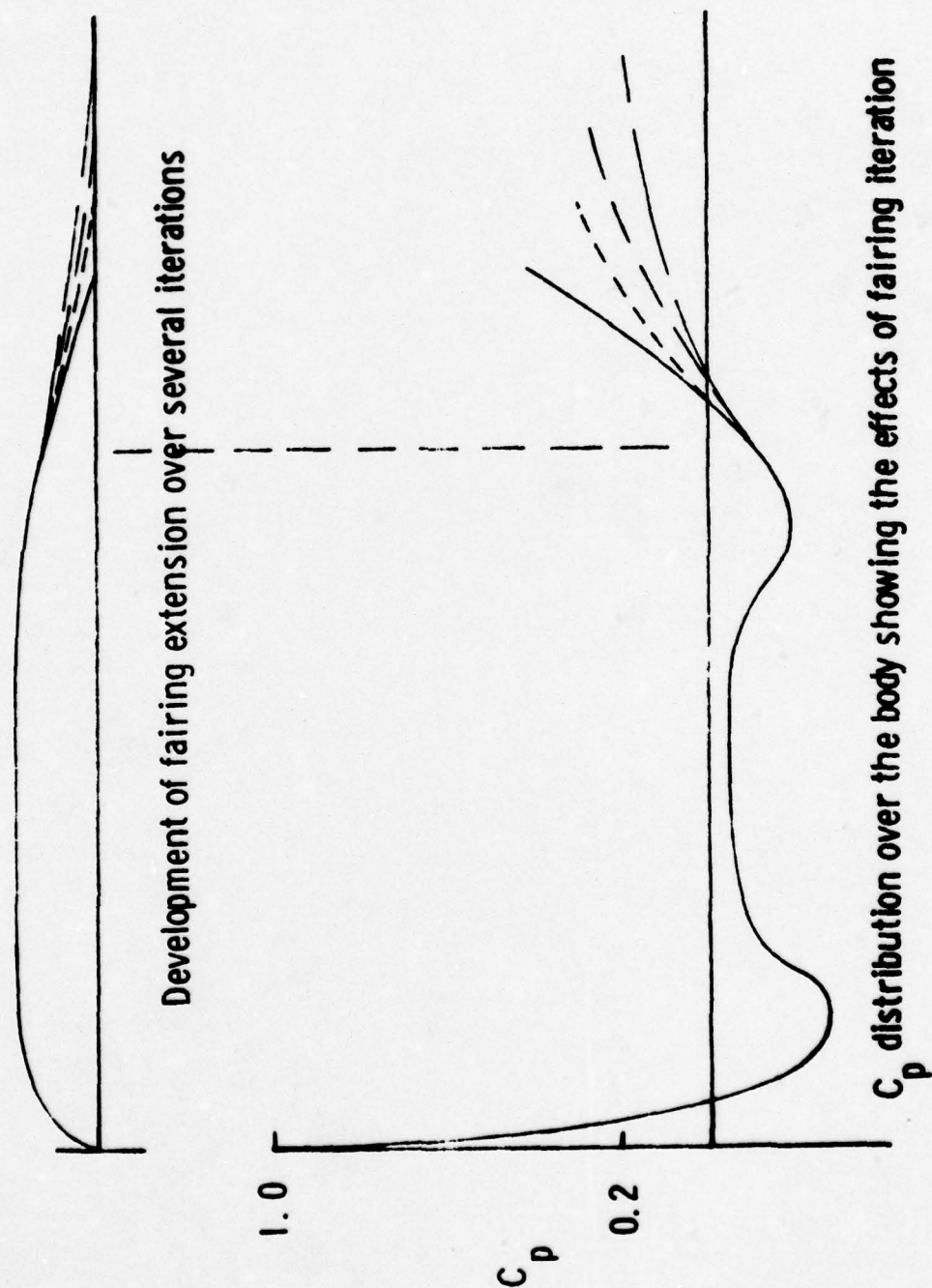


Fig. 3 Development and effect of wake fairing extension

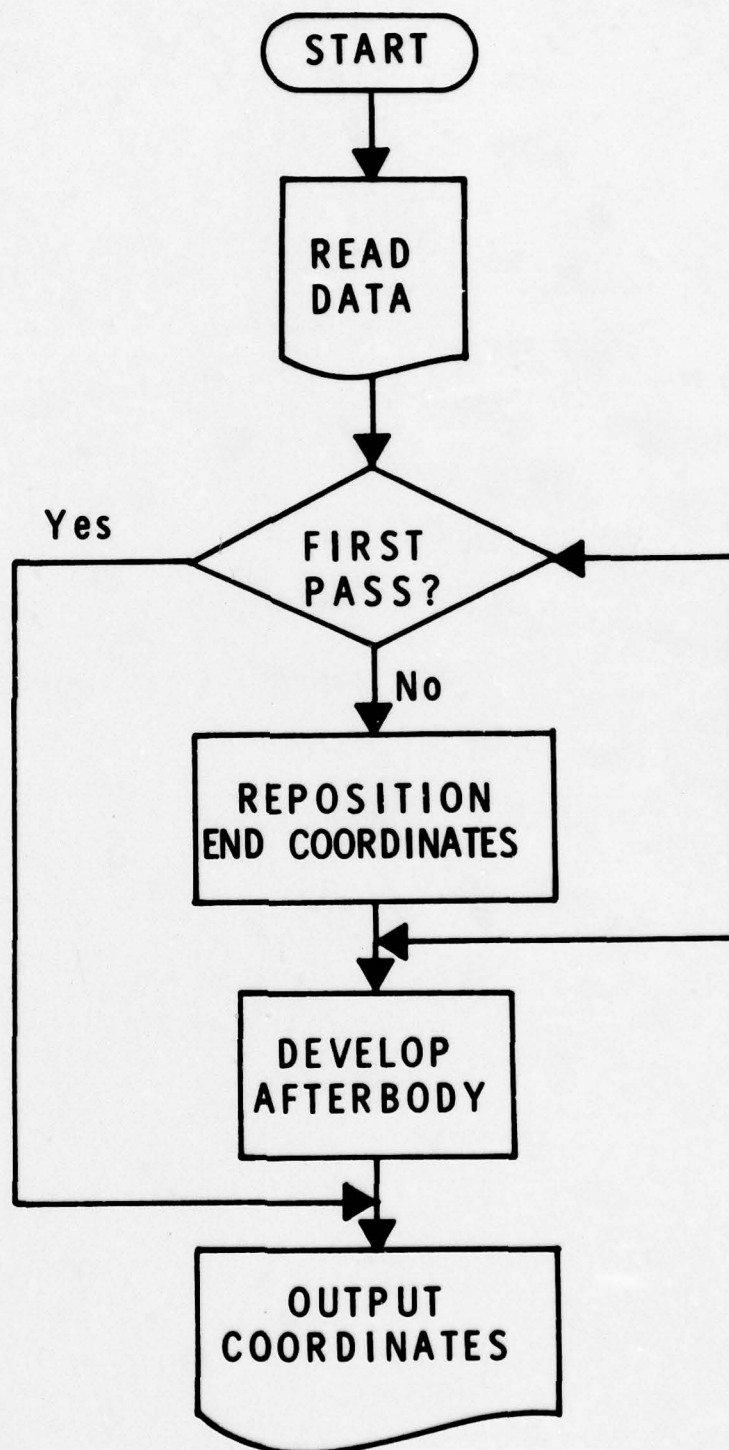


Figure 4. LOGICAL FLOW OF DATADEV



COORD	KTE	Station number of trailing edge on original body.
COORD	KTE1	Station number of trailing edge of faired (extended) body.
CORFIT	NNN	Station number of beginning of re-positioned coordinates.
COORD	NOPRFS	Number of profiles in the part of the Navier-Stokes region on the body.
COORD	X	Original x coordinates on first pass, re-positioned coordinates on subsequent passes.
COORD	Y	Original y coordinates on first pass, re-positioned coordinates on subsequent passes.
CORFIT	X1	Axial distance from the beginning of the fairing to KTE1.
CORFIT	Y1	Radial distance from the beginning of the fairing to the axis.
COORD	XI	Array of x coordinates with afterbody fairing.
COORD	YI	Array of y coordinates with afterbody fairing.

#### Description of Subroutines.

MAIN. MAIN reads in the body coordinates. On the first pass, the original coordinates are read. On successive passes the original

coordinates with the coordinates of the afterbody repositioned to give a constant  $x$  stepsize are read. MAIN then calls LINDEV and HESSPA to generate and write out new coordinates with afterbody.

The variables listed below are used in MAIN. A description can be found in VARIABLES IN COMMON: KWAKE, KTE, KTE1, X, Y.

Subroutine LINDEV. LINDEV develops the trial afterbody fairings and reads in the separation information, including the iteration number. The routine then repositions the coordinates near the trailing edge to give a constant stepsize and on subsequent iterations, extends the fairing into the wake LWAKE points and steps back the beginning of the fairing IWAKE points. This set of  $x$ -coordinates is used in developing the fairing which is done in FIT.

#### Description of Variables.

**DX**             $X$  stepsize in afterbody for repositioned coordinates. Set at one percent of body length.

**KK**            Number of repositioned coordinates.

**LWAKE**        Number of points in wake used in extension of afterbody,  
LWAKE = IWAKE\*5

**MM**            Number of body stations with repositioned coordinates.

Subroutine FIT. Subroutine FIT generates a curve to fit the boundary conditions given by LINDEV in the form of  $X1$ ,  $X2$ ,  $Y1$ , and  $C$ .  $C$  is the body slope at  $X1$ ,  $Y1$ ; the slope at the trailing edge is assumed to be zero. The fit is based on the equations.

$$Y'_N = [\Delta Y(K) + \Delta Y(K^2) + \Delta Y(K^3) + \dots + \Delta Y(K^N)],$$

$$N = 1, KK, KK = \text{No. of points on curve} \quad (1)$$

$$Y_N = Y_1 - Y'_N \quad (2)$$



$$K = \frac{\Delta X}{\Delta Y} C \quad (3)$$

DELY is initially set to 0.0 and successively increased by DY. K is calculated according to Eq. 3. If Y from Eqs. 1 and 2 is less than Y1, DELY is increased and the calculation is redone until the convergence criterion  $(YK - Y1) = 0.0001$  is attained. The Y's based on the last K are used in the afterbody coordinate sets.

#### Description of Variables.

DELX	X stepsize (= dx)
DELY	Y stepsize
K	Constant multiplier in numerical curve fit
L	Station number of the beginning of the afterbody
Y	Working array of Y coordinates of afterbody

Other variables used in FIT and described in Variables in Common are C, Y1, X1, YI, and DX.

Subroutine HESSPA. HESSPA writes out a complete HESS data set using the body coordinate arrays XI and YI which include the afterbody. The routine first reads in the HESS parameters and includes the changed parameters, if any, in the written set.

#### Description of Input and Output.

Input Data. Three data sets are input into DATADEV for execution. They are: COORD DATA, SEPARA DATA, and HESS PARMDATA.

COORD DATA contains the original body coordinates together with parameters and flags.

Card 1      KWAKE      (I3)

	KWAKE	Flag for including wake points in solution: 0 no wake points 1 use wake points (must have data set of wake points if KWAKE = 1)
Card 2	KTE, NOPRFS, KTE1 (1x,3I3) KTE	Station number of trailing edge on original body (first pass original T. E., successive passes repositioned T. E.)
	NOPRFS	Number of profiles on the body in the APLNS box. Maximum of 15 is the recommended value
	KTE1	Station number of trailing edge on faired body
Cards 3-KTE+3	X,Y	(2F12.6)
	X	x coordinate of the original body geometry
	Y	y coordinate of the original body geometry

See Appendix B, Table 1.1 for a sample COORD DATA file.

SEPARA DATA contains information on the status of the iterations and flags on separation.

Card 1	IWAKE	Iteration counter, on first iteration has a value of 0
Card 2	JSTA, KTE JSTA	(1x,3I3) Station number of start of faired body. For initial data set can be 0

	KTE	Described above
Card 3	ICP	(I3)
	ICP	Separation flag, 0 for no separation; 1 for separation. Set to 0 initially.

See Appendix B, Table 1.2 for a sample SEPARA DATA data set.

HESS PARMDATA contains the HESS execution parameters. A further description can be found in the HESS user's guide.

Card 1	HEDR, CASE	(15A4,2x,2A4)
	HEDR	Alphanumeric array with the case title
	CASE	Alphanumeric array with the case number
Card 2	ICARD2	(I3)
	ICARD2	HESS execution flags, for body only solution set at 1,0,1
Card 3	ICARD3	(I5)
	ICARD3	HESS execution flags, set to 0 (see HESS user's guide)
Card 4	ICARD4, NN	(1x,I4,I5)
	ICARD4	HESS execution flags, for body only solution set to 1,0,0,1
	NN	Number of body stations. Set to KTE initially and will be changed to KTE1 for separating case
Card 5	IBDN	(9x,I1)
	IBDN	Body number, for body only solution set to 1

See Appendix B, Table 1.3 for a sample HESS PARMDATA data set.



Output Data. The output files created by DATADEV are:

SEPARA DATA, COORD DATA, and HESSBLI DATA.

SEPARA DATA	Described above. Rewritten for use by DATAMA
COORD DATA	Described above. Values of KTE1 and original coordinates changed to reflect fairing extension (KTE1) and repositioning of original body coordinates
HESSBLI DATA	Complete data set for HESS execution, including fairing when one is used (second and subsequent iterations)
Card 1-5	Described above in HESS PARMDATA
Card 6 - KTE1 XI, YI	(2F12.6)
XI, YI	Body coordinates

See Appendix B, Table 1.4 for a sample HESSBLI DATA data set.

#### Program Datama

Description of Program Datama. DATAMA EXEC executes program DATAMA. DATAMA evaluates the pressure distribution developed by HESS and decides if the geometry will produce separating flow. The program also interpolates the  $C_p$  data set at on-coordinate points for use in the HESS/ICBLINT iterative scheme. If the developed afterbody successfully prevents separation, the full HESS/ICBLINT data sets are written. An option is included to add wake points for a wake solution from HESS/ICBLINT. A flow chart of DATAMA is shown in Fig. 5.

See Appendix A, Tables 2.4 and 2.5 for listings of DATAMA EXEC and DATAMA FORTRAN.

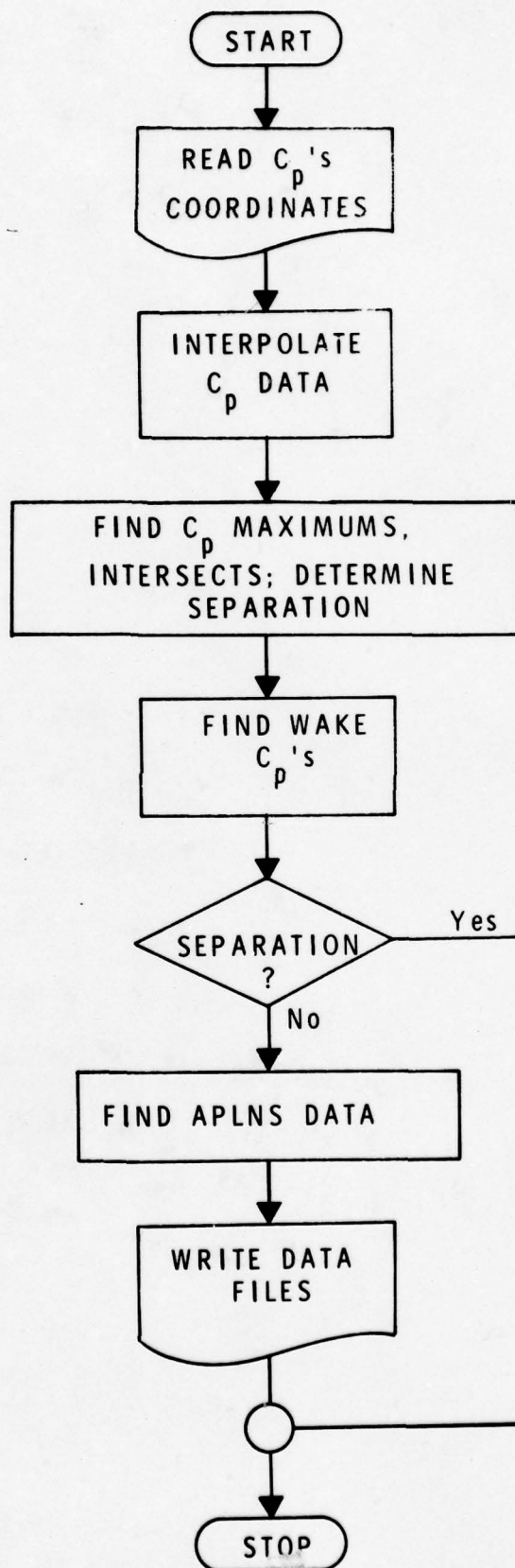


Figure 5. LOGICAL FLOW OF DATAMA

## Description of Variables in Common.

<u>Variable</u>	<u>Description of Variable</u>
DYDX	Slope of straight taper approximation of tail section (without afterbody) for use in APLNS geometry data
JSTA	Station near trailing edge at which the $C_p$ changes sign (- to +), which determines the beginning of the fairing extension.
ICP	Separation flag; 1 if flow is separating, 0 if otherwise
IIMAX	Maximum number of coordinate stations. Values in coordinate array including wake points
JWAKE	Number of wake points at which a solution is to be found
KTE	Station number of original body
KTE1	Station number of trailing edge of body with fairing
KWAKE	Wake flag; 1 if wake points are to be used, 0 if otherwise
X	Array of faired body coordinates
XI	Array of original body coordinates
XLOCAT	X coord of beginning of fairing X(JSTA)
Y	Array of final y body coordinates with fairing
YI	Array of original body coordinates



YWAKE                                      Array of Y values of wake coordinates.

#### Description of Subroutines.

MAIN. MAIN reads in wake coordinates, if used, and calls subroutines CPDATA, CURVE, and READAT. The last two routines are called only if ICP = 0.

Subroutine CPDATA. Subroutine CPDATA is the working section of the program. Pressure coefficients are read in from the previous HESS execution and, since these coefficients are given at off-coordinate points, the data are interpolated to on-body coordinate points. These  $C_p$  data are examined to find locations of sign changes, negative minimums and magnitudes over the fairing. If the fairing  $C_p$  data go higher than 0.2, the body is assumed to produce separating flow. If wake points are to be used, they are added to the coordinate array and given a constant  $C_p$  value of the last negative minimum.

#### Description of Variables.

CP	Array of interpolated $C_p$ values
F	Array of $C_p$ values for off-body points
ICPAR	Station number of negative minimum $C_p$ used in giving initial values to wake $C_p$ data
IWAKE	Iteration counter
LWAKE	Number of points in wake used in fairing extension = IWAKE*5

Subroutine CURVE. CURVE is called when ICP = 0. CURVE reads in the original body coordinates and finds the slope of the body at XI(KSTA). The procedure used defines the straight tapered tail for

the APLNS geometry. CURVE also prints the necessary data for DEVELOP to calculate the inviscid, perturbed flowfield.

Subroutine READAT. Subroutine READAT reads in the HESS/ICBLINT execution parameters and writes out the complete working data sets. For coordinates the routine uses the last (now nonseparating) faired set developed in DATADEV found in HESSBLI DATA. The routine also writes out the stations at which complete solutions in ICBL are to be obtained (IPR array) and the stations at which solutions are to be written out (IPRINT array). For simplicity these arrays are equal, the stations used are dependent on IIMAX.

#### Description of Variables.

K Station number at which IPRINT array begins to be incremented by 1.

#### Description of Input and Output.

Input Data. There are seven data sets used by DATAMA: WAKE COORDATA, ICBLINT PARMDATA, HESSBLI DATA, SEPARA DATA, SUMDS DATA, HESSBLI OUTPUT and COORD DATA. Of these data sets, HESSBLI DATA, SEPARA DATA, and COORD DATA have been described above in INPUT and OUTPUT for DATADEV.

WAKE COORDATA. WAKE COORDATA contains the coordinates of wake points if a wake solution is desired. The input data are as follows:

Card 1	JWAKE	(I3)
	JWAKE	JWAKE is the number of wake points in the arrays XWAKE and YWAKE
Card 2-KWAKE+1	XWAKE	(F12.6) KWAKE is the number of points in wake coordinate data set



**XWAKE** The array of values of coordinates in the array of wake points.

See Appendix B, Table 1.5 for a sample WAKE COORDATA data set.

**ICBLINT PARMDATA.** ICBLINT PARMDATA is the data set of HESS/ICBL execution parameters. The data set contains all the necessary ICBLINT/HESS data except for the axial, radial, and surface coordinates. The data are updated in DATAMA to include any changes made in the coordinates. For a complete description of ICBLINT PARMDATA see the ICBLINT user's guide, "Description of Input," under SUB DATA. SUB DATA contains in Cards 1-20 the set ICBLINT PARMDATA.

**SUMDS DATA.** SUMDS DATA is the data set output by HESS giving the surface distance to each of the coordinates which becomes the XSTA array used in ICBLINT. The data set is read in by READAT and written on SUB DATA.

Card 1-NN XSTA (12x,F12.6)

See Appendix B, Table 1.6 for a sample SUMDS DATA data set.

**HESSBLI OUTPUT.** HESSBLI OUTPUT is the off-coordinate  $C_p$  data from HESS.

Cards 1-NN XW ← XTO ← F(3F12.6)

**XW** XW is the off-coordinate point at which the  $C_p$  data have been calculated in HESS

**XTO** XTO is the on-coordinate point to which the  $C_p$  data will be interpolated

**F** F is the off-coordinate  $C_p$  value

**Output Data.** DATAMA outputs five data files: SUB DATA, HESSCP OUTPUT, SEPARA DATA, DATAMAKE DATA, and INTER DATA.

SUB DATA. SUB DATA is the complete data file for HESS/ICBL execution with all parameters and coordinate points (see INPUT FOR ICBLINT).

HESSCP OUTPUT. HESSCP OUTPUT is the final, interpolated data set of  $C_p$  values for use in HESS/ICBL along with SUB DATA. The data contain the on-coordinate  $C_p$  values. HESSCP OUTPUT is described in the ICBLINT user's guide, "Description of Input."

See Appendix B, Table 1.7 for a sample HESSCP OUTPUT data set.

SEPARA DATA. SEPARA DATA, described earlier, is changed in DATAMA, and output again with the new information.

DATAMAKE DATA. DATAMAKE DATA is the data set for execution of BLDMAKER FORTRAN and is simply the number of points in the final body coordinate set.

Card 1	NN	(I3)
	NN	NN is the number of body points

See Appendix B, Table 1.8 for a sample DATAMAKE DATA data set.

INTER DATA. INTER DATA is the data set for DATFIELD to use in developing the inviscid flowfield.

Card 1	IHESSI	(5I1.I5)
	IHESSI	Counter for the number of repetitions completed through DEVELOP
Card 2	XLOCAT,DX,DY	(3F12.6)
	XLOCAT	Location of the upstream edge of Navier-Stokes region
	DX	x stepsize for placement of off-body points

Δy                      y stepsize for placement of off-body  
points

See Appendix B, Table 1.9 for a sample INTER DATA data set.



## DESCRIPTION OF PROCEDURE BLINT

BLINT EXEC is the controlling exec procedure for the HESS/ICBLINT system of codes. The iterative scheme involves the execution of these programs, together with the support program BLDKER in a loop. The number of loops is user determined, since an accurate criterion for convergence is difficult to define. In using the method, it has been found that generally convergence is obtained after the sixth iteration. For simple geometries, fewer than six iterations are required.

The HESS/ICBLINT iterative sequence is the prime data developer of the APLNS program. In the present form the sequence uses the HESS potential flow program in very nearly its original form, the exceptions being the output of off-body point solutions, pressure distributions, and surface coordinates. Program ICBLINT has been modified to both accept and employ in calculations,  $C_p$  values from the inviscid solution, calculation of wake properties and a restart capability. All of these are used in the viscous/inviscid, iterated solution. The concepts and theory of this iterative procedure have been described, and the following is a description of the code mechanics.

Figures 6 and 7 show the operation of BLINT. The procedure begins with the execution of ICBLINT to yield the initial displaced body BODYCOOR DATA, which is run by HESS. HESS output is the  $C_p$  distribution on the body. The  $C_p$  data set (HESSBLI OUTPUT) is manipulated by BLDKER to yield HESSCP OUTPUT which, together with the original coordinates and the displaced body coordinates, forms the input for the second iteration. In the second and subsequent iterations, the original body and the displaced body coordinates are averaged together (weighting factor of 0.5)

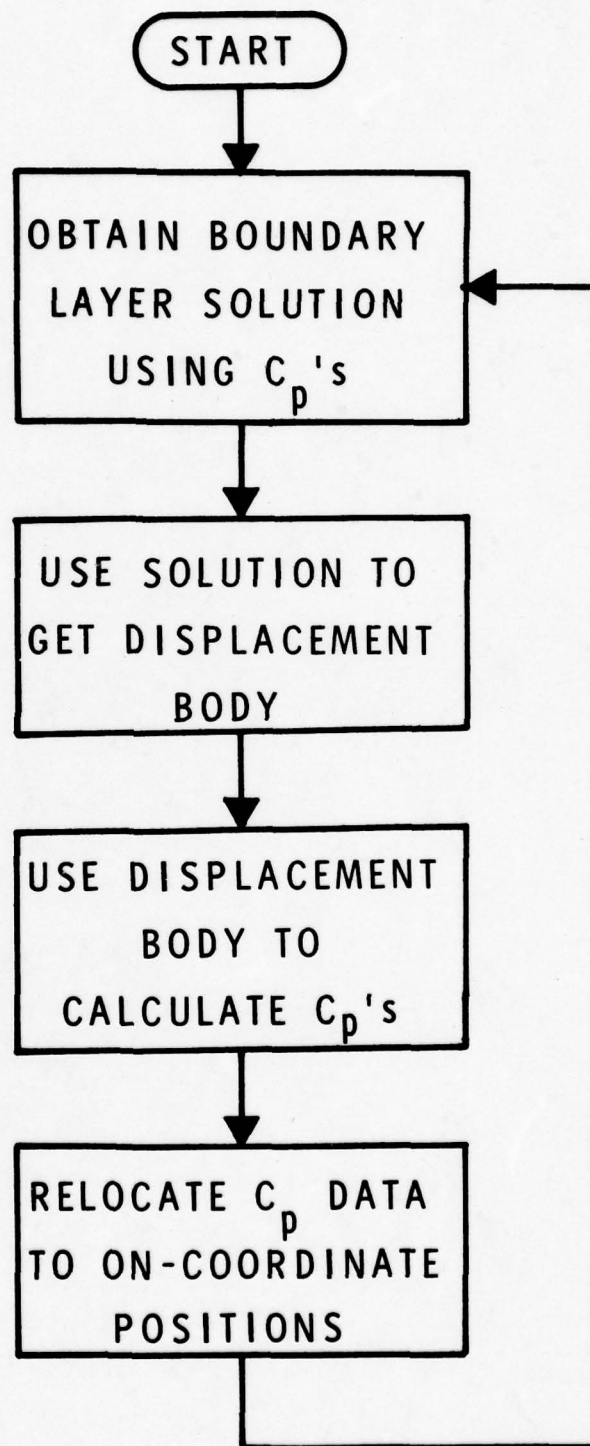


Figure 6. LOGICAL FLOW OF HESS/ICBLINT

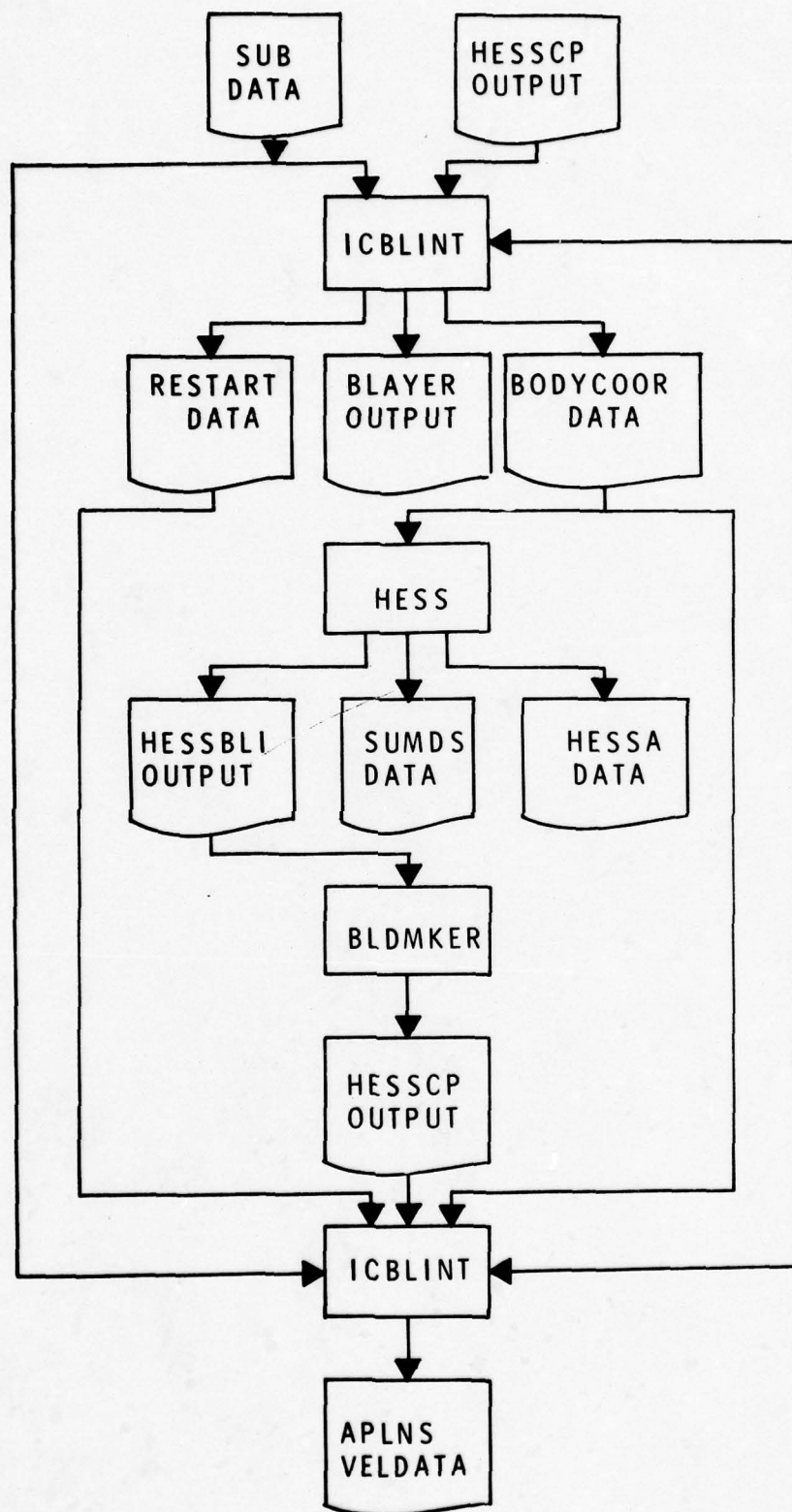


Figure 7. MECHANICAL FLOW OF HESS/ICBLINT



in ICBLINT. Each run yields a displaced body (again BODYCOOR DATA) which is used as HESS input. The procedure then repeats itself for the number of iterations desired.

The procedure for the wake calculations enables the user to obtain iterated wake solutions for nonseparating, no-propeller cases. The extension into the wake may be as far as desired within the array dimensions which will be discussed later. Data set WAKE COORDATA containing the wake points has been described earlier.

The restart capability is a method of saving execution time on the second and subsequent executions of ICBLINT. There is virtually no interaction on the forward region of most bodies and therefore no reason to redo boundary-layer calculations in this region. Therefore, a tape is written at the restart station, and in subsequent iterations the tape is read and the solution begun at the restart station. The actual location of this station is dependent on geometry and must be determined initially by the user.

See Appendix A, Table 3.1 for a listing of BLINT EXEC.

#### Program HESS

The HESS potential flow code is controlled by HESSBLI EXEC. Only three modifications have been made to the original version of the Douglas computer program and are as follows:

1. The pressure coefficients are written out on a separate tape (HESSBLI OUTPUT).
2. The complete inviscid, off-body flowfield is written on a separate tape, and added on during each execution. Details of this modification are found in the description of program

DEVELOP, where the modification is used.

3. The surface distance from the leading edge (SUMDS DATA) is written out on separate tape for use in ICBLINT input data sets.

The complete HESS user's guide is sent under separate cover, describing the code and is accurate except for the above modifications. A listing of HESSBLI EXEC is given in Table 3.2 of Appendix A.

#### Program BLDKER

Description of Program BLDKER. BLDKER is an interpolating program which performs the same function as Program DATAMA in routine CPDATA. BLDKER interpolates the  $C_p$  data output by HESS in HESSBLI OUTPUT and finds the  $C_p$  at on-coordinate positions, creating HESSCP OUTPUT.

See Appendix A, Table 3.3 and Table 3.4 for listings of BLDKER EXEC and BLDKER FORTRAN.

Description of Input for BLDKER. BLDKER requires two input data files: DATAMA DATA and HESSBLI OUTPUT.

DATAMA DATA is the number of points on the body.

Card 1	NN	(I3)
	NN	Number of body points.

HESSBLI OUTPUT has been described in "Input of DATAMA."

Description of Output for BLDKER. This is described in "Input to Program ICPL."

#### Program ICBLINT

Description of the Program ICBLINT. Program ICBLINT has been developed to provide solutions to a large number of incompressible boundary-layer flows. The program can calculate either body only or body

and near wake cases and can treat 2-D or axisymmetric geometries with blunt or sharp noses. Solutions may be obtained using only ICBLINT or ICBLINT in a viscous-inviscid iterative procedure with pressure coefficients of the displaced body as the medium of iteration. The program can predict laminar and/or turbulent flows, the transition models used are described in the contractor report under separate cover.

The flow of logic in the program is controlled by MAIN (see description of MAIN). To assist the user, two flow diagrams of MAIN are included. Figure 8 gives a flow chart of MAIN by the logical functions used, while Fig. 9 gives a flow diagram of MAIN by the subroutines called. As the major subroutines have particular logical functions, there is a close correlation between the two flow charts.

Additional Comments on the use of HESS/ICBLINT. Although the number of body points allowed is a maximum of 501, for the body problems of concern here, fewer than 101 points are preferred. The reasons for this are twofold: first, only a maximum 101 profiles may be solved, the remainder will be used for body definition only; and second, the solutions at only 101 points may be written and hence used in the development of the displaced body in the Potential Flow Code and for the displaced body definition in ICBLINT. For separating flows, the number of body points should be checked and, if necessary, adjusted after CDCP EXEC has been executed.

See Appendix A, Table 3.5 for a listing of BLAYER EXEC and Table 3.6 for a listing of ICBLINT FORTRAN.



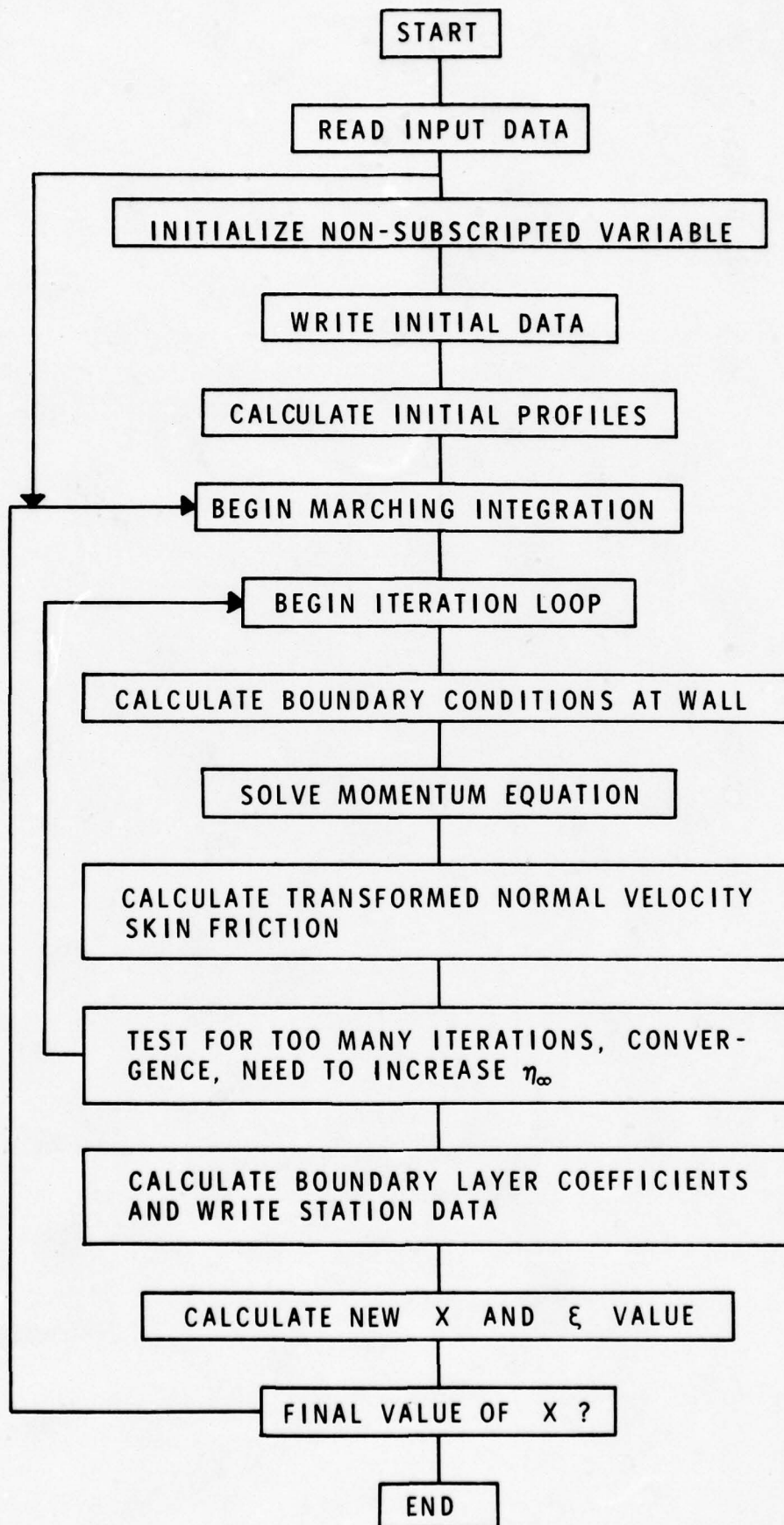


Figure 8. FLOW DIAGRAM OF MAIN ROUTINE BY FUNCTION

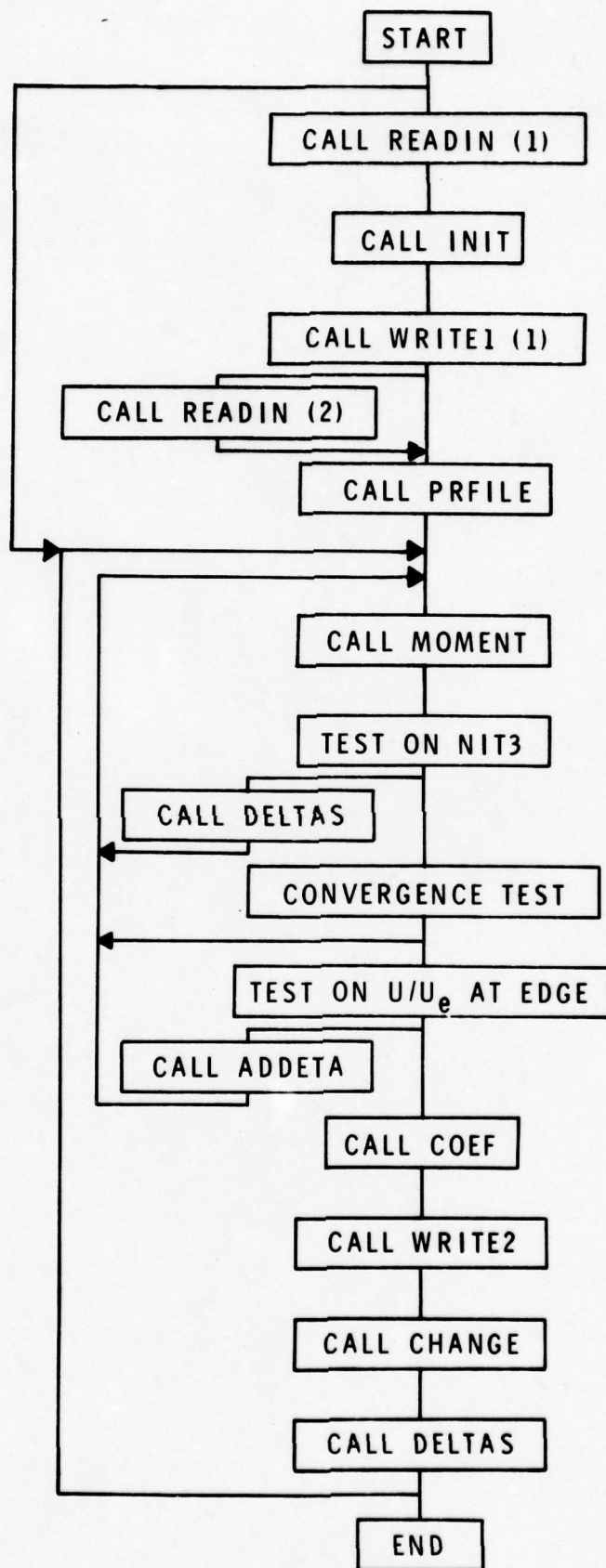


Figure 9. FLOW DIAGRAM OF MAIN ROUTINE BY SUBROUTINES CALLED

Description of Variables in Common. In this section, each variable which is included in a labeled common block is given a brief description. The name of the labeled common block in which the variable occurs is given to the left of the variable name.

<u>Common Block</u>	<u>Variable Name</u>	<u>Description of Variable</u>
NMLCRD	ADTEST	, Criterion for Increasing ETAINF, $(F(IE) - F(IE-4))$ is compared with ADTEST)
GEOME	ANGLE	, Local Body Angle, in Degrees (Converted to Radians)
TRANS	ATR	, Transition Constant (=0.412)
ARRAY1	A0B	= $A_0$
ARRAY1	A0BP	= $\frac{\partial A_0}{\partial \eta}$
ARRAY1	A1	, Partial Differential Equation Coefficient
COMWLL	A1B	, Derivative of $U/U_e$ at Wall
ARRAY1	A2	, Partial Differential Equation Coefficient
ARRAY1	A3	, Partial Differential Equation Coefficient
ARRAY1	A4	, Partial Differential Equation Coefficient
EDGPRP	BETA	= $\beta = 2\xi/U_e(dU_e/d\xi)$
CNVERG	CCRNI	= $1 - CRNI$
CFPR	CF	, Skin Friction in Trans- formed Coordinates (= $C_{f_\infty}/\epsilon_{VD}$ )



COEFF	CFBAR	=	$\bar{C}_f = \frac{1}{x} \int_0^x C_{f_\infty} dt$
COEFF	CFBEX	=	$\bar{C}_f \sqrt{REX}$
COEFF	CFE	=	$C_{f_e} = 2\tau_w/\rho_e U_e^2$
COEFF	CFINF	=	$C_{f_\infty} = 2\tau_w/\rho_\infty U_\infty^2$
COEFF	CFRES	=	CFREY
COEFF	CFREY	=	$C_{f_\infty} \sqrt{REX}$
COEFF3	CF1	,	Term used in Computing CFBEX
ARRAY1	CHI	=	$\chi = \frac{y^2}{\nu} \frac{\partial u}{\partial y}$ , Vorticity Reynolds Number
TRANS	CHICRT	,	Value of CHIMAX at which Transition Regime Cal- culations are Begun
TRANS	CHIMAX	,	Maximum Value in CHI Array
CNVERG	CONVRG	,	Convergence Criterion
CNVERG	CRNI	,	Selector for Finite Difference Scheme; 1.0 for Fully Implicit, 0.5 for Crank-Nicolson, and 0.0 for Fully Explicit
COEFF	DEL	=	$\delta$ , Boundary Layer Thick- ness (Value of y where $U/U_e = 0.995$ )
COEFF2	DELORF	=	$\delta/\text{reference length}$
COEFF2	DELOX	=	$\delta/x$
COEFF	DELST	=	$\delta^*$ , Boundary Layer Displacement Thickness
COEFF	DELTA	=	$\delta/\epsilon_{VD}$

CNVERG	DIF	,	Maximum Difference in G or F (or their Derivative at the Wall) between Iterations (Compared with CONVRG in Convergence Test)
CNVERG	DIFF	,	Local Difference in G or F between Iterations
CNVERG	DIF2	,	Difference in the Derivative of F at the Wall Between Iterations
ARRAY1	DN	,	Array of $\Delta\eta$ Values
ARRAY1	DN2	,	Array of $\Delta\eta$ Values (Used only when ETAINF is Increased)
GEOME	DS	=	$\Delta\xi$ Corresponding to $\Delta x$
COEFF2	DSAXOR	=	$\delta_{axi}^*/\text{reference length}$
COEFF	DSTARK	=	$\delta_k^*$ , Incompressible Boundary Layer Displacement Thickness
COEFF2	DSTODL	=	$\delta^*/\delta$
COEFF2	DSTORF	=	$\delta^*/\text{reference length}$
COEFF2	DSTOTH	=	$\delta^*/\theta$
COEFF2	DSTOX	=	$\delta^*/x$
COEFF	DSTRAX	=	$\delta_{axi}^* = r \{ \sqrt{1+2\delta^*/r} - 1 \}$ (Zero for 2-D Flow)
EDGPRP	DUEDS	=	$dUE/ds$
GEOME	DX	=	$\Delta x$ , Step Size in x Direction
GEOME	DXMAX	,	Maximum Value of $\Delta x$ Permitted in the Calculations
GEOME	DXOLD	,	Previous Value of $\Delta x$
GEOME	DX1	,	Storage Value of $\Delta x$ at the First Station

GEOME	DYDX	,	Body Slope at JSTA
ARRAY1	EPSO	=	$\epsilon_0^+$ , the Outer Eddy Viscosity
ARRAY1	EPSPL	=	$\epsilon_i^+$ , or $\epsilon^+$ , the Inner Eddy Viscosity or the Combined Inner and Outer Eddy Viscosities
VSCSTY	EPSVD	=	$\epsilon_{VD} = \{\mu_{ref}/(\rho_\infty U_\infty L)\}^{1/2}$ , where L is the Unit Length in REINF
NMLCRD	ETAINF	,	Maximum Value of $\eta$
COMWLL	E1	,	Matrix Inversion Coefficient Evaluated at the Wall
ARRAY1	FC	=	$CRNI(F2-F1) + F1$
ARRAY1	FCN	=	$CRNI(F2N-F1N) + F1N$
ARRAY1	FCP	=	$(F2-F1)/DS$
COMWLL	FF	,	Wall Boundary Condition on F
ARRAY1	F1	,	Value of F ( $U/U_e$ ) from Previous Iteration or Station
ARRAY1	F1N	=	$\frac{\partial F1}{\partial \eta}$
ARRAY1	F1NN	=	$\frac{\partial^2 F1}{\partial \eta^2}$
ARRAY1	F2	,	Value of F from Solution of Momentum Equation
ARRAY1	F2N	=	$\frac{\partial F2}{\partial \eta}$
ARRAY1	F2NN	=	$\frac{\partial^2 F2}{\partial \eta^2}$
COMWLL	F2N1	,	Value of F2N at Wall from Previous Iteration



TRANS	GAMMA	,	Transition Intermittency Factor, $\Gamma$ , $\Gamma = 1 - \exp(-A\bar{\xi}^2)$ , where $A = ATR$ and $\bar{\xi} = XIBAR$
COEFF	HAFCF	=	$C_{f_{\infty}}/2$
INTGR	IE	,	Number of Grid Points in $\eta$ Direction
NTEGER	II	,	Subscript for Array IPR
INTGR	IIMAX	,	Maximum Number of Values in Geometry Arrays (i.e. ZA, XSTA, etc.)
INTGR	IM	=	$IE - 1$
NTEGER	IPFL	,	Number of Values in Array IPRFL
ARRAY2	IPR	,	Array of Subscripts for Array XSTA Giving Values of $x$ at which a Solution is to be Obtained
ARRAY2	IPRFL	,	Array of Subscripts for Array XSTA Giving Values of $x$ at which Complete Solutions (with Profiles) are to be Printed
NTEGER	IPRINT	,	Number of Values in Array IPR
INTGR	IPRNT	,	Subscript for Array IPRFL
INTGR	ISTOP	,	Number of Iterations Since Last Converged Solution
NTEGER	JJ	,	Integer Used in Computing DX
APLDAT	JSTA	,	Beginning of N-S Box
NTEGER	K	,	Station Counter
NTEGER	KADETA	,	Indicator, if Zero, ETAINF is Held Constant, if Non-zero, ETAINF can be Increased

NTEGER	KEND	,	Maximum Value Allowed for K
NTEGER	KEP	,	Subscript in EPSPL Array Where the Inner and Outer Eddy Viscosities are Matched
INTGR	KL	,	Index for Profile Output DO Loop, 1 Gives Output for Each Grid Point, 2 for Every Second Grid Point
NTEGER	KSTOP	,	Indicator, Normally Zero, Set to One when Solution is Completed (X = XSTA (IIMAX))
TRANS	KTRANS	,	Indicator for Transition Regime, Zero for No Transition or Instantaneous Transition, One for Transition Regime (Set at Two at "End of Transition")
NTEGER	KTRNSN	,	Subscript in XSTA Array at Which Instantaneous Transition Occurs
INTGR	KVSLAW	,	Indicator for Inner Eddy Viscosity Law, Zero for Reichardt Law, Non-zero for Van Driest Law
NTEGER	LAMTRB	,	Indicator, 1 for Laminar Flow, 2 for Turbulent Flow
CNVERG	NC	,	Specifies Convergence Test, Zero for Test on Derivatives at Wall, One for Test on Functions at all Points in Profile
INTGR	NIT	,	Number of Iterations at Current Value of x
NTEGER	NITTOT	,	Cumulative Total Number of Iterations in x Direction

INTGR	NIT1	,	If, after a converged solution is obtained, NIT is less than or equal to NIT1, $\Delta x$ is doubled
INTGR	NIT2	,	If, after a converged solution is obtained, NIT is greater than or equal to NIT2, $\Delta x$ is halved
INTGR	NIT3	,	If NIT = NIT3 before a converged solution is obtained, $\Delta x$ is halved, X and XI are recomputed and the iteration loop is restarted with the smaller values of X and XI
APLDAT	NOPRFS	,	Number of Profiles in N-S Box
INTGR	NOSE	,	Indicator of Geometry, 1 for a Blunt Nose, 2 for a Sharp Nose
STRT	NRSTRT	,	Increment in K for which the Restart Tape is Written
EDGPRP	PE	=	$P_e/P_{ref}$ , where $P_{ref} = \rho_{ref} U_{ref}^2$
EDGPRP	PESO	=	$P_e/P_{ref}$ , at $s = 0$
FRSTRM	PFS	,	Freestream Static Pressure, PS A
GEOME	PNC	=	$\frac{\sqrt{2E}}{u_e r_w^j}$ , Term in Transformation of Normal Coordinate
EDGPRP	PP	=	$dPE/ds$
REF	PREF	=	$P_{ref} = \rho_{ref} U_{ref}^2$
STAG	PSTAG	,	Freestream Stagnation Pressure, PSFA



ARRAY2	PZ	,	Local Pressure Array, $P/P_{ref}$
STAG	P10	=	$P_0/P_{ref}$
GEOME	REFLEN	,	Reference Length (may be any Value Appropriate to User's Needs)
FRSTRM	REINF	,	Freestream Reynolds Number per Unit Length
COEFF	RETHET	=	$Re_\theta$ , Edge Unit Reynolds Number Times $\theta$
COEFF	REX	,	Local Reynolds Number Based on Edge Conditions
FRSTRM	RHOF5	=	$\rho_\infty$ , slugs/ft <sup>3</sup>
REF	RHOREF	=	$\rho_{ref} = \rho_\infty$ , slugs/ft <sup>3</sup>
COEFF2	ROREFL	=	r/reference length
ARRAY2	RZ	=	r, Array of Radius Values
GEOME	RO	=	r, Local Radius
GEOME	SCF	,	Scale Factor used to Convert Unit Length for REINF (REINF is Computed per Foot if SCF=1; per inch if SCF=12.)
COEFF3	SUM	,	Term used in Computing CFBREX
COEFF	THET	=	$\theta$ , Boundary Layer Momentum Thickness
COEFF2	THODEL	=	$\theta/\delta$
COEFF2	THOREF	=	$\theta$ /Reference Length
EDGPRP	UE	=	$U_e/U_{ref}$
EDGPRP	UER02	=	$(U_e/U_{ref})r^{2j}$
EDGPRP	UES0	=	$U_e/U_{ref}$ at $s = 0$

ARRAY2	UEZ	=	$U_e/U_\infty$ , Array
FRSTRM	UFS	=	$U_\infty$ , ft/sec
REF	UREF	=	$U_{ref} = U_\infty$ , ft/sec
ARRAY1	VC	=	$V = \int_0^\eta (-2\xi \frac{\partial F}{\partial \xi} - F) d\eta$ , Transformed Normal Velocity Component
COMWLL	VW	,	Value of VC at Wall
GEOME	X	,	Local Surface Distance, x
TRANS	XBAR	,	Measure of Relative Length of Transition (i.e. $X_{End\ of\ Transition} \approx$ $XBAR * X_{Beginning\ of\ Transi-}$ tion)
GEOME	XI	=	$\xi$ , Transformed Surface Distance
TRANS	XIBAR	=	$\bar{\xi}$ , Transition Inter- mittency Factor Coordinate $\bar{\xi} = (X - XZERO)/XLAMDA$ , where $XLAMDA = (XBAR - 1) *$ $XZERO/4$ and $XZERO$ is the Value of x at the Start of Transition
GEOME	XIOLD	,	Previous Value of XI
GEOME	XI2	=	$2 * XI$
GEOME	XJAY	=	XJFAC
GEOME	XJFAC	,	Indicator, Zero for 2-D Flow, One for Axially Symmetric Flow
NMLCRD	XKETA	,	Parameter Which Controls the Grid Spacing in the $\eta$ Direc- tion (1.0 Gives an Equally Spaced Grid, a Value Greater than 1.0 Gives a Grid with a Smaller Spacing at the Wall than at the Outer Edge)

VSCSTY	XK1	,	Constant for Van Driest Inner Eddy Viscosity Law
VSCSTY	XK2	,	Constant for Outer Eddy Viscosity Law
ARRAY1	XN	,	Array of $\eta$ Values
ARRAY1	XN2	,	Array of $\eta$ Values (Used only when ETAINF is Increased)
GEOME	XOLD	,	Previous Value of X
COEFF2	XOREFL	=	$x/\text{Reference Length}$
ARRAY2	XSTA	=	$x$ , Array of Surface Distance Values used to Specify Geometry
ARRAY1	Y	=	$y/\epsilon_{VD}$ , Stretched Normal Coordinates
ARRAY1	YOVDL	=	$y/\delta$
ARRAY1	YOVTHT	=	$y/\theta$
ARRAY1	YY	=	$y$ , Normal Coordinate
GEOME	Z	=	$z$ , Local Axial Coordinate
ARRAY2	ZA	=	$z$ , Array of Axial Coordinate Values used to Specify Geometry
GEOME	ZOL	=	$z/\text{Body Length}$
COEFF2	ZOREFL	=	$z/\text{Reference Length}$
COEFF3	SUM1		Incremental Viscous Drag due to Finite Surface Distance
COEFF3	SUMT		Total Drag due to Skin Friction and Pressure
STAG	RHO		Density from Stagnation/Static Pressure
TVCURV	TVC		Flag for TVC Calculations; Yes for TVC, No for 2-D



TVCURV	BODANG	Local Body Angle
TVCURV	RTVC	Local Body Radius
TVCURV	RORW	TVC Body Radius
TVCURV	RORWSQ	RORW
TVCURV	RW	Local Body Radius, ft.
SPTVC	RNOSE	Nose Radius, ft.
WTE	IW	Counter for IWT
WTE	IWT	Increment for Printing Full Profile Data
TE	KTE	Station Number of Trail- ing Edge
TE	KTSTTE	Flag for L.E. Station Calculations
WAK	XKFAC	Flag for Making Wake Calculations; 0 for No Wake, 1 Include Wake
HESS	IWRTH	Displacement Body-Original Body Weighting Factor
HESS	ICARD1	Hess Code Execution Parameter, Printed on Bodycoor Data
HESS	ICARD2	
HESS	ICARD3	
HESS	ICARD4	
HESS	NN	Number of Body Stations
HESS	IBDN	Body Sequence
HESS	HEDR	Array of Alphanumeric Characters Describing the Executing Case
HESS	CASE	Alphanumeric for Record- ing Case Number

HESS	KHESS	Flag: 1 if Inviscid $C_p$ Data are Read in from HESS, 0 if no Inviscid $C_p$ Data are Read in
DRAG	CDV1	Old Value of CDV2
DRAG	CDV2	Pressure Drag for Incremental Length dx
DRAG	XCP	$C_p$ at x from Current Iteration
DRAG	XCP1	$C_p$ at x from Previous Iteration
DRAG	CP	$C_p$ Array from Current Iteration
DRAG	CP1	$C_p$ Array from Previous Iteration
DRAG	ROMAX	Maximum Body Radius
INTACT	BETAS	Minimum BETA
STRTUP	IREAD	Flag for Restart Procedure; 1 use Restart, 0 do not use Restart
STRTUP	ITER	Station Number at Which Restart Tape is Written
STRTUP	ITER	Iteration Number
BDCOOR	ZDELST	Axial Displaced Body Coordinate at Original Axial Coordinate Station
BDCOOR	RODELS	Displaced Body Radius at Station k
BDCOOR	ZOLD	Value of Z from Previous Iteration
BDCOOR	ROLD	Value of R from Previous Iteration
BDCOOR	MM	IRST
APLDAT	XLOCAT	Axial Location of the Upstream N-S Region Boundary

APLDAT	DYDX	Body Slope over the Tail Section, Taken as Constant for the Straight Taper Requirement of the APLNS Code
APLDAT	JSTA	Station Number of the Beginning of the N-S Box
APLDAT	NOPRFS	Number of APLNS Code Stations on the Body

#### Description of Subroutines.

Subroutine MAIN. The principle function of MAIN is to control the flow of logic in the program; however, some calculations are also made in MAIN. In general, the calculations in MAIN are such that they cannot conveniently be performed in the subroutines or they are not sufficiently similar to the calculations made in particular subroutines.

Subroutine READIN is called first. If the input data are from the restart tape, the calculations are made which normally occur at the end of MAIN after subroutine WRITE2 is called, i.e., the calculations that enable the program to set up for the next station are made. The next section of the program is skipped, and the marching integration is resumed. Otherwise, the initial data and profiles are calculated and written by subroutine WRITE1 and the integration is begun with the statement; DO 330 K=KK, KEND. An iteration loop is then entered for the solution of the velocity profile at that station. The boundary conditions at the wall are calculated and the momentum equation is solved. The transformed normal velocity component  $V$  is calculated together with the skin friction in the transformed coordinates (CF). The iteration counters are incremented and NIT and ISTOP are checked. If ISTOP is greater than



100, the program is stopped. If NIT equals (or exceeds) NIT3 the step-size is halved, X and DX are recalculated, and control is returned to the beginning of the iteration loop. Otherwise, the next test is the convergence test. If the convergence criterion is not satisfied, control is returned to the beginning of the iteration loop.

When convergence has been obtained, the velocity profile is checked to see if  $\eta_{\infty}$  needs to be increased. If so, subroutine ADDETA is called and control is returned to the beginning of the iteration loop. If not, subroutines COEF and WRITE2 are called. New values of x and  $\xi$  are obtained and the present values of velocity are assigned to the arrays which contain the values from the previous iteration, and the iteration counters NIT and ISTOP are reset. If a solution has been obtained for the final value of x, (or for K = KEND) the program stops, otherwise, the program returns to the beginning of the marching integration loop to obtain a solution at the new value of x.

#### Description of Variables.

ABST = F2(IE) - F2(IE-4). If ABST is greater than or equal to ADTEST,  $\eta_{\infty}$  is increased

IPRIIM = IPR (II-1)

KREADN ; Indicator for Subroutine READIN, 1 for Input Data, 2 for Initial Data Written on Restart Tape, 3 for Station Data Written on Restart Tape

N , Array subscript

The following variables used in MAIN are described in the section Description of Variables in Common: ADTEST, AIB, CCRNI, CF, CF1, CONVERG CRNI, DIF, DN, DUEDS, DX, EPSVD, FC, FCN, FCP, F1, F1N, F2, F2N, F2NN,

F2N1 IE, II, IIMAX, IPR, IPRNT, ISTOP, K, KADETA, KEND, KSTOP, KSTRT, LAMTRB, NIT, NITTOT, NIT3, NOSE, NT3, PNC, REINF, RHOFS, RO, SCF, UE, UFS, UREF, VC VW, X, XI, XIOLD, XI2, XJFAC, XKFAC, XN, XOLD, XSTA, Y, YY.

Subroutine ADDETA. Subroutine ADDETA is used to increase/decrease ETAINF when the value of F at the outermost grid point and the value of F four points inward differ by more/less than the quantity ADTEST. A new array of values is generated with the maximum value increased by 10 percent. Three point interpolation is used to obtain the values of velocity at the new grid points, whereas at the grid points lying between the new and old values of  $\eta_\infty$ , f is set equal to unity. First and second derivatives of F are then calculated. The storage arrays for F and their derivatives are updated and V is recalculated using the new values. The arrays for y are not updated in this subroutine but are recalculated at the normal points in the solution procedure.

The subroutine provides the output of the intermediate profiles following the message that  $\eta_\infty$  has been increased. DX, XKETA, ETAINF, and ADTEST are also included in the output.

USAGE:

CALL ADDETA

Description of Variables.

DETA1	$\Delta\eta$ at wall
ETAIN2	New value $\eta_\infty$
JC	Array subscript
N	Array subscript

The following variables used in subroutine ADDETA are described in the section Description of Variables in Common: AOBP, CHI, DN, DN2, DX, EPSPL, ETAINF, FC, FCN, FCP, F1, F1N, F1NN, F2, F2N, F2NN, IE, IM, ISTOP KL, VC, XKETA, XN, XN2, YOVDEL, YOVTH, YY.

Subroutine BLUNT1. This subroutine calculates the edge and reference conditions at the stagnation point for a blunt body. The derivative of  $U_e$  with respect to  $s$  is obtained using the five-point differentiation formula with two points reflected about the stagnation point.

USAGE:

CALL BLUNT1

Description of Variables.

DUM	Dummy variable
DUM1	Dummy variable
DUM2	Dummy variable
DUM3	Dummy variable
J	Array subscript
NERR	Dummy variable
PE	Array of PL values
UE	Array of U values

The following variables used in Subroutine BLUNT1 are described in the section Description of Variables in Common: BETA, DUEDES, PE, PESO PFS, PNC, PP, PREF, PSTAG, PZ, POPRIM, P10, REINF, RO, SCF, UE, UER02 UFS, UREF, X, XJFAC, XM, XSTA, Z, ZA.

Subroutine BLUNT2. For a blunt body, the edge properties required by subroutine DELTAS to calculate  $\Delta \xi$  are provided by subroutine BLUNT2. In the immediate vicinity of the stagnation point,  $z$ ,  $r$ ,  $Pe$  and



$du_e/ds$  are calculated using five point interpolation with two points reflected about the stagnation point.

USAGE:

CALL BLUNT2

Description of Variables.

DUM	Dummy variable
DUM1	Dummy variable
DUM3	Dummy variable
J	Array subscript

The following variables used in subroutine BLUNT2 are described in the section Description of Variables in Common: DUEDS, IIAX, PE, PP, PZ, P10, RZ, RO, UE, UEZ, X, XSTA, Z, ZA.

Subroutine CHANGE. Subroutine CHANGE adjusts the x step-size when necessary to obtain a solution at the specified values of x. Subroutine CHANGE is also used when calculations are made with the instantaneous transition model. In this case LAMTRB is reset to two, the stepsize is reduced and a message is printed.

Subroutine CHANGE also increases or decreases the x-stepsize depending on the number of iterations required to converge the previous station.

USAGE:

CALL CHANGE

Description of Variables.

IPRII	= IPR(II)
IPRIIM	= IPR(II-1)

The following variables used in subroutine CHANGE are described

in the section Description of Variables in Common: DX, DXMAX, DXOLD, DX1, EPSVD,, II, IIMAX, IPR, JJ, KSTOP, DTRNSN, LAMTRB, NIT, NIT1, NIT2, X, XOLD, XSTA.

Subroutine COEF. Subroutine COEF calculates the skin-friction coefficients for the boundary-layer flow, the pressure drag, and total drag. It calculates the Reynolds number, displacement thickness, momentum thickness and other dimensionless parameters. At  $X = 0$  the calculations in this subroutine are omitted except for  $Z/L$ .

USAGE:

CALL COEF

Description of Variables.

CF2	Term used in computing CFBREX
DSUM	Term used in computing CFBREX
FAC1	Dummy variables
FAC2	Dummy variables
I	Array subscript
N	Array subscript
RESE	$Re_x^2 \epsilon_{VD}$
SQREX	Square root of REX
STRES	CHREY

The following variables used in subroutine COEF are described in the section Description of Variables in Common: A1B, CF, CFBAR, CFBREX, CFINF, CFRES, CFREY, CF1, DEL, DELORF, DELOX, DELST, DELTA, DN, DSAXOR, DSTODL, DSTORF, DSTOTH, DSTOX, STRAX, DX, EPSVD, FC, HAFCF, IE, IIMAX K, KFS, LAMTRB, REFLN, REINF, RETHET, REX, PNC, RHOF, ROREFL, RO SUM, THET, THODEL, THOREF, UE, UFS, X, XJFAC, XOREFL, Y, YOYDEL, YOYTH, YY,

Z, ZA, ZOL, ZOREFL.

Subroutine DELTAS. Subroutine DELTAS calculates the transformed surface distance  $\xi$  using integration by Simpson's rule. A value of  $\xi$  is obtained for each increment  $\Delta\xi$  from the equation

$$d\xi = U_e r_w^{2j} U_e^{2k} dx$$

The transformation factor PNC,

$$PNC = \frac{\sqrt{2\xi}}{U_e r_w^j}$$

and the pressure gradient term,  $\beta$ ,

$$\beta = \frac{2\xi}{U_e} \frac{dU_e}{d\xi}$$

are also calculated.

USAGE:

CALL DELTAS

Description of Variables.

HA	X - DX/2
RP	RO at X
ROHA	UE at HA
XI	Storage value of X

The following variables used in subroutine DELTAS are described in the section Description of Variables in Common: BETA, DS, DUEDS, DX, PNC, RO, UE, UERO2, X, XI, XIOLD, X12, XJFAC, XKFAC.

Subroutine DERIV3. Subroutine DERIV3 uses subroutine FD3 to generate the first derivative of a function which is given by the



array F. The array of abscissa values is given by X and the derivative of F with respect to X is returned in the array FP.

USAGE:

CALL DERIV3 (F,X,IMAX,IMIN,FP) where F and X are the arrays of ordinate and abscissa values, and where IMAX and IMIN are the upper and lower subscripts for the array FP.

Subroutine EFFMU. Subroutine EFFMU calculates the terms in the coefficients of the differential equations which contain the eddy viscosity. These terms are  $A_0$  and  $\frac{\partial A_0}{\partial n}$  where:

$$A_0 = (1 + \epsilon^+)$$

for the momentum equation. For the laminar case,  $\epsilon^+ = 0$  and the terms reduce to

$$A_0 = 1$$

and

$$A_0' = 0$$

The first portion of the subroutine calculates the terms for the laminar case, and the next portion of the subroutine calculates the vorticity Reynolds number,  $x$ ,

$$x = \frac{y^2}{\nu} \frac{\partial u}{\partial y}$$

For calculations with a transition regime, the routine initiates transition and calculates the transition intermittency factor  $\Gamma$  where

$$\Gamma = 1 - \exp(-0.412 \bar{\xi}^2),$$

$$\bar{\xi} = 4 \frac{x - x_0}{(\bar{x} - 1)x_0}$$

and  $x_0$  is the location of the beginning of transition and  $\bar{x}$  is a measure of the relative length of transition.

In the third portion of the subroutine, the eddy viscosity is computed for turbulent flow calculations and the terms  $A_0$  and  $A_0'$  are then computed.

#### USAGE:

CALL EFFMU (LAMTRB, II, DSTARK)

#### Description of Variables.

ARG	Dummy variable
DELTA	$\delta/\epsilon_{VD}$ , boundary-layer thickness in stretched coordinates
DSTARK	$\delta_k^*$ , incompressible displacement thickness
FAC	Dummy variable
FAC1	Dummy variable
FAC2	Dummy variable
FAC3	Dummy variable
FAC4	Dummy variable
GAMMA	$\gamma$ , outer eddy viscosity intermittency factor
I	The subscript in the EPSPL array where the inner and outer eddy viscosities are matched.
LAMTRB	Indicator for laminar or turbulent flow; 1 for laminar, 2 for turbulent
N	Array subscript
XLAMDA	$\lambda = (\bar{x}-1)x_0/4$
XZERO	$x_0$ , location of start of transition

The following variables used in subroutine EFFMU are described in the section Description of Variables in Common: ATR, AOB, AOBP, CF,

CHI, CHICRT, CHIMAX, DN, DX, DXOLD, EPSO, EPSPL, EPSVD, FC, FCN, GAMMA, PRT, RO, UE, X, XBAR, XIBAR, XI2, XJFAC, XKFAC, XK1, XK2, XN, Y.

Subroutine EDGPROP. Subroutine EDGPROP obtains the edge properties used in subroutine DELTAS to calculate  $\Delta\xi$ . The edge properties are obtained from subroutine BLUNT1.

USAGE:

CALL EDGPROP

Subroutine FD3 and FD5. Subroutines FD3 and FD5 use the first derivative of the Lagrangian interpolating polynomial of second and fourth order, respectively, to provide the first derivative of the function F at point X. The returned value is denoted by FX. The interpolating polynomials are described in the descriptions of subroutines INTER3 and INTER5.

USAGE:

CALL FD3 (X,X1,X2,X3,F1,F2,F3,FX) or

CALL FD5 (X,X1,X2,X3,X4,X5,F1,F2,F3,F4,F5,FX) where X1, X2, etc. are the abscissa values, and where F1, F2, etc. are the ordinate values.

Subroutine GEOM. This subroutine obtains the edge properties at the initial value of x for the geometry specified by the variable NOSE which is passed through common. The edge properties are obtained from subroutine BLUNT1 for a blunt nosed body (NOSE = 1), from subroutine CONE1 for a sharp nose (NOSE = 2).

USAGE:

CALL GEOM

Subroutine INIT. Many variables are given fixed initial values in the program before the marching integration procedure is begun.



The non-subscripted variables are given the initial values in subroutine INIT.

USAGE:

CALL INIT

Description of Variables.

JT            Array subscript

The following variables used in subroutine INIT are described in the section Description of Variables in Common: CCRNI, CF, CHIMAX, CRNI, DS, DX, DXOLD, DX1, E1, FF, GAMMA, IE, IIMAX, IM, IPRNT, ISTOP, JJ, KEP, KFS, KSTOP, KTPW, KTW, LAMTRB, NIT, NITTOT, NOSE, NRSTRT, RHOF, SUM, UFS, VW, X, XI, XIBAR, XIOLD, XI2, XJAY, XJFAC, XKFAC, XM, XOLD, XSTA, Z.

Subroutine INTER3. Subroutine INTER3 uses a second-order Lagrangian interpolating polynomial, interpolating on the points  $x_1$ ,  $x_2$ , and  $x_3$ , with the corresponding function values  $F_1$ ,  $F_2$ ,  $F_3$  to provide a value  $F(x)$ .

The general form of the polynomial is

$$F(x) = \sum_{k=1}^3 f_x L_k(x)$$

where

$$L_k(x) = \prod_{\substack{m=1 \\ m \neq k}}^3 \frac{x - x_m}{x_k - x_m}$$

USAGE:

CALL INTER3 (X, X1,X2,X3,F1,F2,F3,F) where  $X_1$ ,  $X_2$ , and  $X_3$  are the abscissa values and  $F_1$ ,  $F_2$ , and  $F_3$  are the function values.

Subroutine INTER5. Subroutine INTER5 uses a fourth-order Lagrangian interpolating polynomial interpolating on the points  $x_1, x_2, x_3, x_4$ , and  $x_5$  with the corresponding function values  $F_1, F_2, F_3, F_4$ , and  $F_5$  to provide a value  $F(x)$ .

The general form of the polynomial is

$$F(x) = \sum_{k=1}^5 f_x L_k(x)$$

where

$$L_k(x) = \prod_{\substack{m=1 \\ m \neq k}}^5 \frac{x - x_m}{x_k - x_m}$$

USAGE:

CALL INTER5 (X,X1,X2,X3,X4,X5,F1,F2,F3,F4,F5,F) where  $X_1, X_2$ , etc. are the abscissa values and  $F_1, F_2$ , etc. are the function values.

Subroutine INTERP. Subroutine INTERP uses function TLU to linearly interpolate in the array F2 for the value FF corresponding to the value XX in the array XN. If XX is not within the range of XN, a message is printed and FF is set equal to  $F_2(IE)$  where IE is the size of the arrays. XN must be a strictly increasing array.

USAGE:

CALL INTERP (XX,XN,F2,IE,FF)

Subroutine INTERP5. Subroutine INTERP5 uses five-point interpolation to obtain a value F0 in the array F1 corresponding to the value X0 in the array X1. The array X1 can be either monotone increasing or monotone decreasing.

## USAGE:

CALL INTRP5 (X0,X1,F1,IMAX,IMIN,I1,F0) where X1 and F1 are the arrays of coordinate values, IMAX and IMIN are the maximum and minimum values allowed for the subscripts of the arrays 0 and I1 is an indicator ( $I1 \leq 0$ , X1 is monotone decreasing;  $I1 \geq 0$ , X1 is monotone increasing).

Subroutine MOMENT. The solution of the momentum equation is obtained in subroutine MOMENT. The coefficients of the partial differential equation are calculated and new values of  $F = U/U_e$  and the first and second derivatives of F with respect to  $\eta$  are obtained from subroutine SOLVE. The difference between the new and the former values is obtained for either the wall or the all points convergence test. The derivative of F with respect to x is also calculated.

## USAGE:

CALL MOMENT

The following variables in subroutine MOMENT are described in the section Description of Variables in Common: A0, AOB, AOBP, A1, A2, A3, A4, BETA, C, CCRNI, CP, CRNI, DIFF, DS, DSTARK, E1, FC, FCN, FCP, FF, F1, F1N, F1NN, F2, F2NN, F2N1, IE, IM, KEP, LAMTRB, NC, TH, VC, X, XI.

Subroutine PRFILE. Subroutine PRFILE calculates the array of  $\eta$  values, XN, which corresponds to the values of IE, ETAINF, and XKETA. The grid spacing is given by  $\Delta\eta_i = K\Delta\eta_{i-1}$  where K corresponds to XKETA and thus at the ith grid point

$$\eta_i = \Delta\eta_1 \frac{K^i - 1}{K - 1}, \quad i = 0, 1, 2, 3, \dots, N \quad (N = IE - 1)$$

where  $\Delta\eta_1$  is given by

$$\Delta\eta_1 = \eta_\infty \frac{K - 1}{K^N - 1}$$



The initial velocity profile,  $F$ , is calculated from the formula  $F = 1 - \exp(-\eta)$ . The derivatives of  $F$  are also calculated as are initial profiles for  $\epsilon^+$ ,  $y/\delta$ ,  $y/\theta$ . Further, the boundary conditions at the outer edge of the boundary layer are set in this subroutine.

USAGE:

CALL PRFILE

Description of Variables.

DETA1         $\eta$  stepsize at wall

N            Array subscript

The following variables used in subroutine PRFILE are described in the section Description of Variables in Common: DN, EPSPL, ETAINF, FC, FCN, FCP, F1, F1N, F1NN, F2, F2NN, IE, IM, PNC, VW, XKETA, XN, Y, YOVEL, YOVTHT.

Subroutine READIN. Subroutine READIN provides the input of data for the program. Input data are from a single data set (SUB DATA) when calculating a noniterative solution, two sets for the initial iterated solution (SUB DATA and HESSCP OUTPUT), and the two plus a restart tape for the subsequent iterations. READIN also resets the input flags to their default value when they are set to 0 in the input data and performs some pressure calculations for the iterated solution.

USAGE:

CALL READIN

Description of Variables.

J            Array subscript

LST            Alphanumeric variable, assigned value of 'LAST' in a DATA statement

All other variables are described in the section Description of Variables in Common, except for LABEL and LSTC which are described in the section.

#### Description of Input Data.

Subroutine RESTAR. Subroutine RESTAR restarts program execution at a predetermined body coordinate location. On the first iteration, when the marching integration reaches the restart location (IRSTRT), a tape is written containing all the data needed to begin execution on the next global iteration. RESTAR first reads in the data written from the previous global iteration, and then reads in the previous displacement body coordinates. Finally the restart tape is re-written using the data calculated by the current execution and the coordinates of the new displacement body are written out at the end of the current execution.

Subroutine SOLVE. Subroutine SOLVE calculates the solution for a general parabolic partial differential equation when the equation is written in the standard form.

$$\phi_{\eta\eta} + A_1\phi_{\eta} + A_2\phi + A_3 + A_4\phi_{\xi} = 0$$

In order to obtain a solution for the above equation, values of  $\phi$  and the first and second derivatives of  $\phi$  with respect to  $\eta$  from a previous iteration or from a previous  $x$  station are required. These data are passed through the argument list as the arrays W1, W1N, and W1NN. The new values of  $\phi$  and the first and second derivatives are returned through the argument list as the arrays W2, W2N, and W2NN.

#### USAGE:

CALL SOLVE (W1NN, W1N, W2NN, W2N, W2, E1, F11, CRNI)

## Description of Variables.

A	Matrix Inversion Coefficient
B	Matrix Inversion Coefficient
CC	Matrix Inversion Coefficient
D	Matrix Inversion Coefficient
E	Array of Matrix Inversion Coefficients
E1	Value of $\epsilon$ at wall
F	Array of Matrix inversion coefficients
F11	Value of F at wall
KON	Array subscript, descending order
N	Array subscript
W1	Value of $\phi$ at previous station
W1N	$\partial\phi/\partial\eta$ at previous station
W1NN	$\partial^2\phi/\partial\eta^2$ at previous station
W2	New value of $\phi$
W2N	New value of $\partial\phi/\partial\eta$
W2NN	New value of $\partial^2\phi/\partial\eta^2$

The following variables which are used in subroutine SOLVE are described in the section Description of Variables in Common: A1, A2, A3, A4, CRNI, DN, DS, IE, IM, XN.

Function TLU. Function TLU searches in the array X for the two values which bracket XSTAR and linearly interpolates for the corresponding value in the array Z. The returned value is TLU. If XSTAR is not within the range of the array X, TLU is set equal to zero and the error flag is set equal to one. The array X must be strictly increasing.



## USAGE:

TLU (NTABLE, Z, X, XSTAR, NFLAG) where NTABLE is the dimension of the arrays Z and X and NFLAG is the error flag.

Subroutine VELDAT. Subroutine VELDAT has been added for the express purpose of writing out data sets for the Navier-Stokes code. The routine writes the solution of the velocity profile at the upstream boundary of the Navier-Stokes region to be used as boundary conditions for the APLNS code.

## USAGE:

CALL VELDAT

Subroutine WRITE1. Subroutine WRITE1 writes out the input data and the initialized data. Integer quantities are written first in the same order as they appear in the input. The next data written are the freestream quantities. The transition parameters are then written, followed by a group of variables, most of which are from the program input and appear in approximately the same order. Next are written the integer arrays which control the values of x at which a solution is obtained and stations at which full profile data are to be written. Finally, the values of axial distance, radius, surface distance, surface pressure, and nondimensional edge velocity are written.

## USAGE:

CALL WRITE1

Description of Variables.

J            Array subscript

The other variables which appear in this subroutine are described in the sections Description of Output and Description of Variables in Common.

Subroutine WRITE2. Subroutine WRITE2 provides the output of computed results after a converged solution is obtained. The output is in two sections. The first section is written at every station at which a solution is obtained. The second section is written for specified values of  $x$ . The first line of output contains the values of geometry related variables (such as  $x$ ,  $z$ , and  $\xi$ ), the pressure gradient term  $\beta$ , the number of iterations, and the station counter,  $K$ . The second line contains the nondimensionalized edge conditions ( $U_e$ ,  $P_e$ , etc.), the skin friction in transformed coordinates, the matched eddy viscosity, and the cumulative total of the number of iterations. The third line gives the first and second derivatives of the velocity at the wall and at the second grid point from the wall. The remainder of the first section is omitted at  $x=0$ . The next line gives transition parameters and the following line contains the Reynolds number. In the remaining lines in the first section are skin friction coefficients, the boundary-layer thicknesses, and quotients of boundary-layer parameters. In the second section of the output, some of the variables which are functions of the normal coordinate are written. The output of this section contains  $\eta$ ,  $y$ ,  $y/\theta$ ,  $y/\delta$ ,  $F(=U/U_e)$ ,  $\partial F/\partial \eta$ ,  $y^+$ ,  $u^+$ ,  $U_{def}$ , and  $\epsilon^+$ .

USAGE:

CALL WRITE2

Description of Variables.

II	Counter or subscript for array IPR
IPRNT	Counter or subscript for array IPRFL
KL	The values of $\eta$ and the functions of $\eta$ are written

at every KLth grid point

XOLD Previous value of x

The above variables are in common and are also described in the section Description of Variables in Common. The other variables which appear in this subroutine (except for N, an array subscript) are described in the section Description of Output.

Subroutine ZRO. Subroutine ZRO uses subroutine INTER5 to interpolate in the arrays ZA and RZ for the values Z and R0 corresponding to the value X2 in the array XSTA. The arrays RZ, XSTA, and ZA contain values of radius, surface distance, and axial distance respectively for an axisymmetric geometry.

#### USAGE:

CALL ZRO (JJ, X2, Z, R0)

Description of Input Data.

There are two sets of input files to be used in obtaining the iterated solution, i.e., SUB DATA, and HESSCP OUTPUT. SUB DATA contains the basic data for execution, and HESSCP OUTPUT contains the  $C_p$  distribution at the edge of the displaced body. SUB DATA will be described first.

CARD 1	IREAD, IRSRT, ITER, KHESS	(6(8X,I2))
	IREAD	Restart flag, 0 no restart tape to be read (or written), 1 read (and write) restart tape
	IRSRT	Station number for restart tape to be written
	ITER	Iteration counter



	KHESS	Flag for using $C_p$ distribution; 0 do not read in $C_p$ data from HESS, 1 read in $C_p$ data
CARDS 2-6	HEDR, CASE, ICARD2, ICARD3, ICARD4, NN, IBDN (10A6, 2x, A6/I3/I5/1x,I4,I5/9x,I1)	Standard HESS input parameters, described in HESS PARMDATA and HESSCOOR DATA
CARD 7	BETAS, ROMAX (6F12.6) BETAS	Minimum value of BETA, the pressure gradient term. If BETA goes lower than BETAS, BETA is set equal to BETAS.
	ROMAX	Maximum body radius
CARD 8	LABEL (18A4)	Alphanumeric data for identification of the case. Printed on the first page of output.
CARD 9	NOSE, LAMTRB, KVSAW, KTRANS, KTRNSN, KONSET (3(8x,I2), 3(7x,I3))	
	NOSE	Indicator for geometry; 1 for a blunt nose, 2 for a sharp nose body. A value of 0 is reset to 1
	LAMTRB	Indicator; 1 for laminar flow, 2 for turbulent flow. A value of 0 is reset to 1

	KVSLAW	Indicator: 0 for Reichardt Eddy Viscosity, 1 for Van Driest Eddy Viscosity
	KTRANS	Indicator for transition regime; 0 for no transition or in- stantaneous transition, 1 for transition regime (LAMTRB must be 1)
	KTRNSN	Subscript for XSTA array giving value of x at which instantaneous transition occurs
	KONSET	Subscript for XSTA array giving value of x at which transition regime begins
CARD 10	NIT1, NIT2, NIT3, NC	(4(8X,I2))
	NIT1	After solution converges, $\Delta x$ is doubled if NIT is less than or equal to 0. A value of 0 is reset equal to 3. A value less than zero is reset equal to 0. Recommended value is 5
	NIT2	After solution converges, $\Delta x$ is halved if NIT is greater than or equal to NIT2. A value of 0 is reset to 6. A recommended value is 10
	NIT3	If NIT = NIT3, $\Delta x$ is halved, X and XI are recomputed and the iteration loop is restarted with the smaller values of X and XI. A value of 0 is reset to 9. A recommended value is 20
	NC	Specific convergence test; 0 for test on derivatives at wall, 1 for test on functions at all points in profile. Recommended value is 1
CARD 11	IE, KEND, IIMAX	(4(7X,I3))
	IE	Number of grid points in ETA di- rection. (program dimensioned for 101, the recommended value)

	KEND	Upper index on K (the station counter). Recommended value, 300-600
	IIMAX	Number of values in geometry and pressure arrays. Arrays dimensioned for 500 values, recommend no more than 101. If more than 101 points are used, changes will need to be made to the dimensions of arrays IPR and IPRFL
CARD 12	KADETA, KL, IPFL, IPRINT, IWT	(5(8X,12))
	KADETA	Indicator; if zero, ETAINF is held constant, if nonzero, ETAINF can be increased or decreased. A nonzero value is recommended
	KL	Index for profile output DO loop; 1 gives output for each grid point, 2 for every second grid point
	IPFL	Number of values in IPRFL array (maximum 100)
	IWT	Increment in station number at which full profiles are printed
CARD 6	CHICRT, XBAR, ATR	(3F12.6)
	CHICRT	Value of CHIMAX at which transition regime calculations begin (arbitrary if KTRANS = 0). Appropriate values have been found to be between 2000 and 4000
	XBAR	Measure of relative length of transition region (i.e. $X_{\text{end of transition}} = XBAR * X_{\text{beginning of transition}}$ )  For Reichardt Law, XBAR should be about 65 percent greater than value used with Van Driest Law. Recommended values are approximately 3.3 and 2.0, respectively



	ATR	Transition constant = 0.412
CARD 14	UFS, REINF, PFS, PSTAG, SCF, RNOSE	(6F12.6)
	UFS	Freestream velocity, ft/sec
	REINF	Freestream Reynolds number per unit length
	PFS	Freestream static pressure, psfa
	PSTAG	Freestream stagnation pressure, psfa
	SCF	Scale factor to convert unit length for REINF (1.0 if REINF/ft, 12.0 if REINF/in. etc.)
	RNOSE	Nose radius, ft
CARD 15	XK1, XK2, CONVRG, ADTEST	(6F12.6)
	XK1	Constant for Van Driest Inner Eddy Viscosity Law. A value of 0.0 is reset to 0.4, the com- mon value
	X	Constant for Outer Eddy Viscosity Law. A value of 0.0 is reset to 0.0168, the common value
	CONVRG	Convergence criterion. A value of 0.0 is reset to 0.001, the recommended value
	ADTEST	Criterion for increasing ETAINF (F(IE))-F(IE-4) is compared with ADTEST.) A value of 0.0 is re- set to 0.001, the recommended value
CARD 16	DX, CRNI, XKETZ, ETAINF, REFLEN	(6F12.6)
	DX	Initial x stepsize
	CRNI	Selector for finite difference scheme; 1.0 for fully implicit

		(recommended), 0.5 for Crank-Nicolson, and 0.0 for fully explicit (not recommended)
	XKETA	Parameter which controls the grid spacing in the ETA direction (1.0 gives an equally spaced grid, a value greater than 1.0 gives a finer grid at the wall than at the outer edge.) A value of 0.0 is reset to 1.09, the value recommended for IE = 101
	ETAINF	Maximum value of ETA. A value of 0.0 is reset to 100 which is the recommended value for a flow which is initially turbulent. For an initially laminar flow this value should be set to 6.0)
	REFLEN	An arbitrary reference length
CARD 17	XJFAC, XKFAC, TVC	(2F12.6,4X,A3)
	XJFAC	Indicator; 0.0 for 2-D flow, 1.0 for axially symmetric flow
	XKFAC	indicator; 0.0 for body only solution, 1.0 for body and wake solution
	TVC	Indicator; YES to include TVC effects, NO without TVC
CARD 18	DXMAX, XLOCA, DYDX, DX, NOPRFS	
	DXMAX	Maximum x stepsize permitted in the calculations
	XLOCAT	Location on the body of the upstream edge of the Navier-Stokes region
	DYDX	Slope of straight taper fit of tail of body
	DX	x stepsize for use in the Navier-Stokes code
	NOPRFS	Number of profiles on the body in the Navier-Stokes region

CARDS 19a, b, c...

IPR

(IPR(J), J = 1, IPRINT) (14I5)

Array of subscript for array XSTA giving values of x at which complete solutions (with profiles) are printed (array dimensioned for 100 values)

CARDS 20a, b, c...

IPRFL

(IPRFL(J), J = 1, IPFL) (14I5)

Array of subscripts for array XSTA setting values of x at which complete solutions (with profiles) are printed (array dimensioned for 100 values). Also at these stations are printed the coordinates of the displaced body. Each value of IPRFL must also be a value of IPR

CARDS 21-21+IIMAX

ZA

ZA(J), XSTA(J), RZ(Z), PZ(J),  
LSTC (4F12.6,A4)

Array of coordinate values along the body axis

XSTA

Array of coordinate values along the body surface (same as ZA for a flat plate)

RZ

Array of radius values for a body

PZ

Array of pressure ratio values -  $P/P_0$  where  $P_0$  is the local stagnation pressure. (These are always 0.0 for the iterated solution and are given values only when KHESS = 0)

LSTC

Alphanumeric variable used to indicate the last data card. LAST is coded on the final card.

See Appendix B, Table 2.1 for a sample SUB DATA data set.

Description of HESSCP OUTPUT.

CARD1-IIMAX

X(J), CP(J), J = 1, IIMAX  
(2F12.6)



X	Axial coordinate of body point, ft
CP	Pressure coefficient at body point

See Appendix B, Table 2.2 for a sample HESSCP OUTPUT data set.

#### Description of Output Data.

ICBLINT outputs three data sets. The first is the complete boundary-layer solution over the body (BLAYER OUTPUT). The second is the velocity profile at the upstream edge of the Navier-Stokes region with information on the profile included (APLNS VELDATA). The third set is the coordinates of the displaced body (BODYCOOR DATA).

This section contains a description of BLAYER OUTPUT in three subsections. The first subsection describes the first section of the output which is the input and initialized data. The second subsection describes the data which are written for each station at which solutions are obtained. The third subsection describes the miscellaneous messages and data written by the program. The output from a sample calculation of turbulent flow over a cylinder is included at the end of this section (see Appendix C, Table 1.1).

#### Input and Initialized Data.

LABEL	,	Alphanumeric Data for identification of the case (written by Subroutine READIN)
-------	---	---

The data in the remainder of the first block is written by subroutine WRITE1 and corresponds to the input data with the following exceptions:

Line 6	RHOFS	=	$\rho_{\infty}$ , slugs/ft <sup>3</sup>
Line 10	EPSVD	=	$\epsilon_{VD} = \{\mu_{ref}/(\rho_{\infty} U_{\infty} L)\}^{1/2}$ , where L is the unit length in REINF

Next in the program output are the arrays IPR and IPRFL (which are described in the section "Description of Input"). Following the arrays IPR and IPRFL are the arrays ZA, RZ, XSTA, PZ, and UEZ with the array subscripts. PZ in the output differs from the values of PZ in the input in that for input PZ is  $P/P_0$  and is changed by the program to  $P/P_{ref}$ . UEZ is the array of nondimensional edge velocities calculated by the program ( $U_e/U_\infty$ ). For a flat plate, the values of UEZ are unity.

#### Station Data.

The station data are divided into two groups. The first group of data is written for each value of  $x$  at which a solution is obtained. The second group --the function profiles--is written only for the values of  $x$  corresponding to XSTA (IPFRL). In the first group, lines 5-13 are not written if  $x = 0$ . In the sixth line, REX alone is written if  $KFS = 0$ . If  $KFS \neq 0$ , REX is written followed by the wall heat transfer ( $\text{BTU}/\text{ft}^2/\text{sec}$ ) and two heat transfer coefficients; one in  $\text{BTU}/\text{in}^2\text{-sec-}^\circ\text{R}$ , the other in  $\text{lbm}/\text{in}^2\text{-sec}$ .

#### GROUP ONE

Line 1	S	,	Surface Distance, $x$
	XI	=	$\xi$ , Transformed Surface Distance
	Z	,	Axial Distance, $z$
	RO	,	Local Radius, $r$ , (Set Equal to One for a Wedge or a Flat Plate)
	BETA	=	$\beta = 2\xi/U_e (dU_e/d\xi)$
	PP	=	$dPE/ds$
	NIT	,	Number of Iterations at Current Value of $x$
	K	,	Station Counter

Line 2	UE	=	$U_e/U_\infty$
	PE	=	$P_e/P_{ref}$
	DUEDS	=	$dUE/ds$
Line 3	CF	,	Skin Friction in Transformed Coordinates = $C_{f_\infty}/\epsilon_{VD}$
	EPSVD	=	$\epsilon_{VD} = \{\mu_{ref}/(\rho_\infty U_\infty L)\}^{1/2}$ , Where L is the Unit Length in REINF
	KEP	,	Subscript in EPSPL Array Where the Inner and Outer Eddy Viscosities are Matched (Zero for Laminar Flow)
	NITTOT	,	Cumulative Total Number of Iterations in x Direction
Line 4	(F = U/U <sub>e</sub> ; Prime Denotes $\partial/\partial\eta$ )		
	F2N(1)	=	$F'_w$
	F2N(3)	=	F' at Two Points from the Wall
	F2NN(1)	=	$F''_w$
	F2NN(3)	=	F'' at Two Points from the Wall
	UPLUS	=	Friction Velocity
Line 5	CHIMAX	,	Maximum Value of Vorticity Reynolds Number - $\chi$
	GAMMA	,	Transition Intermittency Factor (Set to Zero for Laminar Flow, Set to One for Turbulent Flow)
	XIBAR	=	$\bar{\xi}$ , Transition Intermittency Factor Coordinate; Initialized as Zero, Calculated after Transition Regime is Entered
Line 6	REX	,	Local Reynolds Number Based on Edge Conditions



## WALL HEAT TRANSFER AND HEAT TRANSFER COEFFICIENTS (If KFS#0)

Line 7	CFE	=	$C_{f_e} = 2\tau_w/\rho_e U_e^2$
	CFINF	=	$C_{f_\infty} = 2\tau_w/\rho_\infty U_\infty^2$
	CF(TOTAL)	=	$\bar{C}_f = \frac{1}{x} \int_0^x C_{f_\infty} dt$
	CFBAR*SQRT(REX)	=	$\bar{C}_f \sqrt{REX}$
	CFINF*SQRT(REX)	=	$C_{f_\infty} \sqrt{REX}$
Line 8	CFINF/2	=	$C_{f_\infty}/2$
Line 9	X/REFLEN	=	x/reference length
	Z/REFLEN	=	z/reference length
	RO/REFLEN	=	r/reference length
	DELTA/X	=	$\delta/x$
	DELSTR/X	=	$\delta^*/x$
Line 10	THETA/REFLEN	=	$\theta$ /reference length
	DELSTR/REFLEN	=	$\delta^*$ /reference length
	DELTA/REFLEN	=	$\delta$ /reference length
	DELSTRAXI/ REFLEN	=	$\delta_{axi}^*$ /reference length
Line 11	THETA/DELTA	=	$\theta/\delta$
	DELSTR/DELTA	=	$\delta^*/\delta$
	DELSTR/THETA	=	$\delta^*/\theta$
	DELSTRAXI	=	$\delta_{axi}^* = r \{ \sqrt{1+2\delta^*/r} - 1 \}$ (Zero for 2-D Flow)
Line 12	DELSTRK	=	$\delta_k^*$ , Incompressible Boundary- Layer Displacement Thickness Computed Only for Turbulent Flow

DELSTR	=	$\delta^*$ , Boundary-Layer Displacement Thickness
DELTA	=	$\delta$ , Boundary-Layer Thickness (Value of $y$ where $U/U_e = 0.995$ )
THETA	=	$\theta$ , Boundary-Layer Momentum Thickness
RETHETA	=	$Re_\theta$ , Edge Unit Reynolds Number Times $\theta$

## GROUP TWO

## PROFILES

Block 1	ETA	,	$\eta$ , Transformed Normal Coordinate
	Y	,	$y$ , Corresponding Physical Coordinate
	Y/THETA	,	$y/\theta$ (Zero for $x = 0$ )
	Y/DELTA	,	$y/\delta$ (Zero for $x = 0$ )
	F=U/UE	,	Non-dimensional Velocity
	FP(N)	=	$\frac{\partial F}{\partial \eta}$
	YPLUS	=	Law of the Wall Normal Coordinate, $yU^+/\nu$
	U/UPLUS	=	$U/U^+$ Where $U^+ = (\tau_w/\rho)^{1/2}$
	UDEF	=	Defect Velocity, $\frac{U-U_\infty}{U^+}$
	EPS+	=	Eddy Viscosity (Zero for Laminar Flow)
	PITOT	=	The local pitot pressure in p.s.t.
	N	,	Grid Point Number

Miscellaneous Messages and Data.

Subroutine READIN writes the message "RESTART TAPE WRITTEN."

K = # KTPW = #" after the station data has been written on the restart

tape. K is the current value of K and KTPW is the next value of I at which the restart tape will be written.

For transition regime calculations, subroutine EFFMU writes the message "TRANSITION BEGINS" at the beginning of transition and the message "TRANSITION ENDS" when XIBAR first exceeds 2.0 with the Reichardt Eddy Viscosity Law or when XIBAR first exceeds 4.0 with the Van Driest Eddy Viscosity Law. The message "TRANSITION ENDS" was found to be useful when the Van Driest Eddy Viscosity Law was used in calculations but less useful with the Reichardt Eddy Viscosity Law. At best, the message indicates only approximately where transition ends.

For the instantaneous transition model, subroutine CHANGE writes the message "TRANSITION BEGINS INSTANTANEOUSLY" and the values of X and DX when transition is initiated.

If the iteration counter NIT reaches the value of NIT3, the stepsize is halved, new values of X and XI and new edge properties are calculated and the program attempts to obtain a converged solution for the smaller value of X. In this case, MAIN writes the values of NIT, DX, X, F2N(1), F2N1, and DIF.

When ETAINF is increased, subroutine ADDETA writes the message "INTERMEDIATE PROFILE DATA--ETAINF INCREASED ISTOP = #", and the values of DX, XKETZ, ETAINF, and ADTEST.

If ISTOP exceeds 100, the message "STOP \*\*\* ISTOP.GT.100" is written by MAIN and the program is stopped. If after a converged solution is obtained, the derivative of F at the wall is negative, subroutine WRITE2 writes the message "PROBLEM TERMINATED. NEGATIVE DF/DETA INDICATES THAT THE BOUNDARY LAYER HAS SEPARATED" and stops the program.



Normal termination of the program is indicated by the message "THE END X = XSTA(IIMAX)" or the message "THE END K = KEND" which is written twice by MAIN.

In the above descriptions, all quantities which have the apparent dimension of length have been nondimensionalized by the per unit length in REINF.

APLNS VELDATA contains the needed parts of the boundary-layer solution at the beginning of the Navier-Stokes region. All information in it is found in BLAYER OUTPUT and is written again for convenience in using the APLNS program.

BODY COORDATA contains the coordinates of the displaced body calculated during the current global iteration. This data set is used by program HESS for calculating a new pressure distribution around the body.

See Appendix B, Table 2.3 for a sample BODY COORDATA data set.

## DESCRIPTION OF PROCEDURE DEVELOP

After the viscous/inviscid solution has been completed, the final displaced body coordinates are used in DEVELOP EXEC to generate the inviscid, displaced flowfield. HESS is run to obtain the flow quantities at off body points (u & v components) for use in the APLNS program input conditions. Since the APLNS code requires 1800 points (as currently dimensioned) and HESS is capable of solving only 400 points per execution, several executions of HESS are required. Each execution supplies a strip of data for input to APLNS. The off-body point locations are developed and the data set written out in DATFIELD using the displaced coordinates from BODYCOOR DATA. DEVELOP EXEC controls the execution of FIELD and HESSBLI EXECs. Execution is in a loop, nominally the loop is executed five (5) times, DATFIELD is executed first, then with the data set written, HESSBLI is run, writing STREAM DATA. Subsequent iterations add data to STREAM DATA until the required full flowfield is completed (1800 points).

See Appendix A, Table 4.1 for a listing of DEVELOP.

### Program DATFIELD

Description of Program DATFIELD. FIELD EXEC controls program DATFIELD. DATFIELD writes out the data sets for the execution of HESS to obtain off-body flow conditions. Input data include the final displaced body from HESS/ICBLINT, and the geometry of the afterbody from DATAMA. DATFIELD then calculates and writes the off-body points, together with the displaced body coordinates on HESSCOOR DATA, the HESS data set.

See Appendix A, Table 4.2 for a listing of DATFIELD FORTRAN.

(See Description of Output for a list of variables used in the program.)

### Description of Input and Output.

Input Data. DATFIELD uses two input sets: INTER DATA and BODYCOOR DATA. INTER DATA has been described in Output for DATAMA. BODYCOOR DATA has been described in Output of ICBLINT.

Output Data. DATFIELD's output is in two sets: INTER DATA and HESS COORDATA. INTER DATA is rewritten to show the iteration count for DEVELOP. Only the counter, IHESSI is changed. HESS COORDATA contains the HESS data set with the off-body points where a solution is desired.

Card 1	HEDR, CASE	(15A4,2x,A4)
	HEDR	Alphanumeric array describing the body that is running
	CASE	Alphanumeric array defining the case run
Card 2	NB, NNU, NAXI, NCF, NOFF	(5I1)
	NB	Number of bodies input
	NNU	Number of nonuniform flows
	NAXI	Flag for axisymmetric flows; 0 if not axisymmetric, 1 if axisymmetric
	NCF	Flag for crossflow case; 0 if no cross flows included, 1 if crossflows included
	NOFF	Flag; 0 for no off-body points, 1 for off-body points
Card 3	blank	
Card 4	IGEOMF, ISIGF, ICURVN, NONEWF, IFORMT, NN1	
	IGEOMF	Flag for curved elements; 0 for no curvature, 1 for curvature



	ISIGF	Flag for source densities; set to 1; piecewise-linear
	ICURVN	Flag for computation of element curvatures; 0 for input curvatures, 1 for internal computation
	NONEWF	Number of new crossflows for the same body
	IFORMT	Flag; if 0, read first the x, then the y coordinates; if 1, read x,y coordinates in 2F12.6 format, if 2 read x,y coordinates in F12.6,12x,F12.6 format
	NN1	Number of off-body points
Card 5	IBDN	
	IBDN	Body sequence number
Cards 6-NN	X,Y	
	X,Y	Body coordinates
Card NN+7	IGEOMF, ISIGF, ICURVN, NONEWF, IFORMT, NN1	
	IGEOMF	Flag for curved elements; 0 for no curvature; 1 for curvature
	ISIGF	Described above
	ICURVN	Described above
	NONEWF	Described above
	IFORMT	Described above
	NN1	Described above
Card NN+8	IIBDN	
	IIBDN	Body sequence number; 0 if off-body points follow
Card NN+8-	XB, YB	
	XB, YB	, Coordinates of off-body points

See Appendix B, Table 3.1 for a sample HESS COORDATA data set.

#### Program APLNS

Description of Program APLNS. Program APLNS solves the complete Navier-Stokes equations using an Alternating Difference Implicit (ADI) scheme. Surrounding boundary conditions are required to initiate execution. The boundary conditions at the upstream boundary are held constant while the remainder of the flowfield is iterated upon. The iteration scheme is discussed in more detail later. Due to the large grid size used within the program, there are very few points within the boundary-layer region. Therefore, the results, particularly on the body, must be viewed with caution. To increase the accuracy of the results obtained from the APLNS program, the user is advised that the size of the region of interest be enlarged, i.e., the array sizes be increased from 30 X 60 to some larger values. The effect of this will be to make the far wake boundary conditions used in the program more appropriate the larger the region size, the better these conditions become. However, execution time will increase with such an enlargement. Care must be taken with regard to the initial flowfield which is input to the program. The stepsizes used must be compatible with the following criterion:

1. There must be at least three or four points within the boundary-layer. Therefore  $\Delta Y$  must be appropriately small.
2. The ratio  $\Delta Y/\Delta X$  must match the slope of the body at the tail region. Since the full Navier-Stokes equations are solved, the solution is very much dependent on the time stepsize.

For high velocities a very small time differential ( $0.1 \times 10^{-4}$  sec) must be used.

### Numerical Procedure

1. Set boundary conditions for  $\xi^{(n+1)}$  and  $\psi^{(n+1)}$ . Coefficients for  $u^{(n+\frac{1}{2})}$  and  $v^{(n+\frac{1}{2})}$  are extrapolated from the previous time step. Boundary conditions are known except for  $\xi_w^{(n+1)}$  which must be iterated upon.
2. Solve the Navier-Stokes equation using an Alternating Difference Implicit (ADI) scheme to get  $\xi^{(n+1)}$ .
3. Solve for  $\psi^{(n+1)}$  using a direct solver method with  $\xi^{(n+1)}$  for the right side.
4. Calculate new values of  $\psi^{(n+1)}$  and  $\xi^{(n+1)}$ .
5. Iterate on  $\psi$  and  $\xi$  until  $\partial u / \partial y)_w - \partial u / \partial y$  meets the convergence criterion.
6. Compute  $u^{(n+1)}$  and  $v^{(n+1)}$  from the new stream function.
7. Modify the stepsize, if necessary, to aid convergence.

Figures 10 and 11 show the flow of logic and the calling sequence of subroutines in program APLNS.

See Appendix A, Table 5.1 for a listing of program APLNS.

### Description of Variables in Common.

BLOCK	VARIABLE	DESCRIPTION OF USE
REALS	DFRODR	$1/\rho \partial F_x / \partial r$ lb-ft <sup>2</sup> /slug
REALS	DT	$\Delta t$ ; time increment (sec)
REALS	DTA	$\Delta t$ ; time increment (sec)
REALS	DT2	$\Delta t/2$
REALS	DX	Axial length increment (ft)



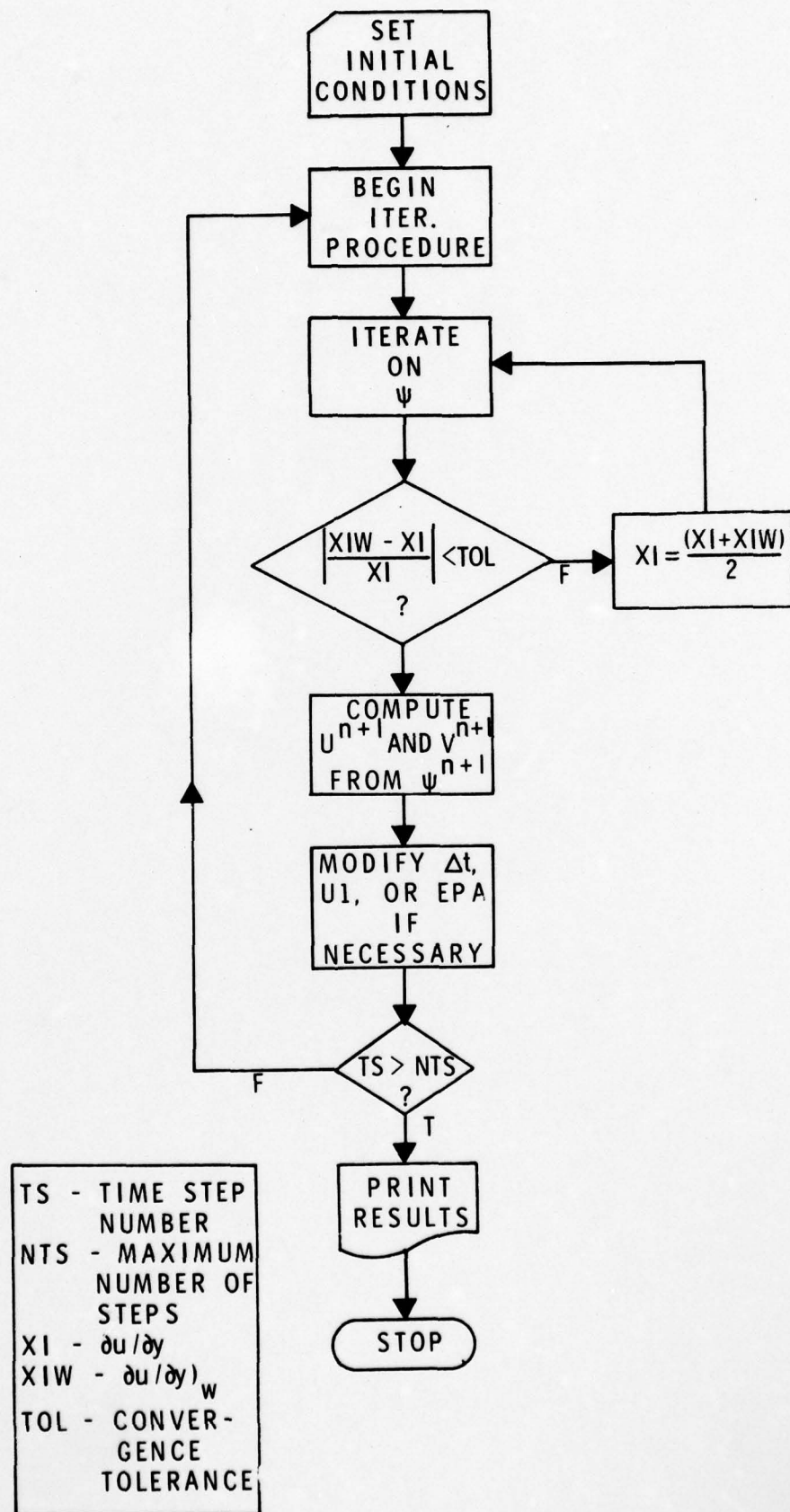


Figure 10. PROCEDURE FLOWCHART OF APLNS

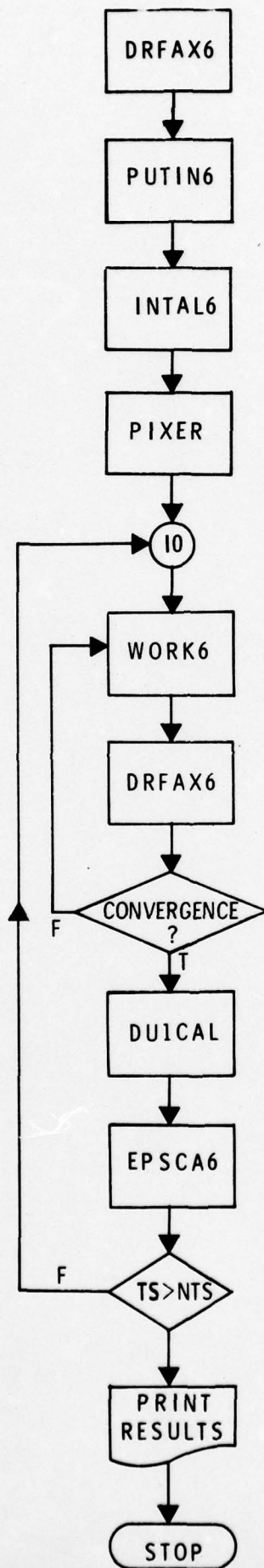


Figure 11. ROUTINE SEQUENCE FLOWCHART OF APLNS

REALS	DY	Radial length increment (ft)
REALS	DY2	$(\Delta y)^2$ (ft) <sup>2</sup>
ARRAYS	EPA	$\epsilon$ , epsilon at each axial location (eddy viscosity)
REALS	EPO	Beginning value of epsilon (ft <sup>2</sup> /sec)
REALS	EPS	Value of epsilon, eddy viscosity, if $\leq 0$ $\epsilon = 0.01686 U_e$ (ft <sup>2</sup> /sec)
REALS	FX	F <sub>x</sub> ; thrust magnitude (lb)
REALS	FXRHO	$F_x/\rho$ (lb-ft <sup>3</sup> /slug)
INTEGS	IDIMY	Number of columns for DMT010
INTEGS	IO	Input-output unit for any saved data
INTEGS	JCI	Point number on wall at the front of the region
INTEGS	JDEL	Boundary-layer edge point at the front of the region
INTEGS	JDIMY	Number of rows for DMT010
INTEGS	L	Number of points per profile
IRRAYS	LAR	Array which defines body shape
LOGICS	LSWH1	Control parameter set to FALSE value
INTEGS	L1	Height of the propeller zone in number of points



INTEGS	M	Number of profiles
INTEGS	M1	Number of profiles on the body
INTEGS	NER	Number of iterations on WORK6
INTEGS	NTS	Number of iterations for solution convergence
LOGICS	OFF	FALSE
LOGICS	ON	TRUE
LOGICS	PRNT	Controls printing for saved output
ARRAYS	PSI	$\psi$ ; stream function (ft <sup>3</sup> /sec)
ARRAYS	PSIB	$\psi$ ; used in WORK6 (ft <sup>3</sup> /sec)
ARRAYS	PSIO	$\psi$ ; on top of region (ft <sup>3</sup> /sec)
INTEGS	PSKP	Controls frequency of DULCAL and EPSCA6 execution
REALS	RHO	$\rho$ ; density (slugs/ft <sup>3</sup> )
REALS	R1	Modifies stepsize
LOGICS	SAVE	Control for saving output
PLOTZ	SKEY	Key for contour plots
PLOTZ	SL	Variables in PIXER
PLOTZ	SL1	Variables in PIXER
PLOTZ	SU	Variables in PIXER
LOGICS	SWHFX	Control for propeller
REALS	TDX	2 $\Delta$ X (ft)
REALS	TDY	2 $\Delta$ Y (ft)

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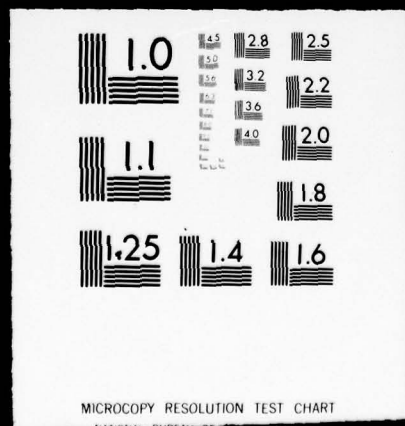
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REALS	TOL	Tolerance for convergence of WORK6
REALS	TRAMP	Modification factor of $1/\rho$ ( $\partial F_x/\partial r$ ) if necessary
ARRAYS	U	Axial velocity (ft/sec)
ARRAYS	UA	Axial velocity in WORK6 (ft/sec)
REALS	UO	Boundary-layer velocities at the front of the region (ft/sec)
ARRAYS	U1	Axial velocity at upper boundary of the region (ft/sec)
REALS	U2	$U_e$ ; edge velocity (ft/sec)
ARRAYS	U10	Initial axial velocity at upper boundary of the region (ft/sec)
ARRAYS	V	Radial velocity (ft/sec)
ARRAYS	VA	Radial velocity in WORK6 (ft/sec)
REALS	X	Axial location from front of the region (ft)
ARRAYS	XI	$\partial u/\partial y$ ( $\text{sec}^{-1}$ )
ARRAYS	XIB	$\partial u/\partial y$ calculation at the wall from stream function in WORK6 ( $\text{sec}^{-1}$ )
ARRAYS	XIW	$\partial u/\partial y$ at the wall ( $\text{sec}^{-1}$ )
REALS	Y	Radial distance from body centerline (ft)

### Description of Subroutines.

DRFAX6. DRFAX6 is the main driver for the axisymmetric case. The routine calls the major routines and tests for convergence of WORK6 calculations. The routine first calls two subroutines which read in data and set up initial conditions. Next, the routine begins the iteration procedure on the stream function, the main iteration loop of the program. After the convergence is met, the  $u$  velocities on the upper boundary are modified every PSKP time steps and modifications to the eddy viscosity are made every PSKP+1 time steps. The iteration on WORK6 is repeated NTS time steps with  $Dt$  modified depending on the number of iterations required for convergence of the previous time step. If more than three iterations were required,  $Dt$  is decreased by R1. If less than three iterations are required, the time step  $Dt$  is increased by the same factor R1. After NTS time steps or the number of iterations in WORK6 exceeds NER, DRFAX6 calls a routine to print the current stream function,  $\partial u / \partial y$  distribution, and the  $u$  and  $v$  velocity components.

Subroutine DU1CAL. DU1CAL calculates a  $\Delta u$  that is added to the  $u$  velocity on the upper boundary of the region. The routine is called periodically to update this boundary condition. A modified value for the stream function is used to calculate the  $\Delta u$ . The routine then prints out the profile number (I), the modified upper boundary condition (UI), the difference between the current velocity and the initial velocity (DDU1), the initial velocity (U10), and the initial stream function value (PSI0). It is important to note that only velocities on the upper boundary are altered in this routine.

Subroutine EPSCA6. EPSCA6 evaluates the eddy viscosity law. It is called periodically as DULCAL is called. The equation used is:

$$\frac{d\epsilon(x)}{dx} = \frac{C_2^2 U_e^2}{2} \left[ \frac{I_2}{I_1} \right] - \frac{a_2 \epsilon^2}{4 U_e C_2 b^2 I_1} - \frac{\epsilon_1}{2 I_1} \frac{dI_1}{dx} + \frac{\epsilon}{2b} \frac{db}{dx} - \frac{\epsilon}{2 U_e} \frac{dU_e}{dx}$$

where,

$$I_1(x) = \int_0^{\ell} \bar{u} \bar{r} \, d\bar{r},$$

$$I_2(x) = \int_0^{\ell} \frac{\partial \bar{u}}{\partial \bar{r}} \bar{r} \, d\bar{r}$$

and

$$\ell = C_2 b, \quad \bar{u} = U/U_e, \quad \bar{r} = r/b, \quad a_2 = 2.0, \quad C_2 = 0.035.$$

The routine prints out the following values

I1	Defined above
I2	Defined above
B	Value of b in above equation
DB	$\Delta B$
DI1	$\Delta I_1$
F1, F2, F3	Terms in the eddy viscosity law
EPN	New value of $\epsilon(x)$
EPA	Original value of $\epsilon(x)$

These updated values are then returned to the program and used to modify the flowfield conditions.

Subroutine INTAL6. INTAL6 is responsible for calculating the inviscid stream function from flowfield velocities read in from Unit 8 data. A simple integration, which has been found to be accurate,



is used to obtain the inviscid stream function. Since the velocities at every station in the flowfield are known, the stream function is calculated using a trapezoidal rule:

$$\Delta\psi_{ij} = (u_{ij}y_i + u_{i,j-1}y_{i-2})\Delta y/2$$

$$\psi_{ij} = \psi_{i,j-1} + \Delta\psi_{i,j}$$

with  $\psi = 0$  at solid body boundaries and for zero radius in the wake.

The inviscid flowfield is printed out giving values of  $\psi$  (PSI) and  $u$  and  $v$  velocity components. The value of  $r$  at the edge of the boundary-layer at the front of the region ( $Y(JDEL)$ ) is printed along with the boundary-layer thickness ( $Y(JDEL) - Y(J(I))$ ), and  $U_e$  ( $U2$ ). The boundary-layer velocity profiles are read in from Unit 11, and the values at the point in question  $Y(J)$  are interpolated using a 3 point Lagrangian formula. The momentum increase ( $FX(1,L1)$ ) is printed out giving the initial values of thrust computed from the following equation;

$$F_x/\rho = F_{x0} = 2 \frac{SU_0}{y(L1)^2 DX} ; \text{ where } SU_0 = \int_0^\delta U(U_e - U)dy$$

In attempting to correct for tip losses the following expression was used:

$$F_x/\rho = \frac{F_{x0}}{2} \left\{ 1 + \cos \left[ \pi \frac{r - (L1-5)\Delta r}{4\Delta r} \right] \right\} \text{ for } (L1-5)\Delta r < r < (L1-1)\Delta r$$

where  $L1(dr)$  is the height of the propeller region. The value of  $\delta^{*2}$  (DELSR2) is calculated by;

$$\delta^{*2} = \int_0^\delta \left( 1 - \frac{U}{U_e} \right) r dy$$

and the corresponding value of  $\epsilon$ (EPS) is given by:  $\epsilon = 0.0168 \delta^* U_e$ .

The boundary-layer velocity profile (U0) is printed out along with the values of X and Y for the region in question. The X distances are taken from the front of the region and the Y values are measured from the axis of the body. Finally  $(1/\rho) \partial F_x / \partial r$ (FXRHO) is printed completing the printed output from the routine.

Subroutine PUTIN6. PUTIN6 reads in values for the flags and various other parameters in the program and prints them out in namelist form. The routine defines the body shape by the LAR array which is also printed out. The initial values for variables which control the key values for the contour plot of  $\partial u / \partial y$ (XI) are printed. For a description of these parameters see the section entitled Description of Input.

Subroutine WORK6. WORK6 calculates the updated values of  $\xi$  which are compared in DRFAX6 and then modified if necessary. Since this routine essentially solves  $n$  equations in  $n$  unknowns, only the numerical procedure is important to the understanding of the workings of WORK6. The use of WORK6 is best seen by referring to the section entitled Numerical Procedure, steps 1-5.

#### Description of Input.

##### Input Variables on Unit 5.

<u>Namelist</u>	<u>Variable</u>	<u>Description of Use</u>
ILIST	L	, Number of points per profile, suggested value $\leq 30$
ILIST	L1	, Number of points on propeller, suggested value $\leq 12$
ILIST	M	, Number of profiles, suggested value $\leq 60$

ILIST	M1	,	Number of profiles on body, suggested value $\leq 15$
ILIST	PSKP	,	Time parameter controlling frequency of DULCAL and EPSCA6, suggested value 4-7
ILIST	NER	,	Number of iterations on WORK6, suggested value 40
ILIST	NTS	,	Number of time steps for convergence, suggested value 35
ILIST	IO	,	Unit number for saved output, suggested value 9
RLIST	DT	,	Time increment (sec), suggested value $1 \times 10^{-4}$ - $1 \times 10^{-5}$
RLIST	RHO	,	Density of fluid (slugs/ft <sup>3</sup> ), suggested value $7.535 \times 10^{-2}$
RLIST	EPS	,	Eddy viscosity (if $EPS \leq 0$ , $EPS = 0.0168 \delta^* U_e$ ), suggested value 0.0
RLIST	TOL	,	Tolerance value for convergence of WORK6, suggested value 0.02-0.05
RLIST	TRAMP	,	Modifying factor for propeller, suggested value 0.1
RLIST	EPO	,	Beginning value of epsilon, suggested value 0.0
RLIST	SCALE1	,	Length scaling factor for nondimensional HESS/ICBLINT I/O
RLIST	SCALE2	,	Velocity scaling factor for nondimensional HESS/ICBLINT I/O
LLIST	SWHFX	,	T No actuator disk F Include actuator disk



LLIST

**SAVE**

T Save data on previous unit defined by variable IO  
F Do not save data

See Appendix A, Table 3.1 for sample APLNS data.

Input Data on Unit 11.

<u>Variable</u>	<u>Description of Variable</u>
DYDX	$dy/dx$ ; slope of the body at the tail
DY	$\Delta y$ ; nondimensional radial length increment
NUM	Number of boundary-layer velocities given
DELTA	Nondimensional boundary-layer thickness
UE	Nondimensional edge velocity
YD	$y$ locations in the boundary layer
UUE	$U/U_\infty$ ; normalized boundary-layer velocities

See Appendix B, Table 3.2 for sample APLNS Unit 11 input data.

### Input Data on Unit 8.

X	Nondimensional axial distance from the front of the body
Y	Nondimensional radial coordinate from the body centerline
U	Nondimensional axial velocity component (INVISCID)
V	Nondimensional radial velocity component (INVISCID)

See Appendix B, Table 3.3 for sample APLNS Unit 8 data.

### Description of Output.

**Output Variables.** Listed in order of appearance.

<u>Origin</u>	<u>Variable</u>	<u>Description of Use</u>
PUTIN6	L	Number of points per profile

PUTIN6	L1	Number of points in the propeller zone (height)
PUTIN6	M	Number of profiles
PUTIN6	M1	Number of profiles on the body
PUTIN6	PSKP	Control variable concerning frequency of DULCAL and EPSCA6
PUTIN6	NER	Number of iterations on WORK6 (maximum)
PUTIN6	NTS	Total number of time steps for solution convergence
PUTIN6	I0	Unit number for saved output
PUTIN6	DT	Time increment (s)
PUTIN6	RHO	Density (slugs/ft <sup>3</sup> )
PUTIN6	EPS	Eddy viscosity (ft <sup>2</sup> /s)
PUTIN6	TOL	Tolerance value for convergence of WORK6
PUTIN6	TRAMP	Modification factor for derivative of thrust in the radial direction
PUTIN6	EPO	Eddy viscosity at beginning of problem (ft <sup>2</sup> /s)
PUTIN6	SCALE1	Length scaling factor (ft)
PUTIN6	SCALE2	Velocity scaling factor (ft/s)
PUTIN6	SWHFX	Control parameter for propeller
PUTIN6	SAVE	Control parameter for printing saved output
PUTIN6	LAR	Array defining body points in terms of grid location

PUTIN6	DX	Axial length increment(ft)
PUTIN6	DY	Radial length increment (ft)
PUTIN6	JDEL	Point number at the edge of the boundary-layer
INTAL6*	PSI	Inviscid stream function (ft <sup>3</sup> /s)
INTAL6*	U	Inviscid axial velocity (ft/s)
INTAL6*	V	Inviscid radial velocity (ft/s)
INTAL6	Y(JDEL)	Radial distance at the edge of the boundary-layer (ft)
INTAL6	Y(JDEL)-Y(J(I))	Boundary-layer thickness (ft)
INTAL6	U2	Axial velocity at the edge of the boundary-layer (ft/s)
INTAL6	FX	Force distribution of the actuator zone (lb <sub>f</sub> )
INTAL6	DELSR2	Square of the boundary-layer displacement thickness (ft <sup>2</sup> )
INTAL6	EPS	Eddy viscosity (ft <sup>2</sup> /s)
INTAL6	UO	Boundary-layer profile (ft/s)
INTAL6	Y	Radial distances of grid points from body centerline (ft)
INTAL6	X	Axial distances of grid points from front of region (ft)
INTAL6	FXRHO	Derivative of propeller force with respect to radial direction (lb <sub>f</sub> -ft <sup>3</sup> /slug)



DRFAX6	TIME	Time from the beginning of the procedure (s)
DRFAX6	XI	Derivative of axial velocity with respect to radial direction (1/s)
WORK6	N	Dimension of working matrix in WORK6
WORK6	IDIMY	Dimension of working matrix in WORK6
WORK6	JDIMY	Dimension of working matrix in WORK6
WORK6	I	Profile number
WORK6	J	Point number on profile
WORK6	XI(I,J)	XI at point I,J (1/s)
WORK6	XIW	Vorticity at the wall of the body at point I,J (1/s)
DRFAX6	ITER	Iteration number in WORK6
DRFAX6	XMAX	Maximum difference between $ XI - XIW /XI$ for all wall points
DRFAX6	TS	Time step number
DU1CAL	U1(I)	Updated axial velocity at the top of the region (ft/s)
DU1CAL	DDU1(I)	Difference between updated and original upper boundary axial velocity (ft/s)
DU1CAL	U10(I)	Initial axial velocity at the upper boundary (ft/s)
DU1CAL	PSIO	Stream function at the top of the boundary (ft <sup>3</sup> /s)
EPSCA6	B	Mixing zone width (ft)
EPSCA6	I1	$I_1(x) = \int_0^x \bar{u} \bar{r} \, d\bar{r}$

EPSCA6	I2	$I_2(x) = \int_0^x \frac{\partial \bar{u}}{\partial \bar{r}} \bar{r} d\bar{r}$
EPSCA6	DB	Change in the value of the mixing width (ft)
EPSCA6	DI1	Change in the value of $I_1(x)$ integral
EPSCA6	F1	Term in the eddy viscosity law
EPSCA6	F2	Term in the eddy viscosity law
EPSCA6	F3	Term in the eddy viscosity law
EPSCA6	EPN	New value of the eddy viscosity at profile I (ft <sup>2</sup> /s)
EPSCA6	EPA	Initial value of the eddy viscosity for profile I (ft <sup>2</sup> /s)
DRFAX6*	PSI	Final stream function (ft <sup>3</sup> /s)
DRFAX6*	XI	Final distribution for XI (1/s)
DRFAX6	V	Final values of radial velocities (ft/s)
DRFAX6	U	Final values of axial velocities (ft/s)

\* - Denotes printed within mentioned subroutine through a call to routine DMT010

See Appendix B, Table 3.4 for sample APLNS OUTPUT data.

APPENDIX A



## APPENDIX A

TABLE 1.1 WAKE EXEC

```

CP SPOOL CONS TO SYSTEM CLASS A
CP TAG DEV CONS PRIOR IOLE DEST RMT35
CP TAG DEV PR PPRIOR IOLE DEST RMT35
CP LINK GOOD 192 192 RR ALL
ACCESS 192 D
EXEC CDCP 5
EXEC BLINT 6
EXEC DEVELOP 5

```

TABLE 1.2 CDCP EXEC

```

&LOOP -ENDLOOP &1
EXEC DATADEV
EXEC HESSBLI HESSBLI DATA F
EXEC DATAMA
EXSERV READ SEPARA DATA E 3 31$COL 1 1 ICP
&IF .&ICP NE .1 &GOTO -NEXT
-ENDLOOP &CONTINUE
&TYPE MAX. NO. OF ITER. EXCEEDED.

```

&EXIT 8  
-NEXT &CONTINUE

TABLE 2.2 DATADEV EXEC

```
&CONTROL ALL
FI * CLEAR
GLOBAL TXLIB FORTLIB VPIUTIL
FI 01 DISK COORD DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 02 DISK SEPARA DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 03 DISK WAKE COORDS E (LRECL 80 BLKSIZE 80 RECFM FB
FI 04 DISK HESS PARMDATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 07 DISK HESSBLI DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 06 DISK ERERR DAATAA A
LOAD DATADEV (NOMAP
START
```

TABLE 2.3 DATADEV FORTRAN

```
C PROGRAM MAIN
C
C
```

## FILE DEFINITIONS

UNIT (1) BODY COORDINATES WITH PARAMETERS  
 UNIT (2) FLOW SEPARATION AND ITERATION DATA  
 UNIT (4) POTENTIAL FLOW CODE EXECUTION PARAMETERS  
 UNIT (7) COMPLETE DATA SET FOR POTENTIAL FLOW CODE  
 EXECUTION WITH FAIRED AFTERBODY.

\*\*\*\*\*

COMMON /COORD/ X,Y,KTE,XI,YI,KTEI,NOPRFS,KWAKE  
 DIMENSION X(501), Y(501), XI(501), YI(501)

READ IN THE ORIGINAL BODY

READ (1,30) KWAKE  
 READ (1,10) KTE, NOPRFS, KTEI  
 DO 1 I=1,KTE  
 1 READ (1,20) X(I), Y(I)  
 REWIND 1  
 CALL LINDEV  
 CALL HESSPA  
 10 FORMAT (1X,3I3)  
 20 FORMAT (2F12.6)  
 30 FORMAT (I3)  
 STOP  
 END





```

DC 3 J=KK,KTE
IF((XI(J)).LT.XXI(I)).AND.(XI(J+1).GT.XXI(I)) YVI(I) =--((XXI(I))-XI
I(J))/(XI(J+1)-XI(J))*(YI(J)-YI(J+1))+YI(J)
IF(XI(J).EQ.XXI(I)) YVI(I) = YI(J)
3 CONTINUE
DO 4 I=1,KTE
IF((XI(I)).LE.XXI(1)).AND.(XI(I+1).GT.XXI(1))) GO TO 6
4 CONTINUE

C
C
C
C
      REPLACE ORIGINAL WITH RELOCATED COORDINATES, MM IS THE TOTAL
      NUMBER OF NEW COORDINATES ON THE BODY.

6 NN = I
  NN = NN+1
  MM = NN+KK
  JJ = 0
  DO 7 I=NN,MM
    JJ = JJ+1
    XI(I) = XXI(JJ)
    YI(I) = YI(JJ)
    KTE = MM
  7 CONTINUE

C
C
C
      DEFINE THE NUMBER OF POINTS IN WAKE EXTENSION

  LWAKE = IWAKE*5
  KTE1 = KTE+LWAKE
  9 CONTINUE

C
C
C
      WRITE OUT BODY COORDINATES FOR USE ON NEXT ITERATION IF ONE
      WRITE (1,15) KWAKE

```

```

WRITE(1,10) KTE, NOPRFS,KTE1
WRITE (1,40) (XI(I),YI(I),I=1,KTE)
IF(IWAKE.EQ.0) GO TO 13
DO 8 I=KTE,KTE1
8 XI(I) = XI(I-1)+DX

      DEVELOP DATA FOR CURVE FIT

      XI = XI(KTE1)-XI(NNN)
      CALL FD3(XI(NNN),XI(NNN-1),XI(NNN),XI(NNN+1),YI(NNN-1),YI(NNN
1),YI(NNN+1),FX)
      C = FX
      Y1 = YI(NNN)
      CALL FIT
15 REWIND 2
      WRITE (2,10) IWAKE
      WRITE (2,10) JSTA,KTE
10 FORMAT (1X,3I3)
15 FORMAT (I3)
20 FORMAT (F12.6)
40 FORMAT (2F12.6)
      DESUG INIT
      RETURN
      END

```

C  
C  
C



```

C
C
C
C
SUBROUTINE HESSPA
SUBROUTINE HESSPA WRITES OUT A HESS DATA FILE USING COORDINATES
DEVELOPED BY FIT

COMMON /COORD/ X,Y,KTE,XI,YI,KTE1,NUPRFS,KWAKE
DIMENSION X(501),Y(501),XI(501),YI(501)
DIMENSION HEDR(15),CASE(2)
READ (4,10) HEDR,CASE,ICARD2,ICARD3,ICARD4,NN,IBDN
WRITE(7,10) HEDR,CASE,ICARD2,ICARD3,ICARD4,KTE1,IBDN
DC 1 J=1,KTE1
1 WRITE (7,20) XI(J),YI(J)
10 FORMAT (15A4,2X,2A4/13/15/1X,14,15/9X,11)
20 FORMAT (2F12.6)
RETURN
END

```

```

C
C
C
C
SUBROUTINE FIT
  FIT DEVELOPS A NUMERICALLY GENERATED CURVE GIVEN THE COORDINATES
  AND SLOPE AT TWO POINTS (AT THE T.E. THE SLOPE IS ASSUMED 0)

  REAL K,M
  COMMON/CORFIT/ DX,Y1,C,X1,NNN
  COMMON /COORD/ X,Y,KTE,XI,YI,KTEL,NOPRFS,KWAKE
  DIMENSION X(501),Y(501),XI(501),YI(501),XXI(500),YYI(500)
  M = C

  DELY IS THE ACTUAL Y STEP SIZE, DY IS THE INCREMENT OF DELY FOR
  THE NEXT ITERATION

  DELY = 0.
  DELX = DX
  DY = -.05*DELY
30 DELY = DELY+DY
  XPRIME = 0.
  YPRIME = 0.
  N = XI/DELY
  K = M*DELY/DELY
  L = NNN

  GENERATE Y'S FOR CURRENT ITERATION

  MF = N+1
  DO 5 I=1,MF
    L = L+1
    YPRIME = YPRIME+DELY*K**I
5 Y(L)=Y1+YPRIME
C

```

```

C      CHECK FOR CONVERGENCE
C
C      IF UNDERSHOOT, CONTINUE
C
C      IF (ABS(Y(KTE1)).LT..00001) GO TO 20
C
C      IF OVERSHOOT, GO BACK AND USE SMALLER DY'S
C
C      IF (Y(KTE1).LT.0.) GO TO 30
C      DELY=DELY-DY
C      DY = DY*.1
C      GO TO 30
20  CONTINUE
C      DO 10 L=NNN,KTE1
C      10  YI(L)=Y(L)
C      RETURN
C      END

```



```
C
FUNCTION ROUND (X,N)
THIS FUNCTION ROUNDS NUMBERS TO THE DESIRED DECIMAL PLACE N
ISIGN=1
IF (X.LT.0.0) ISIGN=-1
I=ABS(X)*10**N+0.5
ROUND=FLOAT(ISIGN*I)*10.0**(-N)
RETURN
END
```

```

SUBROUTINE FD3 (X,X1,X2,X3,F1,F2,F3,FX)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE FD3 IS CALLED BY SUBROUTINE DERIV3.

SUBROUTINE FD3 CALCULATES THE FIRST DERIVATIVE-FX-CORRESPONDING
TO POINT X USING 3 POINT LAGRANGIAN DIFFERENTIATION FORMULA.

ASSUMES X1 .LE. X .LE. X3.

A1=2.0*X-X2-X3
A2=2.0*X-X1-X3
A3=2.0*X-X1-X2
D1=(X1-X2)*(X1-X3)
D2=(X2-X1)*(X2-X3)
D3=(X3-X1)*(X3-X2)
C1=A1/D1
C2=A2/D2
C3=A3/D3
FX=C1*F1+C2*F2+C3*F3
RETURN
END

```

U U U U U U U U

TABLE 2.3      DATAMA EXEC

```

&CONTROL ALL
FI * CLEAR
GLOBAL TXTLIB FORLIB V2UTIL
FI 03 DISK WAKE COORDS E (LRECL 80 BLKSIZE 80 RECFM F
FI 04 DISK ICBL PARMDATA E (LRECL 100 BLKSIZE 80 RECFM FB
FI 05 DISK HESSBLI DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 06 DISK SUB DATA E (LRECL 100 BLKSIZE 80 RECFM FB
FI 07 DISK SEPARA DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 08 DISK SUMOS DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 09 DISK HESSBLI OUTPUT E (LRECL 80 BLKSIZE 80 RECFM FB
FI 10 DISK HESSCP OUTPUT E (LRECL 80 BLKSIZE 80 RECFM FB
FI 11 DISK COORD DATA E (LRECL 80 BLKSIZE 80 RECFM FB)
FI 12 DISK INTER DATA B
LOAD DATAMA (NOMAP
START

```

TABLE 2.5      DATAMA FORTAN

```

C
C
MA100010
MA100020

```





MAI00350  
 MAI00360  
 MAI00370  
 MAI00380  
 MAI00390  
 MAI00400  
 MAI00410  
 MAI00420  
 MAI00430  
 MAI00440  
 MAI00450  
 MAI00460  
 MAI00470  
 MAI00480  
 MAI00490  
 MAI00500  
 MAI00510  
 MAI00520  
 MAI00530  
 MAI00540

```

C      READ (11,30) KWAKE
      READ(3,10) JWAKE
      DO 1 I=1,JWAKE
1     READ(3,20) XWAKE(I)
      DO 2 J=1, JWAKE
2     YWAKE(J) = 0.0
      CALL CPDATA

C      IF THE FAIRING DOES NOT DRIVE THE CP'S LOW ENOUGH DO NOT WRITE
C      OUT HESS/ICBLINT DATA SETS
C
C      IF(ICP.NE.0) GO TO 3
C      CALL CURV
C      CALL READAT
10     FORMAT (I2)
20     FORMAT (F12.6)
30     FORMAT(I3)
      3 STOP
      END

```





```

C      CP(KTE1) = (1.+DEL)*F(KTE1)-DEL*F(KMINUS)
C      CPD00330
C      CPD00340
C      FIND LAST, MOST NEGATIVE CP'S AND LOCATION FOR USE IN GIVING INIT
C      CPD00350
C      INITIAL WAKE PRESSURES. ALSO DETERMINE IF CP'S GO TO HIGH IN
C      CPD00360
C      REGION OF TRAILING EDGE
C      CPD00370
C      CPD00380
C      CPD00390
C      CPD00400
C      CPD00410
C      IF ((CP(I-1).GT.CP(I)).AND.(CP(I+1).GT.CP(I)).AND.(CP(I).LE.O.))
C      CPD00420
C      IICPAR = I
C      CPD00430
C      IF ((CP(I).GT.O.).AND.(CP(I-1).LT.O.)).OR.((CP(I).LT.O.).AND.
C      CPD00440
C      1(CP(I-1).GT.O.)) IINFL = IINFL+1
C      CPD00450
C      IF (IINFL.EQ.2).AND.(CP(I).GE.O.2)) ICP = 1
C      CPD00460
C      IF ((CP(I).GT.O.).AND.(CP(I-1).LT.O.)).OR.((CP(I).LT.O.).AND.
C      CPD00470
C      1(CP(I-1).GT.O.)) JSTA = I
C      CPD00480
C      2 CONTINUE
C      CPD00490
C      IF (KWAKE.EQ.O) GO TO 6
C      CPD00500
C      CPD00510
C      FIND WHERE WAKE STARTS AND FAIRING ENDS
C      CPD00520
C      CPD00530
C      JTE = KTE1+1
C      CPD00540
C      DO 8 I=1,JWAKE
C      CPD00550
C      IF (XW(KTE1).LT.XWAKE(I)) GO TO 9
C      CPD00560
C      8 CONTINUE
C      CPD00570
C      GO TO 6
C      CPD00580
C      PUT WAKE POINTS INTO ACTUAL COORDINATE ARRAYS
C      CPD00590
C      CPD00600
C      CPD00610
C      CPD00620
C      CPD00630
C      CPD00640
C      9 II = I
C      IIMAX = KTE1+JWAKE-II
C      IICUNT = II

```

```

DC 3 I=JTE,IIMAX
ICOUNT = ICOUNT+1
XW(I) = XWAKE(ICOUNT)
3 CP(I) = CP(ICPAR)
6 DC 4 I=1,IIMAX

WRITE OUT THE FULL ON-COORDINATE CP DATA SET WITH WAKE POINTS
ANY
4 WRITE(10,10) XW(I), CP(I)
IWAKE = IWAKE+1
REWIND 7

WRITE OUT THE SEPARATION DATA

WRITE (7,20) IWAKE
WRITE (7,20) JSTA,KTE
WRITE (7,30) ICP
RETURN
10 FORMAT (3F12.6)
20 FORMAT (1X,3I3)
30 FORMAT (13)
END

```

```

C
C
C
C
C
SUBROUTINE CURV
SUBROUTINE CURV DEVELOPS THE DATA FOR USE IN THE INVISCID FLOW
FIELD DEVELOPMENT, INCLUDING FITTING A STRAIGHT TAPERED TAIL TO
THE ORIGINAL BODY.
COMMON /WAKE/XWAKE,YWAKE,KTE,IIMAX,KWAKE,KTEL,X,Y,XI,YI,JSTA
1,DYDX,XLOCAT,JWAKE
DIMENSION X(501),Y(501),XI(501),YI(501),XWAKE(20),YWAKE(20)
DATA IHESI/1/
READ IN ORIGINAL BODY COORDINATES
READ (11,10) KTEE,NOPRFS,KTEA
READ (11,20) (XI(I),YI(I),I=1,KTEE)
N = 0
1 JSTA = JSTA-N
DX = (XI(KTEL)-XI(JSTA))/NOPRFS
N = N+1
DYDX = YI(JSTA)/(XI(JSTA)-XI(KTEL))
DY = ABS(DYDX*DX)
IF(DY.LT..0020) GO TO 1
XLOCAT = XI(JSTA)
WRITE (12,30) IHESI,XLOCAT,DX,DY
WRITE (13,30) KTEL
30 FORMAT (11/3F12.6)
10 FORMAT (1X,3I3)
20 FORMAT (2F12.6)
RETURN
END
C
C
C
C
C
CUR00010
CUR00020
CUR00030
CUR00040
CUR00050
CUR00060
CUR00070
CUR00080
CUR00090
CUR00100
CUR00110
CUR00120
CUR00130
CUR00140
CUR00150
CUR00160
CUR00170
CUR00180
CUR00190
CUR00200
CUR00210
CUR00220
CUR00230
CUR00240
CUR00250
CUR00260
CUR00270
CUR00280

```



```

C
C
C
C
SUBROUTINE READAT
  READAT READS AND WRITES OUT THE HESS/ICBLINT DATA SETS IF
  FAIRING ITERATION WAS SUCCESSFUL

  COMMON /WAKE/ XWAKE,YWAKE,KTE,IIMAX,KWAKE,KTEL,X,Y,XI,YI,JSTA,
  IDYDX,XLOCAT,JWAKE
  DIMENSION X(501), Y(501), XSTA(501), XWAKE(20), YWAKE(20), HEDR(15)
  1), LABEL(18), IPR(101), IPFL(101), CASE(2), XI(501), YI(501)
  DATA LSTC/4HLAST/
  ZERO = 0.0
  READ(4,10) IREAD, IRSRT,ITER, KHESS
  WRITE(6,10) IREAD, IRSRT, ITER, KHESS
  READ(5,20) HEDR, CASE,ICARD2,ICARD3,ICARD4, NN,IBDN
  WRITE(6,20) HEDR, CASE,ICARD2,ICARD3,ICARD4, KTEL,IBDN
  READ(4,30) BETAS, ROMAX
  WRITE(6,30) BETAS, ROMAX
  READ(4,40) LABEL
  WRITE(6,40) LABEL
  READ(4,50) NOSE, LAMTRB, KVSLAW, KTRANS, KTRNSN, KONSET, KTE
  WRITE(6,50) NOSE, LAMTRB, KVSLAW, KTRANS, KTRNSN, KONSET, KTE1
  READ(4,10) NIT1, NIT2, NIT3, NC
  WRITE(6,10) NIT1, NIT2, NIT3, NC
  READ(4,60) IF, KEND, KKMAX
  WRITE(6,60) IF, KEND, IIMAX
  READ(4,10) KADETA, KL, IPFL, IPRINT, IWT
  WRITE(6,10) KADETA, KL, IPFL, IPRINT, IWT
  READ(4,30) CHICRT, WBAP, ATR
  WRITE(6,30) CHICRT, WBAP, ATR
  READ(4,25) UFS, REINF, PFS, PSTAG, SCF, RNOSE
  WRITE(6,25) UFS, REINF, PFS, PSTAG, SCF, RNOSE
  READ(4,30) XF1,XF2, CONVRG, ADTEST
  
```

```

  REA00010
  REA00020
  REA00030
  REA00040
  REA00050
  REA00060
  REA00070
  REA00080
  REA00090
  REA00100
  REA00110
  REA00120
  REA00130
  REA00140
  REA00150
  REA00160
  REA00170
  REA00180
  REA00190
  REA00200
  REA00210
  REA00220
  REA00230
  REA00240
  REA00250
  REA00260
  REA00270
  REA00280
  REA00290
  REA00300
  REA00310
  REA00320
  
```

```

WRITE(6,30) XF1,XF2, CONVRG, ADTEST
READ (4,30) DX, CRNI, XKETA, FTAINF, REFLEN
WRITE(6,30) DX, CRNI, XKETA, FTAINF, REFLEN
READ (4,70) XJFAC, XKFAC, TVC
WRITE(6,70) XJFAC, XKFAC, TVC
READ (4,30) DXMAX
WRITE(6,35) DXMAX, XLOCAT, DYD, JSTA, NOPRFS
IF (IIMAX.GT.101) GO TO 4
DO 5 J=1,IIMAX
  IPR(J) = I
  IPRFL(J) = I
5 CONTINUE
GO TO 6
4 IPRINT = 101
  IPFL = 101
  K = IIMAX-101
DO 7 J=1,101
  IPR(J) = IPR(J-1)+1
  IF(J.LE.K) IPR(J) = 2*J-1
  IPRFL(J) = IPR(J)
7 CONTINUE
6 WRITE(6,80) (IPR(J),J=1,IPRINT)
  WRITE(6,80) (IPRFL(J),J=1,IPFL)
  READ (8,100) (XSTA(I), I=1,KTEL)
DO 2 I=1,KTEL
2 READ (5,30) X(I), Y(I)
  IF(KWAKE.EQ.0) GO TO 3
  KPLUS = KTEL+1
  ICOUNT = JWAKE
DO 1 I = KPLUS, IIMAX
  ICOUNT = ICOUNT+1
  X(I) = XWAKE(ICOUNT)

```

REA00330  
 REA00340  
 REA00350  
 REA00360  
 REA00370  
 REA00380  
 REA00390  
 REA00400  
 REA00410  
 REA00420  
 REA00430  
 REA00440  
 REA00450  
 REA00460  
 REA00470  
 REA00480  
 REA00490  
 REA00500  
 REA00510  
 REA00520  
 REA00530  
 REA00540  
 REA00550  
 REA00560  
 REA00570  
 REA00580  
 REA00590  
 REA00600  
 REA00610  
 REA00620  
 REA00630  
 REA00640

REA00650  
 REA00660  
 REA00670  
 REA00680  
 REA00690  
 REA00700  
 REA00710  
 REA00720  
 REA00730  
 REA00740  
 REA00750  
 REA00760  
 REA00770  
 REA00780  
 REA00790  
 REA00800  
 REA00810  
 REA00820  
 REA00830  
 REA00840  
 REA00850

```

Y(I) = YWAKE(I)
1 XSTA(I) = XSTA(I-1)+(X(I)-X(I-1))
3 JJMAX = IIMAX-1
  WRITE (6,110) (X(I),Y(I),XSTA(I),ZERO, I=1, JJMAX)
  WRITE (6,90) X(IIMAX),Y(IIMAX),XSTA(IIMAX),ZERO,LSTC
  WRITE (13,120) KTEI
10 FORMAT (6(7X,13))
20 FORMAT (15A4,2X,2A4/I3/I5/I1X,I4,I5/9X,I1)
25 FORMAT (F12.6, E12.6, 4F12.6)
30 FORMAT (6F12.6)
35 FORMAT (3F12.6,2I3)
40 FORMAT (18A4)
50 FORMAT (8I10)
60 FORMAT (4(7X,13))
70 FORMAT (2F12.6,4X,A3)
80 FORMAT (14I5)
90 FORMAT (4F12.6,A4)
100 FORMAT (12X,F12.6)
110 FORMAT (4F12.6)
120 FORMAT (2X,13)
      RETURN
      END
  
```



TABLE 3.1 BLINT EXEC

```

CP MSG SUB STARTING BLINT
CP LINK GOOD 192 192 RF ALL
ACCESS 192 D
CP LINK SUB 192 194 PR ALL
ACCESS 194 C
CP TAG DEV PRT ACCT 51841 LONGKEY EVETS PRIOR IDLE DEST LOCAL
&ITER = &I
&COUNT = 1
&LOOP -ENDLOOP &ITER
EXEC BLAYER SUB DATA B
&IF &RETCODE NE 0 &EXIT 1
EXEC HESSBLI BODYCOOP DATA B
EXEC CREPLOT1
EXEC CREPLOT2
&IF &RETCODE NE 0 &EXIT 2
EXEC BLDMAKER DATAMAKER DATA B
&IF &RETCODE NE 0 &EXIT 3
&COUNT = &COUNT + 1
EXEC CHITER &COUNT
&IF &RETCODE NE 0 &EXIT 4
-ENDLOOP &CONTINUE
EXEC BLNTPLT1 &ITER
EXEC BLNTPLT2 &ITER

```

TABLE 3.2 HESSBLI EXEC

```

&CONTROL ALL
FI * CLEAR
GLOBAL TXLIB FORTLIB
FI 5 DISK &1 &2 &3
TESTBAT
&IF &RETCODE EQ 0 &GOTO -NOTBAT
FI 06 PRINTER
&GOTO -REST
-NOTBAT &CONTINUE
-REST &CONTINUE
FI 06 DISK HESSA OUTPUT A ( RECFM FA BLKSIZE 133
&CONTINUE
FI 1 DISK FILE FT01 A
FI 2 DISK FILE FT02 A
FI 3 DISK FILE FT03 A
FI 4 DISK FILE FT04 A
FI 8 DISK FILE FT08 A
FI 9 DISK FILE FT09 A
FI 10 DISK FILE FT10 A
FI 11 DISK FILE FT11 A
FI 12 DISK FILE FT12 A
FI 13 DISK FILE FT13 A
FI 15 DISK FILE FT15 A
FI 16 DISK FILE FT16 A
FI 17 DISK HESSBLI OUTPUT E ( LRECL 80 BLKSIZE 80 RECFM FB
FI 18 DISK HESSCP OUTPUT A (LRECL 80 BLKSIZE 80 RECFM FB

```

```

FI 19 DISK SUMDS DATA E (LRECL 80 BLKSIZE 80 RECFM FB
FI 21 DISK STREAM DATA E (RECFM FB BLKSIZE 87 LRECL 87 DISP MOD
LOAD HESSBLI HESSA (CLEAR NOMAP
START
&EXIT &RETCODE

```

TABLE 3.3 BLDMMK EXEC

```

FI 17 DISK HESSBLI OUTPUT E (LRECL 80 BLKSIZE 80 RECFM FB
FI 18 DISK HESSCP OUTPUT B (LRECL 80 BLKSIZE 80 RECFM FB
FI 19 DISK &1 &2 &3
LOAD BLDMMK
START
&EXIT &RETCODE

```

TABLE 3.5 BLDMMK FORTRAN

```

DIMENSION CP(401),XW(401),X(401),F(401)
100 FORMAT (3F12.6)
110 FORMAT (2F12.6)
120 FORMAT (2X,13)

```

```

BLD000010
BLD000020
BLD000030

```



```

      READ(19,120) IBDYPT
      IPTM1=IBDYPT-1
10  READ (17,100) (XW(I),X(I),F(I),I=1,IBDYPT)
      CP(1)=F(1)
      DO 20 I=2,IPTM1
20  CP(I) = (F(I)+F(I+1))/2.0
      DELX1=X(IBDYPT)-X(IPTM1)
      DELX2=XW(IBDYPT)-X(IBDYPT)
      DEL=DELX2/DELX1
      CP(IBDYPT)=(1+DEL)*F(IBDYPT)-DEL*F(IPTM1)
      WRITE (18,110) (XW(I),CP(I),I=1,IBDYPT)
      STOP
      END

```

```

      BLD000050
      BLD000060
      BLD000070
      BLD000080
      BLD000090
      BLD000100
      BLD000110
      BLD000120
      BLD000130
      BLD000140
      BLD000150
      BLD000160

```

TABLE 3.6 BLAYER EXEC

```

&CONTROL ALL
GLOBAL TXLIB FORTLIB VPIUTIL
FI * CLEAR
FI 03 DISK BODYCUR DATA B ( LRECL 80 BLKSIZE 80 RECFM FB
FI 18 DISK HESSCP OUTPUT B (LRECL 80 BLKSIZE 80 RECFM FB
FI 19 DISK SUMDS DATA B (LRECL 80 BLKSIZE 80 RECFM FB
FI 20 DISK RESTART DATA B (LRECL 80 BLKSIZE 800
FI 05 DISK &1 &2 &3 ( LRECL 80 BLKSIZE 80 RECFM FB
&IF &RETCODE NE 0 &EXIT &RETCODE
TESTBAT
&IF &RETCODE EQ 0 &GOTO -NCIBAT
FI 06 PRINTER
&GOTO -REST
-NCIBAT &CONTINUE
-REST &CONTINUE
FI 06 DISK BLAYER OUTPUT E ( RECFM FA BLKSIZE 133
&CONTINUE
FI 21 TERM
FI 22 DISK VCRT DATA B (LRECL 132 BLKSIZE 13200 RECFM FB
FI 07 DISK APLNS VELDATA E (LRECL 80 BLKSIZE 80 RECFM FB
LOAD RESTAR READIN VELDAT ICLINT (CLEAR NOMAP
START
&EXIT &RETCODE

```

TABLE 3.7 ICBLINT FORTRAN

C	MAIN PROGRAM	PROGRAM ICBL	MAIN 10
C		NOVEMBER 1975	MAIN 20
C			MAIN 30
C			MAIN 40
C			MAIN 50
C			MAIN 60
C	A PROGRAM FOR 2-D AND AXISYMMETRIC INCOMPRESSIBLE TRANSITIONAL AND		MAIN 70
C	FOR TURBULENT BOUNDARY-LAYER FLOW INCLUDING EFFECTS OF TRANSVERSE		MAIN 80
C	CURVATURE		MAIN 90
C			MAIN 100
C		BY	MAIN 110
C	D.L. DWYER, C.H. LEWIS AND E.C. ANDERSON		MAIN 120
C	AEROSPACE AND OCEAN ENGINEERING DEPT.		MAIN 130
C	VIRGINIA POLYTECHNIC INSTITUTE AND STATE UNIVERSITY		MAIN 140
C	BLACKSBURG, VA. 24061		MAIN 150
C	PHONE - (703)-552-6126		MAIN 160
C			MAIN 170
C			MAIN 180
C	MAIN ROUTINE		MAIN 190
C	IMPLICIT REAL*8(A-H,O-Z)		MAIN 200
C			MAIN 210
C	MAIN CALLS SUBROUTINES ADDETA, CHANGE, CCEF, DELTAS, DERIV3,		MAIN 220
C	GEOM, INIT, MOMENT, PRFILE, READIN, WRITE1 AND WRITE2.		MAIN 230



```

MAIN PROVIDES CONTROL OF THE FLOW OF LOGIC IN THE PROGRAM AND
SOME CALCULATIONS.
MAIN 240
MAIN 250
MAIN 260
MAIN 270
MAIN 280
MAIN 290
MAIN 300
MAIN 310
MAIN 320
MAIN 330
MAIN 340
MAIN 350
MAIN 360
MAIN 370
MAIN 380
MAIN 390
MAIN 400
MAIN 410
MAIN 420
MAIN 430
MAIN 440
MAIN 450
MAIN 460
MAIN 470
MAIN 480
MAIN 490
MAIN 500
MAIN 510
MAIN 520
MAIN 530
MAIN 540
MAIN 550

COMMON /ARRAY1/ AOB(101),AOBP(101),A1(101),A2(101),A3(101),A4(101),
1,CHI(101),DN(102),DN2(102),EPSO(101),EPSPL(101),FI(101),FIN(101),FMAIN
21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(1
301),XN(102),XN2(102),Y(101),YCVDEL(101),YCVTH(101),YY(101)
COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(
1101),RZ(501)
COMMON /CONVRG/ CONVRG,CCRN1,CRNI,DIF,DIFF,NC
COMMON /COEFF3/ CF1,SUM
COMMON /COMWLL/ A1B,E1,FF,F2N1,VW
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA,DUEOS,PE,PESO,PP,UE,UERO2,UESO
COMMON /FRSTRM/ PFS,REINF,RHOF5,UFS
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXCLD,PNC,REFLEN,SCF,X,X1,XI2,XIOLD,MA
1,XJ,XJFAC,Z,ZOL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITMA
13,NOSE
COMMON /INTEGER/ I1,IPFL,IPRINT,JJ,K,KACETA,KEND,KEP,KSTOP,KTRNSN,LMA
1AMTRB,NITOT
COMMON /NMLCRD/ ADTEST,ETAINF,XKETA
COMMON /REF/ PREF,RHOREF,UREF
COMMON /VSCST/ EPSVD,XK1,XK2
COMMON /DIFP/ DIFM(301)
COMMON /COEFF/ CFBAR,CFBREX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,MA
1DSTARX,DSTARX,HAFCF,RETHET,REX,THET
COMMON /TVCURV/ TVC,BONANG,RTVC(101),RCRW(101),RORWSQ(101),RW
COMMON /SPTVC/ RNOSE
COMMON /WAK/ XKFAC

```

```

COMMON /TE/ KTE,KISTIE
COMMON /HESS/ IMRTH
COMMON /STRUP/ IREAD,IRSRT,KK
C
C
DATA YES/3HYES/
C
C
ABS(X)=DABS(X)
SQRT(X)=DSQRT(X)
CALL ERRSET(208,260,2)
C
C
READ INPUT DATA; EXECUTION PARAM
RESTART TAPE IF ONE.
C
C
CALL READIN
IF (IREAD.EQ.1) GO TO 70
K=0
CALL INIT
EPSVD=1./SQRT(REINF)
CALL WRITE1
CALL PRFILE
XIOLD=XI
XGILD=X
Y(1)=0.0
YY(1)=0.0
RW=1.00
IF (XJFAC.GT.1.0-05.OR.XKFAC.GT.1.0-05) RW=RO
RTVC(1)=RW
RORW(1)=1.000
IF (XKFAC.LT.1.0-05) GO TO 10
IF (INOSE.EQ.1) RORW(1)=1.00/DUEDS
C
C
MAIN 560
MAIN 570
MAIN 580
MAIN 590
MAIN 600
MAIN 610
MAIN 620
MAIN 630
MAIN 640
MAIN 650
MAIN 660
MAIN 670
MAIN 680
MAIN 690
MAIN 700
MAIN 710
MAIN 720
MAIN 730
MAIN 740
MAIN 750
MAIN 760
MAIN 770
MAIN 780
MAIN 790
MAIN 800
MAIN 810
MAIN 820
MAIN 830
MAIN 840
MAIN 850
MAIN 860
MAIN 870

```





```

C
IF (XKFAC.GT.1.D-06) RDDD=DUEDS
RT=0.D0
DO 40 N=2,IE
Y(N)=XN(N)*DUEDS*(XKFAC-.5D0)/DSQRT(XJFAC+XKFAC+1.D0)
CONTINUE
CONTINUE
ANG=80DANG
CSORW=1.D0
IF (RW.GT.1.D-06) CSUFW=DCCS(ANG)/RW
FCP NO TRANSVERSE CURVATURE CASE
DO 60 N=2,IE
RORW(N)=RORW(1)
RORWSQ(N)=RORWSQ(1)
RTVC(N)=RW
YY(N)=Y(N)*EPSVD
IF (TVC.NE.YES) GO TO 60
FOR TRANSVERSE CURVATURE CASES
YY(N)=(-1.D0+SQRT(1.D0+2.D0*EPSVD*Y(N)*CSORW))/CSORW
RDJM=RD+RDD*YY(N)*CSORW
RTVC(N)=RT*RDJM
RORW(N)=RDJM/RDDD
RORWSQ(N)=RORW(N)**2
Y(N)=YY(N)/EPSVD
CONTINUE
BEGIN MARCHING INTEGRATION
60
C
C
C

```

```

MAIN1200
MAIN1210
MAIN1220
MAIN1230
MAIN1240
MAIN1250
MAIN1260
MAIN1270
MAIN1280
MAIN1290
MAIN1300
MAIN1310
MAIN1320
MAIN1330
MAIN1340
MAIN1350
MAIN1360
MAIN1370
MAIN1380
MAIN1390
MAIN1400
MAIN1410
MAIN1420
MAIN1430
MAIN1440
MAIN1450
MAIN1460
MAIN1470
MAIN1480
MAIN1490
MAIN1500
MAIN1510

```

```

70      KK=1
      DO 270 K=KK,KEND
      IREAD=0
      F1(1)=0.00
      F2(1)=0.00
      FC(1)=0.00
      F2N(1)=1.00
      CONTINUE
80      GENERATE CURVATURE DATA FOR RESTARTED EXECUTION
      GENERAL 2-D CASE
      NL WAKE
      RW=1.00
      FOR WAKE CASES
      IF (XJFAC.GT.1.D-05.OR.XKFAC.GT.1.D-05) RW=RO
      RTVC(1)=RW
      RORW(1)=1.00
      RCRWSQ(1)=1.00
      IF (NOSE.EQ.1.AND.K.EQ.1) GO TO 110
      IF (XKFAC.LT.1.D-05) GO TO 90
      SHARP NUSE, WAKE CASES
      RORW(1)=RW/UE
      RCRWSQ(1)=RORW(1)**2
      CONTINUE
90      DO 100 N=2,IE

```

```

MAIN1520
MAIN1530
MAIN1540
MAIN1550
MAIN1560
MAIN1570
MAIN1580
MAIN1590
MAIN1600
MAIN1610
MAIN1620
MAIN1630
MAIN1640
MAIN1650
MAIN1660
MAIN1670
MAIN1680
MAIN1690
MAIN1700
MAIN1710
MAIN1720
MAIN1730
MAIN1740
MAIN1750
MAIN1760
MAIN1770
MAIN1780
MAIN1790
MAIN1800
MAIN1810
MAIN1820
MAIN1830

```

```

100      Y(N)=XN(N)*PNC
        CONTINUE
        RDD=RW
        RD=RW
        RDD=RD
        IF (XKFAC.GT.1.D-06) RDD=UE
        IF (XKFAC.GT.1.D-06.AND.RW.LT.1.D-06) RDD=1.D0
        RT=1.D0
        GC TO 140
        CONTINUE

110      PLUNT NDSE CASE
        C
        C
        C
        RD=RN0SE
        RDD=1.D0
        RDD=RD
        IF (XKFAC.LT.1.D-06) GC TO 120
        C
        BLUNT NCSE, WAKE CASE
        C
        C
        RDD=DUEDS
        RORW(1)=1.D0/DUEDS
        RCRWSQ(1)=RORW(1)**2
        CONTINUE
        RT=0.D0
        C
        CALCULATE UNSTRETCHED COORDINATES FOR BLUNT NDSE, WAKE CASES
        C
        C
        DC 130 N=2, IE
        Y(N)=XN(N)*DUEDS**(XKFAC-.500)/DSQRT(XJFAC+XKFAC+1.D0)
        CONTINUE
        C
130      CONTINUE
140      CONTINUE

```

```

MAIN1840
MAIN1850
MAIN1860
MAIN1870
MAIN1880
MAIN1890
MAIN1900
MAIN1910
MAIN1920
MAIN1930
MAIN1940
MAIN1950
MAIN1960
MAIN1970
MAIN1980
MAIN1990
MAIN2000
MAIN2010
MAIN2020
MAIN2030
MAIN2040
MAIN2050
MAIN2060
MAIN2070
MAIN2080
MAIN2090
MAIN2100
MAIN2110
MAIN2120
MAIN2130
MAIN2140
MAIN2150

```



```

C      MAIN2160
C      MAIN2170
C      MAIN2180
C      MAIN2190
C      MAIN2200
C      MAIN2210
C      MAIN2220
C      MAIN2230
C      MAIN2240
C      MAIN2250
C      MAIN2260
C      MAIN2270
C      MAIN2280
C      MAIN2290
C      MAIN2300
C      MAIN2310
C      MAIN2320
C      MAIN2330
C      MAIN2340
C      MAIN2350
C      MAIN2360
C      MAIN2370
C      MAIN2380
C      MAIN2390
C      MAIN2400
C      MAIN2410
C      MAIN2420
C      MAIN2430
C      MAIN2440
C      MAIN2450
C      MAIN2460
C      MAIN2470

2-D CASES, CALCULATE UNSTRETCHED COORDINATES AND CURVATURE ARRAYS
ANG=BODANG
CSORW=1.D0
IF (RW.GT.1.D-06) CSORW=DCOS(ANG)/RW
IF (RW.LT.1.D-06.AND.XKFAC.GT.1.D-05.AND.K.NE.1) CSORW=DCOS(ANG)
DO 150 N=2,IE
  RCRW(N)=RCRW(1)
  RGRWSQ(N)=RGRWSQ(1)
  YY(N)=Y(N)*EPSVD
  RTVC(N)=RW
C
GENERAL TRANSVERSE CURVATURE CASES, CALCULATE STRETCHED AND
UNSTRETCHED COORDINATES AND CURVATURE ARRAYS.
IF (TVC.NE.YES) GO TO 150
YY(N)=(-1.DO+SQRT(1.DO+2.DO*EPSVD*Y(N)*CSORW))/CSORW
IF (RW.LE.1.D-08.AND.K.GT.1) YY(N)=DSQRT(EPSVD*2.DO*Y(N))
ROUM=RD+RDD*YY(N)*CSORW
RTVC(N)=RT*RDUM
RGRW(N)=RDUM/RDDD
RGRWSQ(N)=RORW(N)**2
Y(N)=YY(N)/EPSVD
CONTINUE
150
C
C      BEGIN ITERATION LOOP
C
F2N1=F2N(1)
CALL MCMNT
VC(1)=0.
DO 170 N=2,IE
  VC(N)=VC(N-1)-(XI2*(FCP(N)+FCP(N-1))+FC(N)+FC(N-1))*DN(N-1)*.5
170

```

```

180  AIB=CRNI*F2N(1)+CCRNI*FIN(1)
190  IF (PNC.LT.1.0E-8) GO TO 190
      CFOLD=CF
      CF=2.0*UE*AIR/PNC
      IF (RW.LT.1.D-08) CF=0.00
      IF (CF.GE.0.0) GO TO 180
      WRITE (6,300) CF,UE,AIR,PNC
      CF=CFOLD
      CONTINUE
      CCNTINUE
      NIT=NIT+1
      NITTOT=NITTOT+1
      ISTOP=ISTOP+1
      IF (ISTOP.GT.100) GO TO 290
      IF (K.EQ.1) GO TO 210
      IF (NIT.LT.NIT3) GO TO 210
      IF (DIF.LE.CONVRG) GO TO 210
      WRITE (6,310) NIT,DX,X
      WRITE (6,320) F2N(1),F2N1,DIF
      IPRIM=IPR(11-1)
      IF (XSTA(IPRIM).EQ.0.000) GO TO 200
      IF (ABS(1.-X/XSTA(IPRIM)).LE.1.E-6) II=11-1
      CONTINUE
200  IF TOO MANY ITERATIONS AT X, GO BACK TO PREVIOUS X AND CUT DX
      IN HALF, AND CONTINUE
      C
      C
      C
      C
      X=XOLD+DX/2.0
      DX=DX/2.0
      NIT=0
      IWRTH=0
      CALL DELTAS
      MAIN2480
      MAIN2490
      MAIN2500
      MAIN2510
      MAIN2520
      MAIN2530
      MAIN2540
      MAIN2550
      MAIN2560
      MAIN2570
      MAIN2580
      MAIN2590
      MAIN2600
      MAIN2610
      MAIN2620
      MAIN2630
      MAIN2640
      MAIN2650
      MAIN2660
      MAIN2670
      MAIN2680
      MAIN2690
      MAIN2700
      MAIN2710
      MAIN2720
      MAIN2730
      MAIN2740
      MAIN2750
      MAIN2760
      MAIN2770
      MAIN2780
      MAIN2790

```





```

C      SAVE CURRENT VALUES AND SOLUTIONS FOR USE IN NEXT ITERATION
C
      XOLD=X
      XIOLD=XI
      DXIOLD=DX
      CALL CHANGE
      DO 250 N=1,IE
      F1(N)=F2(N)
      F1N(N)=F2N(N)
      F1NN(N)=F2NN(N)
      CONTINUE
250
C
      RESET COUNTERS
C
      NIT=0
      ISTOP=0
      IF (KSTOP.EQ.1) GO TO 260
      FIVE TRANSFORMED COORDINATES OF NEX
C
      CALL DELTAS
      UER02=UE
      IF (XJFAC.GT.1.D-04) UER02=UE*R0**2
      IF (XKFAC.GT.1.D-04) UER02=UE**3
      CFL=2.00*UE*A1B/PNC*EPSVD*DCOS(BODANG)
      CONTINUE
260
      KMX1=K+10
      IF (KSTOP.EQ.0) GO TO 270
      WRITE (6,330)
      WRITE (6,330)
      GO TO 280
      CONTINUE
270

```

```

MAIN3120
MAIN3130
MAIN3140
MAIN3150
MAIN3160
MAIN3170
MAIN3180
MAIN3190
MAIN3200
MAIN3210
MAIN3220
MAIN3230
MAIN3240
MAIN3250
MAIN3260
MAIN3270
MAIN3280
MAIN3290
MAIN3300
MAIN3310
MAIN3320
MAIN3330
MAIN3340
MAIN3350
MAIN3360
MAIN3370
MAIN3380
MAIN3390
MAIN3400
MAIN3410
MAIN3420
MAIN3430

```

```

280      WRITE (6,340)
290      WRITE (6,340)
300      CONTINUE
310      STOP
320      WRITE (6,350)
330      STUP
340      C
350      C
360      C
370      FORMAT (1H0,16HCF, UE, A1B, PNC/4E15.6///)
380      FORMAT (1H0,///6H NIT=,15.5H DX=,E14.6,4H X=,E14.6/)
390      FORMAT (9H F2N(1)=,1PE14.6,7H F2N1=,E14.6,6H DIF=,E14.6///)
400      FORMAT (1H1,///50X,9H THE END ,14H X=XSTA(11MAX))
410      FORMAT (1H1,///50X,9H THE END ,7H K=KEND)
420      FORMAT (25H STOP *** ISTOP.GT.100//)
430      END

```

```

MAIN3440
MAIN3450
MAIN3460
MAIN3470
MAIN3480
MAIN3490
MAIN3500
MAIN3510
MAIN3520
MAIN3530
MAIN3540
MAIN3550
MAIN3560
MAIN3570
MAIN3580
MAIN3590

```

```

SUBROUTINE ADDETA (SUBTST)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE ADDETA CALLS SUBROUTINES INTER3 AND DERIV3.

SUBROUTINE ADDETA IS CALLED BY MAIN.

SUBROUTINE ADDETA INCREASES ETAINF IF F(IE) AND F(IE-4) DIFFER BY
MORE THAN ADTEST.
GENERATES NEW ETA SPACING AND INTERPOLATES FOR NEW VELOCITY
PROFILE.

COMMON /ARRAY1/ AOR(101),AORP(101),A1(101),A2(101),A3(101),A4(101),
1,CHI(101),DN(102),DN2(102),EPSU(101),EPSPL(101),F1(101),F1N(101),FADDO
2INN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(101),
3OI),XN(102),XN2(102),Y(101),YCVDEL(101),YOVTH(101),YY(101)
COMMON /COMMON1/ A1B,E1,FF,F2N1,VM
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,X1,XI2,XIOLD
1,XJ,XJFAC,Z,ZGL,RO
COMMON /INTGR/ IF,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITADDO
13,NOSE
COMMON /NTEGER/ I1,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,LADDO
1AMTRB,NITIGT
COMMON /NMLCRD/ ADTEST,ETAINF,XKETA

FLCAT(M)=DFLCAT(M)

INCREASE OR DECREASE ETAINF, DEPENDING ON TEST-SUBTST

IF (SUBTST.EQ.2.0D0) GO TO 10
WRITE (6,80) ISTOP,K

```



```

ETA1N2=ETA1NF+.1D0*ETA1NF
GO TO 20
WRITE (6,100) ISTOP,K
ETA1N2=ETA1NF-0.1D0*ETA1NF
C
C
C
CALCULATE NEW ETA PROFILE
C
C
C
20
CONTINUE
IF (XKETA.EQ.1.0) DETAI=ETA1N2/FLGAT(IE-1)
IF (XKETA.NE.1.0) DETAI=ETA1N2*(XKETA-1.0)/(XKETA**IM-1.0)
DN2(1)=DETAI
XN2(1)=0.0
DO 30 N=1,IE
DN2(N+1)=DN2(N)*XKETA
XN2(N+1)=XN2(N)+DN2(N)
CONTINUE
30
DC 60 N=1,IE
IF (XN2(N).GE.ETA1NF) GO TO 50
JC=0
JC=JC+1
IF (XN2(N).GT.XN(JC)) GO TO 40
IF (JC.LT.2) JC=2
IF (JC.GT.(IE-1)) JC=IE-1
CALL INTER3 (XN2(N),XN(JC-1),XN(JC),XN(JC+1),F1(JC),F1(JC+1),F2(N))
1+1),F2(N))
GO TO 60
F2(N)=1.0
60
CONTINUE
C
C
C
INTERPOLATE OLD SOLUTION TO NEW ETA GRID FOR 1ST GUESS ON CURRENT SOLUTION
C
C
C

```

```

C      CALL DERIV3 (F2,XN2,IE,1,F2N)
C      CALL DERIV3 (F2N,XN2,IE,1,F2NN)
C      VC(1)=VM
C
C      PUT NEW GRIDS AND PROFILES INTO WORKING ARRAYS
C
C      DO 70 N=1,IE
C      DN(N)=DN2(N)
C      XN(N)=XN2(N)
C      F1(N)=F2(N)
C      FIN(N)=F2N(N)
C      F1NN(N)=F2NN(N)
C      FC(N)=F1(N)
C      FCN(N)=FIN(N)
C      FCP(N)=0.0
C      IF (N.EQ.1) GO TO 70
C      VC(N)=VC(N-1)-(F2(N)+F2(N-1))*DN(N-1)*0.50
C      CONTINUE
C      ETAINF=ETAIN2
C      WRITE (6,90) DX,XKETA,ETAINF,ADTEST,X
C      RETURN
C
C      FORMAT (1H0,9X,42HINTERMEDIATE PROFILE DATA-ETAINF INCREASED,2X,6HADD0 890
C      11STOP=,13,3H K=,13)
C      FORMAT (1H0,2X,3HDX=,F12.6,1X,6HXKETA=,F12.6,1X,7HETAINF=,F12.6,1XADD0 910
C      1,7HADTEST=,F12.6,1X,2HX=,F12.6)
C      FORMAT (1H0,9X,42HINTERMEDIATE PROFILE DATA-ETAINF DECREASED,2X,6HADD0 930
C      11STOP=,13,3H K=,13)
C      END
C
C      70
C
C      90
C
C      100

```

```

SUBROUTINE BLUNT1
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE BLUNT1 CALLS SUBROUTINE FD5.

SUBROUTINE BLUNT1 IS CALLED BY SUBROUTINE GEOM.

SUBROUTINE BLUNT1 CALCULATES THE EDGE AND REFERENCE PROPERTIES
FOR THE STAGNATION POINT OF A BLUNT BODY.

COMMON /ARRAY2/ PZ(501),UFZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(101),RZ(501)
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,USERO2,UESO
COMMON /FRSTRM/ PFS,REINF,RHOF,UF5
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXCLOD,PNC,REFLEN,SCF,X,XI,XI2,XIOLDBLAO
1,XJ,XJFAC,Z,ZOL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITBLAO
13,NOSE
COMMON /REF/ PREF,RHOREF,UREF
COMMON /STAG/ P10,PSTAG
COMMON /VSCSTY/ EPSVD,XK1,XK2
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RCRW(101),ROPWSQ(101),RW
COMMON /WAK/ XKFAC

ALOG10(X)=DLOG10(X)
SQRT(X)=DSQRT(X)

P10=PSTAG/(RHOF*UF5*UF5)
DO 10 J=1,IIMAX
PZ(J)=PZ(J)*P10

```

BLAO 10  
BLAO 20  
BLAO 30  
BLAO 40  
BLAO 50  
BLAO 60  
BLAO 70  
BLAO 80  
BLAO 90  
BLAO 100  
BLAO 110  
BLAO 120  
BLAO 130  
BLAO 140  
BLAO 150  
BLAO 160  
BLAO 170  
BLAO 180  
BLAO 190  
BLAO 200  
BLAO 210  
BLAO 220  
BLAO 230  
BLAO 240  
BLAO 250  
BLAO 260  
BLAO 270  
BLAO 280  
BLAO 290  
BLAO 300  
BLAO 310  
BLAO 320



```

10      UEZ(J)=SQRT(2.*(P10-PZ(J)))
        CONTINUE
        BODANG=DARCOS(-1.000)/2.000
        Z=ZA(1)
        RO=0.0
        PE=P10
        UE=0.0
        PP=0.0
        C
        C      FIND STAGNATION POINT EDGE VELOCITY GRADIENT BY INTERPOLATION AND
        C      REFLECTION AROUND THE CPIGIN
        C
        CALL FD5 (X,-XSTA(3),-XSTA(2),XSTA(1),XSTA(2),XSTA(3),-UEZ(3),-UEZ(3),-UEZ(3),-UEZ(3))
        I(2),UEZ(1),UEZ(2),UEZ(3),DUEDS)
        UERJ2=0.0
        PNC=SQRT((XKFAC+1.00)/((XJFAC+1.00)*DUEDS))
        BETA=0.500
        PESQ=PE
        WRITE (6,20) P10
        WRITE (6,30) UE,PE
        RETURN
        C
        C
        C      20      FORMAT (1H ,2X,4HP10=,D15.7)
        C      30      FORMAT (9H      UESQ= ,D15.7,9H      PESQ= ,D15.7)
        C      END

```

```

BLAO 330
BLAO 340
BLAO 350
BLAO 360
BLAO 370
BLAO 380
BLAO 390
BLAO 400
BLAO 410
BLAO 420
BLAO 430
BLAO 440
BLAO 450
BLAO 460
BLAO 470
BLAO 480
BLAO 490
BLAO 500
BLAO 510
BLAO 520
BLAO 530
BLAO 540
BLAO 550
BLAO 560
BLAO 570
BLAO 580

```

```

SUBROUTINE BLUNT2 (IFLAG)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE BLUNT2 CALLS SUBROUTINES FD5, INTER5 AND ZR0

SUBROUTINE BLUNT2 IS CALLED BY SUBROUTINE EGPROP.

SUBROUTINE BLUNT2 CALCULATES THE EDGE PROPERTIES FOR A BLUNT BODY
AT THE VALUES OF X AFTER THE INITIAL VALUE OF X.

COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(
101),RZ(501)
COMMON /EDUPRP/ BETA,DUEDS,PE,PESO,PP,UE,UEO2,UESO
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXLDD,PNC,REFLEN,SCF,X,XI,XI2,XIOLD
1,XJ,XJFAC,Z,ZOL,R0
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITBL
13,NJSE
COMMON /STAG/ P10,PSTAG
COMMON /VSCSTY/ EPSVD,XK1,XK2
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RCRW(101),RORWSQ(101),RW
COMMON /DRAG/ CDV1,CDV2,XCP,XCP1,CP(501),CP1(501)
COMMON /HESS/ IWH,ICARD2,ICARD3,ICARD4,NN,IBDN,HEDR(10),CASE,KHES
15
SQRT(X)=DSQRT(X)

IF (X.LT.XSTA(3)) GO TO 30
J=0
J=J+1
IF (X.GT.XSTA(J)) GO TO 10

```

```

C
C
C
IF (J.LT.3) J=3
IF (J.GT.(IIMAX-2)) J=IIMAX-2
FIND PROPERTIES IF PAST THE THIRD STATION
CALL ZRO (IIMAX,X,Z,RO)
IF (RO.LT.0.00) RO=0.00
CALL FDS (Z,ZA(J-2),ZA(J-1),ZA(J),ZA(J+1),ZA(J+2),RZ(J-2),RZ(J-1),RZ(J),RZ(J+1),RZ(J+2),TANBOD)
BCDANG=DATAN(TANBOD)
CALL INTER5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),PZ(J-2),PZ(J-1),PZ(J),PZ(J+1),PZ(J+2),PE)
UE=SQRT(2.*(PI0-PE))
CALL FDS (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),UEZ(J-2),UEZ(J-1),UEZ(J),UEZ(J+1),UEZ(J+2),DUEDS)
IF (IFLAG.EQ.0) GO TO 20
IF (KHESS.EQ.0) GO TO 20
CALL INTER5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),CP(J-2),CP(J-1),CP(J),CP(J+1),CP(J+2),XCP)
CALL INTER5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),CPI(J-2),CPI(J-1),CPI(J),CPI(J+1),CPI(J+2),XCPI)
CONTINUE
PP=-UE*DUEDS
RETURN
CONTINUE
CALL ZRO (IIMAX,X,Z,RO)
CALL FDS (Z,ZA(1),ZA(2),ZA(3),ZA(4),ZA(5),RZ(1),RZ(2),RZ(3),RZ(4),RZ(5),TANBOD)
BCDANG=DATAN(TANBOD)
CALL INTER5 (X,-XSTA(3),-XSTA(2),XSTA(1),XSTA(2),XSTA(3),PZ(1),PZ(2),PZ(3),PE)
CALL FDS (X,-XSTA(3),-XSTA(2),XSTA(1),XSTA(2),XSTA(3),-UEZ(3),-UEZ(2),-UEZ(1),-UEZ(3),-UEZ(2),-UEZ(1))

```

20

30

```

BLBO 330
BLBO 340
BLBO 350
BLBO 360
BLBO 370
BLBO 380
BLBO 390
BLBO 400
BLBO 410
BLBO 420
BLBO 430
BLBO 440
BLBO 450
BLBO 460
BLBO 470
BLBO 480
BLBO 490
BLBO 500
BLBO 510
BLBO 520
BLBO 530
BLBO 540
BLBO 550
BLBO 560
BLBO 570
BLBO 580
BLBO 590
BLBO 600
BLBO 610
BLBO 620
BLBO 630
BLBO 640

```



```

1(2),UEZ(1),UEZ(2),UEZ(3),DUEDS)      BLB0 650
IF (IFLAG.EQ.0) GO TO 40                BLB0 660
IF (KHES.EQ.0) GO TO 40                 BLB0 670
CALL INTER5 (X,-XSTA(3),-XSTA(2),XSTA(1),XSTA(2),XSTA(3),CP(3),CP(BLB0 680
12),CP(1),CP(2),CP(3),XCP)              BLB0 690
CALL INTER5 (X,-XSTA(3),-XSTA(2),XSTA(1),XSTA(2),XSTA(3),CP(3),CP(BLB0 700
11(2),CP(1),CP(2),CP(3),XCPI)          BLB0 710
UE=SQRT(2.*(PI0-PE))                   BLB0 720
GO TO 20                                BLB0 730
END                                       BLB0 740

```

40

```

SUBROUTINE CHANGE
  IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE CHANGE IS CALLED BY MAIN.

SUBROUTINE CHANGE ADJUSTS THE X STEP SIZE IF NECESSARY TO OBTAIN
  A SOLUTION AT A SPECIFIED VALUE OF X.
  WHEN INSTANTANEOUS TRANSITION IS TO BE CALCULATED, THIS SUBROUTINE CHANGES
  THE SOLUTION PROCEDURE FROM LAMINAR TO TURBULENT AND
  RESETS DELTA X.
  THIS SUBROUTINE DOUBLES/HALVES THE X STEP SIZE IF NIT IS LESS THAN
  NIT2 OR GREATER THAN NIT1 RESPECTIVELY. DX CAN NEVER BE SET
  GREATER THAN DXMAX.

COMMON /ARRAY1/ A08(101),A08P(101),A1(101),A2(101),A3(101),A4(101),A5(101),
1,CHI(101),DN(102),DN2(102),EPSG(101),EPSPL(101),F1(101),F1N(101),F2(101),
21NN(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(101),VCN(101),
301),XN(102),XN2(102),Y(101),YCVDEL(101),YCVHT(101),YY(101)
COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(101),
1101),RZ(501)
COMMON /GEOME/ OS,DX,DX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLD
1,XJ,XJFAC,Z,ZCL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITCHAO
13,NOSE
COMMON /NTEGER/ II,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTCP,KTRNSN,L
1AMTRB,NITTOT
COMMON /TRANS/ ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS,KONSET
COMMON /TE/ KTE,KTSTIE
COMMON /HESS/ IWRTH

  ABS(X)=DABS(X)

```

CHAO 10  
CHAO 20  
CHAO 30  
CHAO 40  
CHAO 50  
CHAO 60  
CHAO 70  
CHAO 80  
CHAO 90  
CHAO 100  
CHAO 110  
CHAO 120  
CHAO 130  
CHAO 140  
CHAO 150  
CHAO 160  
CHAO 170  
CHAO 180  
CHAO 190  
CHAO 200  
CHAO 210  
CHAO 220  
CHAO 230  
CHAO 240  
CHAO 250  
CHAO 260  
CHAO 270  
CHAO 280  
CHAO 290  
CHAO 300  
CHAO 310  
CHAO 320

C  
C





```
C      C      C
ADJUST DX TO SOLVE AT IPR STATIONS

DC 70 IF=1,IPRINT
IF (XSTA(IPR(III)).LE.X) GO TO 70
IF (XSTA(IPR(III)).GT.(X+1.25D0*DX)) GO TC 60
SET FINAL VALJE
DX=XSTA(IPR(II))-X
X=XSTA(IPR(II))
IWRTH=1
GO TO 80
X=X+DX
GO TO 80
CONTINUE
LAST STATION SOLVED, TERMINATE RUN
KSTOP=1
RETURN
DXOLD=DX
XOLD=X

C      C      C
CHECK IF INSTANTANEOUS TRANSITION

IF (KTRNSN.EQ.IIMAX) GO TC 90
IF (X.LT.XSTA(KTRNSN)) GO TC 90
GAMMA=1.D0
LAMTB=2
CONTINUE
IF (KTE.EQ.IIMAX) GO TC 100
IF (X.LE.XSTA(KTE)) GO TC 100
KTSTF=1
CONTINUE
RETURN

90      100
```

CHAO 970  
CHAO 980  
CHAO 990

C  
110 FCRMAT (1H0,24HQUITTING DUE TC SMALL DX)  
END

```

SUBROUTINE COEF
  IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE COEF CALLS SUBROUTINE INTERP.

SUBROUTINE COEF IS CALLED BY MAIN.

SUBROUTINE COEF COMPUTES FLOW COEFFICIENTS SUCH AS SKIN FRICTION
  COEFFICIENT, ETC.
  ALSO COMPUTES DELTA, THETA, AND DELTA*.

COMMON /ARRAY1/ AOB(101),AOBP(101),AI(101),A2(101),A3(101),A4(101)
1,CHI(101),DN(102),DN2(102),EPSO(101),EPSPL(101),F1(101),FIN(101),FCOE
21,N(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(10
301),XN(102),XN2(102),Y(101),YOVDEL(101),YOVTH(101),YY(101)
COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(COE
1101),RZ(501)
COMMON /COEFF/ CFBAR,CFBREX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,COE
1DSTARK,DSTARX,HAFCF,RETHET,REX,THET
COMMON /COEFF2/ DELCRF,DELOX,DSAXOR,DSTCDL,DSTORF,DSTGTH,DSTOX,RLRCOE
1EFL,THODEL,THOREF,XOREFL,ZOREFL
COMMON /COEFF3/ CF1,SUM,SUM1,SUMT
COMMON /COMWLL/ A1B,E1,FF,F2N1,VM
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UER02,UES0
COMMON /FRSTRM/ PFS,REINF,RHOF,S,UFS
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,XI,XI2,XICLDCOE
1,XJ,XJFAC,Z,ZOL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITCOE
13,NUSE
COMMON /NIEGER/ II,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,LCOE
1AMTRB,NITTOT

```

COE0 10  
COE0 20  
COE0 30  
COE0 40  
COE0 50  
COE0 60  
COE0 70  
COE0 80  
COE0 90  
COE0 100  
COE0 110  
COE0 120  
COE0 130  
COE0 140  
COE0 150  
COE0 160  
COE0 170  
COE0 180  
COE0 190  
COE0 200  
COE0 210  
COE0 220  
COE0 230  
COE0 240  
COE0 250  
COE0 260  
COE0 270  
COE0 280  
COE0 290  
COE0 300  
COE0 310  
COE0 320



```

COMMON /TRANS/ ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS,KONSET
COMMON /VSCSTY/ EPSVD,XK1,XK2
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RCRW(101),RORWSQ(101),RW
COMMON /LWALL/ UCUPLS(101),YPLUS(101),UDEF(101),UPLUS
COMMON /TE/ KTE,KTSTTE
COMMON /DRAG/ CDVL,CDV2,XCP,XCPL,CP(501),CPI(501),ROMAX
COMMON /STAG/ P10,PSTAG,RHO
COMMON /WKPRL/ RSTAR
COMMON /HESS/ IWITH,ICARD2,ICARD3,ICARD4,NN,I8DN,HEDR(10),CASE,KHESCOF0
1S
DATA YES/3HYES/
DIMENSION FD(101)

SORT(X)=DSQRT(X)

IF (X.EQ.XSTA(1)) GO TO 60

PI=DARCOS(-1.D0)

RESE=UE*X
REX=REINF*RESF
SOREX=SQRT(REX)
CFRES=CF*SQREX
CFE=CF*EPSVD/(UE*UE)
CFINF=CF*EPSVD
CFRFY=CFRES*EPSVD
IF (X.EQ.0.0) GO TO 20
CALL INTERP (0.995D0,FC,Y,IE,DELTA)
DO 10 I=1,IE
YUDEL(I)=Y(I)/DELTA

```

```

COE0 330
COE0 340
COE0 350
COE0 360
COE0 370
COE0 380
COE0 390
COE0 400
COE0 410
COE0 420
COE0 430
COE0 440
COE0 450
COE0 460
COE0 470
COE0 480
COE0 490
COE0 500
COE0 510
COE0 520
COE0 530
COE0 540
COE0 550
COE0 560
COE0 570
COE0 580
COE0 590
COE0 600
COE0 610
COE0 620
COE0 630
COE0 640

```

C  
C  
C  
C  
C  
C

```

10 CONTINUE
20 CONTINUE
C
C
C      AVG. CF=SQRT(REX)
C
C      IF (K.EQ.1) GO TO 30
C      IF (KTSTTE.GT.0) GO TO 40
C      CF=REX=.2*.5*ALB
C      CF2=CF*INF*DCOS(BODANG)
C
C      CALCULATE INCREMENTAL SKIN DRAG DUE TO DX
C
C      DSUM=0.50*DX*(CF2+CF1)
C
C      RUNNING SUM OF SKIN DRAG
C
C      SUM=SUM+DSUM
C      CF=REX=SUM/X*SQREX
C      IF (KHESS.EQ.0) GO TO 30
C      REFA=PI*ROMAX**2
C      C=4.0*PI/UFS**2/REFA/RHO
C      CDV2=C*(XCP-XCP1)*RO*DSIN(BODANG)
C
C      CALCULATE INCREMENTAL PRESSURE DRAG
C
C      DSUM1=0.5*DX*(CDV1+CDV2)
C
C      RUNNING SUM OF PRESSURE DPAG
C
C      SUM1=SUM1+DSUM1
C      CDV1=CDV2
C      SUMT=SUM+SUM1

```

COE0 650  
COE0 660  
COE0 670  
COE0 680  
COE0 690  
COE0 700  
COE0 710  
COE0 720  
COE0 730  
COE0 740  
COE0 750  
COE0 760  
COE0 770  
COE0 780  
COE0 790  
COE0 800  
COE0 810  
COE0 820  
COE0 830  
COE0 840  
COE0 850  
COE0 860  
COE0 870  
COE0 880  
COE0 890  
COE0 900  
COE0 910  
COE0 920  
COE0 930  
COE0 940  
COE0 950  
COE0 960

```

30      CONTINUE
      HAFCF=CF*EPSVD/2.0
      IF (X.EQ.0.0) GO TO 40
      CFBAR=CFBREX/SQREX
      CONTINUE
40      C
      C
      C      CALCULATE MUMENTUM THICKNESS
      THET=0.0
      DO 50 I=2,IE
      FAC1=FC(I)*(1.000-FC(I))
      FAC2=FC(I-1)*(1.000-FC(I-1))
      THET=THET+0.500*(FAC1+FAC2)*DN(I-1)*PNC*EPSVD
      CONTINUE
      FASANG=BODANG
50      C
      C
      C      THETA FOR TRANSVERSE CURVATURE CASE FOR A 0.0 OR FINITE WALL RADIUS
      IF (TVC.EQ.YES.AND.RW.GT.1.0-08) THET=RW/DCOS(FASANG)*(-1.000+DSQRCOE01150
      1Y(1.000+2.000*DCOS(FASANG)*THET/RW))
      IF (TVC.EQ.YES.AND.RW.LE.1.0-08) THET=DSQRT(2.00*THET)
      DELST=0.0
60      C
      C
      C      INTEGRATE TO FIND THE DISPLACEMENT THICKNESS
      DO 70 I=2,IE
      FAC1=1.00-FC(I)
      FAC2=1.00-FC(I-1)
      DELST=DELST+0.500*(FAC1+FAC2)*DN(I-1)*PNC*EPSVD
      CONTINUE
      IF (TVC.EQ.YES.AND.RW.GT.1.0-08) DELST=RW/DCOS(FASANG)*(-1.000+DSQRCOE01270
      1Y(1.000+2.000*DCOS(FASANG)*DELST/RW))
70      C
      C
      C

```

COE0 970  
 CCE0 980  
 CUE0 990  
 COE01000  
 COE01010  
 CCE01020  
 COE01030  
 CCE01040  
 CCE01050  
 CCE01060  
 CCE01070  
 CCE01080  
 CCE01090  
 CCE01100  
 CCE01110  
 CCE01120  
 CCE01130  
 CCE01140  
 CCE01150  
 CCE01160  
 CCE01170  
 CCE01180  
 CCE01190  
 CCE01200  
 CCE01210  
 CCE01220  
 CCE01230  
 CCE01240  
 CCE01250  
 CCE01260  
 CCE01270  
 CCE01280



```

C
C
C
      IF (TVC.EQ.YES.AND.RW.LE.1.D-08) DELST=DSQRT(2.D0*DELST)
      IF (X.EQ.XSTA(1)) RETURN

      CALCULATE PRINTED BOUNDARY LAYER QUANTITIES

      RETHET=UE*THET/(EPSVD*EPSVD)
      DEL=DELTA*EPSVD
      ROREFL=R0/REFLEN
      XOREFL=X/REFLEN
      THOREF=THET/REFLEN
      DSTJRF=DELST/REFLEN
      DSTOX=DELST/X
      DELOX=DEL/X
      DELORF=DEL/REFLEN
      IF (XJFAC.NE.0.0) DSTRAX=F0*(SQRT(1.0+2.0*DELST/R0)-1.0)
      IF (TVC.EQ.YES) DSTRAX=DELST
      IF (XJFAC.EQ.0.0) DSTRAX=0.0
      ZOREFL=Z/REFLEN
      THODEL=THET/DEL
      DSTOOL=DELST/DEL
      DSTOTH=DELST/THET
      DSAXOR=DSTRAX/REFLEN
      DO 80 N=1,IE
      YDVTHT(N)=YY(N)/THET
      IF (KTSTTE.GT.0) GO TO 100
      UPLUS=SQRT(UE*EPSVD*DABS(A1B)/PNC)
      DO 90 I=1,IE
      UCUPLS(I)=FC(I)/UPLUS*UE
      YPLUS(I)=YY(I)*UPLUS/EPSVD**2
      UDEF(I)=UE*(FC(I)-1.D0)/UPLUS
      CONTINUE
      CONTINUE
80
90
100

```

```

COE01290
COE01300
COE01310
COE01320
COE01330
COE01340
COE01350
COE01360
COE01370
COE01380
COE01390
COE01400
COE01410
COE01420
COE01430
COE01440
COE01450
COE01460
COE01470
COE01480
COE01490
COE01500
COE01510
COE01520
COE01530
COE01540
COE01550
COE01560
COE01570
COE01580
COE01590
COE01600

```

COE01610  
 COE01620  
 COE01630  
 COE01640  
 COE01650  
 COE01660  
 COE01670  
 COE01680  
 COE01690  
 COE01700  
 COE01710  
 COE01720  
 COE01730  
 COE01740  
 COE01750

```

VCRT=DSQRT(2.D0*X1)/UE/DELTA
THETA=80DANG
RDEL=RO+DELTA*DCOS(THETA)
ZDEL=Z-DELTA*DSIN(THETA)
WRITE (22,120) VCRT,Z,RO,ZDEL,RDEL,DELTA,THETA
IF (KTSTTE.LT.1) RETURN
BIGUD=1.D0-FC(1)
DO 110 I=1,IE
  FD(1)=1.D0-FC(1)
  FD(1)=FD(1)/BIGUD
  CALL INTERP (0.5D0,FD,YY,IE,RSTAR)
  RETURN
110
C
120  FORMAT (7E15.6)
      END

```

```

SUBROUTINE CONE1
  IMPLICIT REAL*8(A-H,O-Z)

  SUBROUTINE CGNE1 CALLS SUBROUTINES FDS, INTER5 AND ZRO.

  SUBROUTINE CONE1 IS CALLED BY SUBROUTINE GEOM.

  SUBROUTINE CONE1 CALCULATES THE EDGE AND REFERENCE PROPERTIES FOR
  THE FIRST CALCULATED POINT ON A SHARP NCSE BODY.

  COMMON /ARPAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(
1101),RZ(501)
  COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITCCA
13,NOSE
  COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UERO2,UESO
  COMMON /FRSTPM/ PFS,REINF,RHOF5,UFS
  COMMON /GEGME/ DS,DX,DX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLDCCA
1,XJ,XJFAC,Z,ZOL,F0
  COMMON /REF/ PREP,RHOREF,UREF
  COMMON /STAG/ P10,PSTAG
  COMMON /VSCSTV/ EPSVD,XK1,XK2
  COMMON /STAG4/ UECN,PECN
  COMMON /TVCURV/ TVC,BODANG,PTVC(101),RORW(101),RORWSQ(101),RW

  SIN(X)=DSIN(X)
  SQRT(X)=DSQRT(X)

  P10=PSTAG/(RHOF5*UFS*UFS)
  DO 10 J=1,IIMAX
    PZ(J)=PZ(J)*P10
    UEZ(J)=DSQRT(2.00*(P10-PZ(J)))

```

```

CCAO 10
CCAO 20
CCAO 30
CCAO 40
CCAO 50
CCAO 60
CCAO 70
CCAO 80
CCAO 90
CCAO 100
CCAO 110
CCAO 120
CCAO 130
CCAO 140
CCAO 150
CCAO 160
CCAO 170
CCAO 180
CCAO 190
CCAO 200
CCAO 210
CCAO 220
CCAO 230
CCAO 240
CCAO 250
CCAO 260
CCAO 270
CCAO 280
CCAO 290
CCAO 300
CCAO 310
CCAO 320

```



```

10  CONTINUE
    CALL ZR0 (IIMAX,X,Z,R0)
    IF (R0.LT.0.00) R0=0.00
    CALL FD5 (Z,ZA(1),ZA(2),ZA(3),ZA(4),ZA(5),RZ(1),RZ(2),RZ(3),RZ(4),
    1RZ(5),TANBOD)
    BUDANG=DATAN(TANBOD)
    CALL INTER5 (X,XSTA(1),XSTA(2),XSTA(3),XSTA(4),XSTA(5),PZ(1),PZ(2),
    1,PZ(3),PZ(4),PZ(5),PE)
    CALL FD5 (X,XSTA(1),XSTA(2),XSTA(3),XSTA(4),XSTA(5),UEZ(1),UEZ(2),
    1UEZ(3),UEZ(4),UEZ(5),DUEDS)
    UE=SQRT(2.*(P10-PE))
    RETURN
    END
    CCA0 330
    CDA0 340
    CCA0 350
    CDA0 360
    CCA0 370
    CDA0 380
    CCA0 390
    CDA0 400
    CCA0 410
    CDA0 420
    CCA0 430
    CDA0 440
    CCA0 450

```

```

C      SUBROUTINE CONE2 (IFLAG)
C      IMPLICIT REAL*8(A-H,O-Z)
C
C      SUBROUTINE CONE2 CALLS SUBROUTINES FD5, INTER5 AND ZRO.
C
C      SUBROUTINE CONE2 IS CALLED BY SUBROUTINE EGPROP.
C
C      SUBROUTINE CONE2 CALCULATES THE EDGE PROPERTIES FOR A SHARP NOSE
C      BODY AT THE VALUES OF X AFTER THE INITIAL VALUE OF X.
C
C      COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(COBO 10
C      1101),RZ(501)
C      COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITCOBO 20
C      13,NOSE
C      COMMON /STAG/ P10,PSTAG
C      COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UEO2,UESO
C      COMMON /GEOME/ DS,DX,DX1,DXMAX,DXCLD,PNC,REFLEN,SCF,X,X1,XI2,XIOLDCOBO 30
C      1,XJ,XJFAC,Z,ZOL,RO
C      COMMON /STAG4/ UECN,PECN
C      COMMON /TVCURV/ TVC,BODANG,RTVC(101),RORW(101),RORWSQ(101),RW
C      150
C      COMMON /HESS/ IWRTH,ICARD2,ICARD3,ICARD4,NN,IBDN,HEDR(10),CASE,KHECCOBO 40
C      155
C      COMMON /DRAG/ CDV1,CDV2,XCP,XCP1,CP(501),CP1(501)
C
C      COS(X)=DCOS(X)
C      SQR(X)=DSQRT(X)
C
C      IF (X.LT.XSTA(3)) GO TO 30
C      J=0
C      J=J+1
C
C      COBO 10
C      COBO 20
C      COBO 30
C      COBO 40
C      COBO 50
C      COBO 60
C      COBO 70
C      COBO 80
C      COBO 90
C      COBO 100
C      COBO 110
C      COBO 120
C      COBO 130
C      COBO 140
C      COBO 150
C      COBO 160
C      COBO 170
C      COBO 180
C      COBO 190
C      COBO 200
C      COBO 210
C      COBO 220
C      COBO 230
C      COBO 240
C      COBO 250
C      COBO 260
C      COBO 270
C      COBO 280
C      COBO 290
C      COBO 300
C      COBO 310
C      COBO 320

```

```

IF (X.GT.XSTA(J)) GO TO 10
IF (J.LI.3) J=3
IF (J.GT.(IIMAX-2)) J=IIMAX-2
CALL ZRO (IIMAX,X,Z,RO)
IF (RO.LT.0.00) RO=0.00
CALL FD5 (Z,ZA(J-2),ZA(J-1),ZA(J),ZA(J+1),ZA(J+2),RZ(J-1),RZ(J-2),RZ(J-3),RZ(J-4),RZ(J-5),TANBOD)
BCDANG=DATAN(TANBOD)
CALL INTER5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),PZ(J-2),PZ(J-1),PZ(J),PZ(J+1),PZ(J+2),PE)
UE=SQR(2.*(PI0-PE))
CALL FD5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),UEZ(J-2),UEZ(J-1),UEZ(J),UEZ(J+1),UEZ(J+2),DUEDS)
IF (IFLAG.EQ.0) GO TO 20
IF (KHESS.EQ.0) GO TO 20
CALL INTER5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),CP(J-2),CP(J-1),CP(J),CP(J+1),CP(J+2),XCP)
CALL INTER5 (X,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),CPI(J-2),CPI(J-1),CPI(J),CPI(J+1),CPI(J+2),XCPI)
CONTINUE
PP=-UE*DUEDS
RETURN
CONTINUE
CALL ZRO (IIMAX,X,Z,RO)
CALL FD5 (Z,ZA(1),ZA(2),ZA(3),ZA(4),ZA(5),RZ(1),RZ(2),RZ(3),RZ(4),RZ(5),TANBOD)
BCDANG=DATAN(TANBOD)
CALL INTER5 (X,XSTA(1),XSTA(2),XSTA(3),XSTA(4),XSTA(5),PZ(1),PZ(2),PZ(3),PZ(4),PZ(5),PE)
CALL FD5 (X,XSTA(1),XSTA(2),XSTA(3),XSTA(4),XSTA(5),UEZ(1),UEZ(2),UEZ(3),UEZ(4),UEZ(5),DUEDS)
IF (IFLAG.EQ.0) GO TO 40

```

20

30

COB0 330  
COB0 340  
COB0 350  
COB0 360  
COB0 370  
COB0 380  
COB0 390  
COB0 400  
COB0 410  
COB0 420  
COB0 430  
COB0 440  
COB0 450  
COB0 460  
COB0 470  
COB0 480  
COB0 490  
COB0 500  
COB0 510  
COB0 520  
COB0 530  
COB0 540  
COB0 550  
COB0 560  
COB0 570  
COB0 580  
COB0 590  
COB0 600  
COB0 610  
COB0 620  
COB0 630  
COB0 640



40

```

SUBROUTINE DELTAS
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE DELTAS CALLS SUBROUTINE EGPROP.

SUBROUTINE DELTAS IS CALLED BY MAIN AND SUBROUTINE INIT.

SUBROUTINE DELTAS CALCULATES DS - DELTA XI, THE TRANSFORMATION
FACTOR - PNC, AND THE PRESSURE GRADIENT TERM - BETA.
INTEGRATION BY SIMPSONS RULE IS USED FOR CALCULATING DS.

COMMON /EDGPRP/ BETA, DUEDS, PE, PESO, PP, LE, UERO2, UESO
COMMON /GEOME/ DS, DX, DX1, DXMAX, DXCLD, PNC, REFLEN, SCF, X, XI, XI2, XIOLD
1, XJ, XJFAC, Z, ZOL, RO
COMMON /INTGR/ IE, IIMAX, IM, IPFNT, ISTOP, KL, KVSLOW, NIT, NIT1, NIT2, NITDEL
13, NCSE
COMMON /WAK/ XKFAC
COMMON /INTACT/ BETAS
COMMON /HESS/ IWRTH, ICARD2, ICARD3, ICARD4, NN, IBDN, HEDR(10), CASE, KHEDEL
155

SQRT(X)=DSQRT(X)

HA=X-DX*0.50
XI=X
X=HA
CALL EGPROP (0)
X=XI
CALL EGPROP (1)

```

DELO 10  
DELO 20  
DELO 30  
DELO 40  
DELO 50  
DELO 60  
DELO 70  
DELO 80  
DELO 90  
DELO 100  
DELO 110  
DELO 120  
DELO 130  
DELO 140  
DELO 150  
DELO 160  
DELO 170  
DELO 180  
DELO 190  
DELO 200  
DELO 210  
DELO 220  
DELO 230  
DELO 240  
DELO 250  
DELO 260  
DELO 270  
DELO 280  
DELO 290  
DELO 300  
DELO 310  
DELO 320

```

C      AXISYMETRIC, WAKE CASES
C
  RP=RO
  UEHA=UE
  ROHA=RO
  RPP=RP
  IF (XJFAC.LT.0.0010) GO TO 10
  GO TO 20

C      2-D, NO WAKE CASES
C
C      CONTINUE
C      RP=1.00
C      RPP=RP
C      ROHA=1.00
C      CONTINUE
C      IF (XKFAC.LT.0.0010) GO TO 30
C
C      2-D OR AXISYMETRIC, WITH WAKE
C
C      RP=UE
C      RPP=RO
C      ROHA=UEHA
C      CONTINUE
C      DS=(UERO2+4.*UEHA*ROHA+UE*RP*RP)*CX/6.
C      XI=XICLO+DS
C      XI2=2.00*XI
C      PNC=SQRT(XI2)/UE
C      IF (RPP.GT.1.0-08) PNC=PNC/RPP
C      BETA=XI2*DUEDS/((UE*RP)**2)
C      IF (KHES.EQ.0) RETURN
C      IF (BETA.LT.8FTAS) BETA=BETAS

```

DELO 330  
DELO 340  
DELO 350  
DELO 360  
DELO 370  
DELO 380  
DELO 390  
DELO 400  
DELO 410  
DELO 420  
DELO 430  
DELO 440  
DELO 450  
DELO 460  
DELO 470  
DELO 480  
DELO 490  
DELO 500  
DELO 510  
DELO 520  
DELO 530  
DELO 540  
DELO 550  
DELO 560  
DELO 570  
DELO 580  
DELO 590  
DELO 600  
DELO 610  
DELO 620  
DELO 630  
DELO 640



DELO 650  
DELO 660

RETURN  
END

```

SUBROUTINE DERIV3 (F,X,IMAX,IMIN,FP)
  IMPLICIT REAL*8(A-H,O-Z)

  SUBROUTINE DERIV3 CALLS SUBROUTINE FD3.

  SUBROUTINE DERIV3 IS CALLED BY MAIN AND SUBROUTINES ADDETA, EFFMU
  AND SOLVE.

  SUBROUTINE DERIV3 CALCULATES THE FIRST DERIVATIVES OF F WITH
  RESPECT TO X AND RETURNS THE ARRAY FP.

  DIMENSION F(101), X(102), FP(101)

  DO 10 J=IMIN,IMAX
    K=J
    IF (K.LT.(IMIN+1)) K=IMIN+1
    IF (K.GT.(IMAX-1)) K=IMAX-1
    CALL FD3 (X(J),X(K-1),X(K),X(K+1),F(K-1),F(K),F(K+1),FP(J))
    CONTINUE
  RETURN
END

10

```

```

DERO 10
DERO 20
DERO 30
DERO 40
DERO 50
DERO 60
DERO 70
DERO 80
DERO 90
DERO 100
DERO 110
DERO 120
DERO 130
DERO 140
DERO 150
DERO 160
DERO 170
DERO 180
DERO 190
DERO 200
DERO 210
DERO 220

```

```

SUBROUTINE EFFMU (LAMTRB,II,DLSTRK)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE EFFMU CALLS SUBROUTINES DERIV3 AND INTERP.

SUBROUTINE EFFMU IS CALLED BY SUBROUTINE MGMENT.

CALCULATES THE TERMS AOB AND AOBP WHICH, FOR THE TURBULENT
CASE, INCLUDE THE EDDY VISCOSITY - EPSPL.
FOR THE TRANSITION REGIME, THE EDDY VISCOSITY IS REDUCED BY THE
TRANSITION INTERMITTENCY FACTOR - GAMMA.

COMMON /ARRAY1/ AOB(101),AOBP(101),A1(101),A2(101),A3(101),A4(101)
1,CHI(101),DN(102),DN2(102),EPSQ(101),EPSPL(101),F1(101),FIN(101),FEFFQ
21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(101),VC
301),XN(102),XN2(102),Y(101),YCVDEL(101),YCVTHT(101),YY(101)
COMMON /ARRAY2/ PZ(501),UFZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(
1101),RZ(501)
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,VERO2,UESO
COMMON /GELME/ DS,DX,DX1,DXMAX,DXGLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLDEFFQ
1,XJ,XJFAC,Z,ZOL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITEFFQ
13,NQSE
COMMON /TRANS/ ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS,KONSET
COMMON /VSCSTY/ EPSVD,XK1,XK2
COMMON /COEFF/ CFBAR,CFBEX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,EFFQ
1DSTAR6,DSTARX,HAFCE,RETHET,REX,THET
COMMON /TVCURV/ TVC,BGDANG,RTVC(101),PCPW(101),RORWSQ(101),PW
COMMON /TE/ KTE,KTSITE
COMMON /WAK/ XKFAC
DATA YES/3HYES/

```



```

C
C
      ARS(X)=DABS(X)
      EXP(X)=DEXP(X)
      SQRT(X)=DSQRT(X)
      TANH(X)=DTANH(X)
      DSTARK=0.

C
C
      LAMTRB = 1 LAMINAR B.L. ,=2 TURBULENT B.L.

C
C
      IF (LAMTRB.EQ.2) GO TO 30

C
C
      LAMINAR

C
C
      COEFFICIENTS FOR MOMENTUM EQUATION

C
C
      DO 10 I=1,IE
      AOR(I)=RORWSQ(I)
      CCNTINUE
      CALL DERIV3 (AOR,XN,IE,1,AORP)
      IF ((X-XSTA(1)).LT.1.E-7) RETURN
      IF (PNC.LT.1.OE-10) RETURN
      CHIMAX=0.

C
C
      CALCULATES VORTICITY REYNOLDS NUMBER

C
C
      DO 20 N=2,IE
      CHI(N)=0.0
      IF (CHI(N).GT.CHIMAX) CHIMAX=CHI(N)

```

```

EFF0 330
EFF0 340
EFF0 350
EFF0 360
EFF0 370
EFF0 380
EFF0 390
EFF0 400
EFF0 410
EFF0 420
EFF0 430
EFF0 440
EFF0 450
EFF0 460
EFF0 470
EFF0 480
EFF0 490
EFF0 500
EFF0 510
EFF0 520
EFF0 530
EFF0 540
EFF0 550
EFF0 560
EFF0 570
EFF0 580
EFF0 590
EFF0 600
EFF0 610
EFF0 620
EFF0 630
EFF0 640

```



```

40 WRITE (6,210)
C WRITE (6,200)
C CONTINUE
C
C TURBULENT
C
C FAC1=0.0
C IF (KVS LAW.NE.0) GO TO 70
C DO 60 I=1,IM
C
C     INNER EDDY VISCOSITY LAW, REICHARDT EQUATION
C
C     FAC=CF/(2.*EPSVD)
C     IF (FAC.GT.0.0) GO TO 50
C     WRITE (6,180) FAC,CF,EPSVD
C     FAC=1.0E-6
C     CONTINUE
C     FAC1=SQRT(FAC)
C     EPSPL(I)=(.4*Y(I)*FAC1-4.4*TANH(Y(I)*FAC1/11.))*GAMMA
C     CONTINUE
C     GO TO 100
C
C     CONTINUE
C
C     INNER EDDY VISCOSITY LAW, VAN DRIEST EQUATION
C
C     FAC=SQRT(.5D0*CF)
C     IF (FAC.GT.0.0) GO TO 80
C     WRITE (6,180) FAC,CF,EPSVD
C     FAC=1.0E-6
C     CONTINUE
C     ROF=1.D0
C     DO 90 I=1,IM
C

```





```

120      CONTINUE
      II=1
      IF (KTSITE.EQ.1) GO TO 140
      IF (XK2.GT.100.0) GO TO 160
      DO 130 I=1,IE
      IF (EPSPL(I).LT.EPSQ(I)) GO TO 130
      II=I
      GO TO 140
130      CONTINUE
      II=IE
      DO 150 I=II,IE
      EPSPL(I)=EPSQ(I)
140      CONTINUE
      DO 170 I=1,IE
      AOB(I)=(1.+EPSPL(I))*RORWSQ(I)
150      CONTINUE
      CALL DERIV3 (AOB,XN,IE,1,AOBP)
      RETURN
      C
      C
      C
180      FORMAT (1H,14H FAC,CF,EPSVD /4F15.6///)
190      FORMAT (28H1
200      FORMAT (1H1)
210      FORMAT (26H1
      TRANSITION BEGINS/)
      TRANSITION ENDS/)
      END

```

```

EFF01610
EFF01620
EFF01630
EFF01640
EFF01650
EFF01660
EFF01670
EFF01680
EFF01690
EFF01700
EFF01710
EFF01720
EFF01730
EFF01740
EFF01750
EFF01760
EFF01770
EFF01780
EFF01790
EFF01800
EFF01810
EFF01820
EFF01830
EFF01840
EFF01850
EFF01860

```

```

C      SUBROUTINE EGPROP (IFLAG)
C      IMPLICIT REAL*8(A-H,O-Z)
C
C      SUBROUTINE EGPROP CALLS SUBROUTINES BLUNT2 AND CONE2.
C
C      SUBROUTINE EGPROP IS CALLED BY SUBROUTINE DELTAS.
C
C      SUBROUTINE EGPROP OBTAINS EDGE PROPERTIES FOR SPECIFIED GEOMETRY
C      FOR VALUES OF X AFTER THE INITIAL VALUE OF X.
C
C      COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITEGPO
13,NOSE
C
C      GO TO (10,20), NOSE
C      CONTINUE
C      CALL BLUNT2 (IFLAG)
C      RETURN
C      CONTINUE
C      CALL CONE2 (IFLAG)
C      RETURN
C      END
10
20
EGPO 10
EGPO 20
EGPO 30
EGPO 40
EGPO 50
EGPO 60
EGPO 70
EGPO 80
EGPO 90
EGPO 100
EGPO 110
EGPO 120
EGPO 130
EGPO 140
EGPO 150
EGPO 160
EGPO 170
EGPO 180
EGPO 190
EGPO 200
EGPO 210
EGPO 220

```



```

SUBROUTINE FD3 (X,X1,X2,X3,F1,F2,F3,FX)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE FD3 IS CALLED BY SUBROUTINE DERIV3.

SUBROUTINE FD3 CALCULATES THE FIRST DERIVATIVE-FX-CORRESPONDING
TO POINT X USING 3 POINT LAGRANGIAN DIFFERENTIATION FORMULA.

ASSUMES X1 .LE. X .LE. X3.

A1=2.0*X-X2-X3
A2=2.0*X-X1-X3
A3=2.0*X-X1-X2
D1=(X1-X2)*(X1-X3)
D2=(X2-X1)*(X2-X3)
D3=(X3-X1)*(X3-X2)
C1=A1/O1
C2=A2/O2
C3=A3/O3
FX=C1*F1+C2*F2+C3*F3
RETURN
END

```

U U U U U U U U

```

C      SUBROUTINE GEOM
C      IMPLICIT REAL*8(A-H,O-Z)
C
C      SUBROUTINE GEOM CALLS SUBROUTINES BLUNT1 AND CONE1.
C
C      SUBROUTINE GEOM IS CALLED BY MAIN AND SUBROUTINE INIT.
C
C      SUBROUTINE GEOM OBTAINS EDGE PROPERTIES FOR SPECIFIED GEOMETRY
C      FOR THE INITIAL VALUE OF X.
C
C      COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITGEOM
C      13,NOSE
C
C      NCSE=1 BLUNT BODY
C      NCSE=2 SHARP NOSE BODY
C
C      GO TO (10,20), NCSE
C      CALL BLUNT1
C      RETURN
C      CONTINUE
C      CALL CONE1
C      RETURN
C      END
10
20

```

GEOM 10  
 GEOM 20  
 GEOM 30  
 GEOM 40  
 GEOM 50  
 GEOM 60  
 GEOM 70  
 GEOM 80  
 GEOM 90  
 GEOM 100  
 GEOM 110  
 GEOM 120  
 GEOM 130  
 GEOM 140  
 GEOM 150  
 GEOM 160  
 GEOM 170  
 GEOM 180  
 GEOM 190  
 GEOM 200  
 GEOM 210  
 GEOM 220  
 GEOM 230



```

SUBROUTINE INIT
  IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE INIT CALLS SUBROUTINES DELTAS AND GEOM.

SUBROUTINE INIT IS CALLED BY MAIN.

THIS SUBROUTINE PROVIDES INITIALIZATION OF DATA FOR THE PROGRAM.

COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(
1101),RZ(501)
COMMON /CONVERG/ CONVRG,CCRN1,CRNI,DIF,DIFF,NC
COMMON /COEFF3/ CFI,SUM,SUM1,SUMT
COMMON /COMMON1/ A15,E1,FF,F2N1,VK
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UE02,UESO
COMMON /FRSTRM/ PFS,REINF,RHOF5,UFS
COMMON /GECME/ DS,DX,DX1,DXMAX,DXCLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLD
1,XJ,XJFAC,Z,ZOL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITINIO
13,NOSE
COMMON /NTEGP/ II,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,L
1AMTRB,NITTOT
COMMON /REF/ PREF,RHOREF,UREF
COMMON /STAG/ PIO,PSTAG
COMMON /TRANS/ ATR,CHICRI,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS
COMMON /VSCSTY/ EPSVD,XK1,XK2
COMMON /STAG4/ UECN,PECN
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RCRW(101),RORWSQ(101),RW
COMMON /TE/ KTE,KTSTTE
COMMON /WAK/ XKFAC
COMMON /DRAG/ CDV1,CDV2,XCP,XCP1

```

INIO 10  
 INIO 20  
 INIO 30  
 INIO 40  
 INIO 50  
 INIO 60  
 INIO 70  
 INIO 80  
 INIO 90  
 INIO 100  
 INIO 110  
 INIO 120  
 INIO 130  
 INIO 140  
 INIO 150  
 INIO 160  
 INIO 170  
 INIO 180  
 INIO 190  
 INIO 200  
 INIO 210  
 INIO 220  
 INIO 230  
 INIO 240  
 INIO 250  
 INIO 260  
 INIO 270  
 INIO 280  
 INIO 290  
 INIO 300  
 INIO 310  
 INIO 320

C  
 C  
 C  
 C  
 C  
 C  
 C

```

C
C
DATA YES,NO/3HYES,2HNO/
BODANG=0.00
IF (TVC.EQ.NO) RW=1.00
XSTA(IIMAX+1)=-2.E6
XSTA = -2.E6 TERMINATES SOLUTION
KEP=0
XJAY=XJFAC
CF=1.00
VM=0.0
KSTUP=0
II=2
IPRNT=1
SUM=0.0
CDVI=0.0
SUMI=0.0
SUMT=0.0
Z=ZA(1)
X=XSTA(1)
XI=0.00
XI2=2.00*XI
XIOLD=XI
XCLO=X
DXCLO=0.0
DS=1.00
CCRN1=1.00-CRNI
EI=0.00
FIN=1.00
FF=0.00
NII=0
NITTOT=0
INI0 330
INI0 340
INI0 350
INI0 360
INI0 370
INI0 380
INI0 390
INI0 400
INI0 410
INI0 420
INI0 430
INI0 440
INI0 450
INI0 460
INI0 470
INI0 480
INI0 490
INI0 500
INI0 510
INI0 520
INI0 530
INI0 540
INI0 550
INI0 560
INI0 570
INI0 580
INI0 590
INI0 600
INI0 610
INI0 620
INI0 630
INI0 640

```

```

10  ISTOP=0
    CHIMAX=0.0
    GAMMA=1.
    IF (LAMTRB.EQ.1) GAMMA=0.0
    XIBAR=0.
    KTSTTE=0
    IM=IE-1
    JJ=1
    RHOF=2.*(PSTAG-PFS)/(UFS*UFS)
    CALL GEOM
    DX1=DX
    IF (NOSE.EQ.2) GO TO 10
    IF (NOSE.EQ.1) GO TO 20
    IF (LAMTRB.NE.2) GO TO 20
    CONTINUE
    X=XSTA(1)+1.D-02
    IF (TVC.EQ.YES) X=XSTA(1)+0.01D0
    IF (TVC.EQ.YES) X=XSTA(1)+0.00025
    RO=X*DSIN(BUDANG)
    DX=0.010
    IF (TVC.EQ.YES) DX=.00025
    XCLOD=X
    UER02=UE
    IF (TVC.EQ.YES) UER02=UE*RO**2
    IF (XKFAC.GT.1.D-04) UER02=UE**3
    CALL DELTAS
    DX=DX1
    CONTINUE
    RETURN
    END

20  C

```

```

INIO 650
INIO 660
INIO 670
INIO 680
INIO 690
INIO 700
INIO 710
INIO 720
INIO 730
INIO 740
INIO 750
INIO 760
INIO 770
INIO 780
INIO 790
INIO 800
INIO 810
INIO 820
INIO 830
INIO 840
INIO 850
INIO 860
INIO 870
INIO 880
INIO 890
INIO 900
INIO 910
INIO 920
INIO 930
INIO 940
INIO 950

```



```

SUBROUTINE INTERP (XX,XN,F2,IE,FF)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE INTERP CALLS FUNCTION TLU.

SUBROUTINE INTERP IS CALLED BY SUBROUTINES COEF AND EFFMU.

SUBROUTINE INTERP USES FUNCTION TLU TO INTERPOLATE IN ARRAY F2
FOR THE VALUE FF CORRESPONDING TO THE VALUE XX IN ARRAY XN.
IF XX .LT. XN(1) .OR. XX .GT. XN(IE), FF IS SET EQUAL TO F2(IE)
AND A MESSAGE IS PRINTED.

DIMENSION XN(101), F2(101)

FF=TLU(IE,F2,XN,XX,NFLAG)
IF (NFLAG.NE.1) RETURN
WRITE (6,10)
FF=F2(IF)
RETURN

FORMAT (1HC,10X,38HINADAQUATE TABLE FOR SUBROUTINE INTERP, //11X,43INPO 240
1HSTANDARD FIXUP TAKEN - EXECUTION CONTINUING)
END

```

INT0	10
INT0	20
INT0	30
INT0	40
INT0	50
INT0	60
INT0	70
INT0	80
INT0	90
INT0	100
INT0	110
INT0	120
INT0	130
INT0	140
INT0	150
INT0	160
INT0	170
INT0	180
INT0	190
INT0	200
INT0	210
INT0	220

```

C SUBROUTINE INTER5 (X,X1,X2,X3,X4,X5,F1,F2,F3,F4,F5,F)
C IMPLICIT REAL*8(A-H,O-Z)
C
C SUBROUTINE INTER5 IS CALLED BY SUBROUTINES BLUNT1, BLUNT2, CONE1,
C CONE2, INIT, ZRO, AND INTRP5.
C
C SUBROUTINE INTER5 INTERPOLATES FOR THE VALUE F CORRESPONDING TO
C POINT X USING 5 POINT LAGRANGIAN INTERPOLATION FORMULA.
C
C ASSUMES X1 .LE. X .LE. X5.
C
C A1=(X-X2)*(X-X3)*(X-X4)*(X-X5)
C A2=(X-X1)*(X-X3)*(X-X4)*(X-X5)
C A3=(X-X1)*(X-X2)*(X-X4)*(X-X5)
C A4=(X-X1)*(X-X2)*(X-X3)*(X-X5)
C A5=(X-X1)*(X-X4)*(X-X3)*(X-X4)
C D1=(X1-X2)*(X1-X3)*(X1-X4)*(X1-X5)
C D2=(X2-X1)*(X2-X3)*(X2-X4)*(X2-X5)
C D3=(X3-X1)*(X3-X2)*(X3-X4)*(X3-X5)
C D4=(X4-X1)*(X4-X2)*(X4-X3)*(X4-X5)
C D5=(X5-X1)*(X5-X2)*(X5-X3)*(X5-X4)
C C1=A1/D1
C C2=A2/D2
C C3=A3/D3
C C4=A4/D4
C C5=A5/D5
C F=C1*C2+C2*C3+F3+C4*C5+C5*F5
C RETURN
C END

```



INT0	10
INT0	20
INT0	30
INT0	40
INT0	50
INT0	60
INT0	70
INT0	80
INT0	90
INT0	100
INT0	110
INT0	120
INT0	130
INT0	140
INT0	150
INT0	160
INT0	170
INT0	180
INT0	190

```

SUBROUTINE MOMENT
  IMPLICIT REAL*8(A-H,O-Z)

  SUBROUTINE MOMENT CALLS SUBROUTINES EFFMU AND SOLVE.

  SUBROUTINE MOMENT IS CALLED BY MAIN.

  THIS SUBROUTINE PROVIDES THE SOLUTION FOR THE MOMENTUM EQUATION.

  COMMON /ARRAY1/ AOB(101),AOBP(101),A1(101),A2(101),A3(101),A4(101),FMCMO 100
  1,CHI(101),DN(102),DN2(102),EPSO(101),EPSPL(101),F1(101),FIN(101),FMCMO 110
  21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(101),VC 120
  3011,XN(102),XN2(102),Y(101),YCVDEL(101),YDVTHY(101),YY(101)
  COMMON /CNVERG/ CONVRG,CCRN1,CRN1,DIF,DIFF,NC
  COMMON /COEFF/ CFBAF,CFPREX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,
  1DSTARK,DSTARX,HAFCF,RETHET,REX,THET
  COMMON /COMWLL/ AIB,E1,FF,F2N1,VW
  COMMON /EDGPRP/ BETA,DUEFS,PE,PESO,PP,UE,UERO2,UESO
  COMMON /GEOME/ DS,DX,DX1,DXMAX,DXLLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLDMCMO 190
  1,XJ,XJFAC,Z,ZCL,RO
  COMMON /INTGR/ IE,IIMAX,IN,IPRNT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITMCMO 210
  13,NOSE
  COMMON /NIEGER/ II,IPFL,IPRINT,JJ,K,KADEIA,KEND,KEP,KSTCP,KTRNSN,L,MCMO 230
  1A,TRB,NITTOT
  COMMON /DIFP/ DIFM(301)
  COMMON /TE/ KTE,KTSTTE

  ARS(X)=DABS(X)

  DIF=0.00

```

```

C      CALL EFFMU (LAMTRB,KEP,DSARK)
C
C      MOMENTUM EQUATION SOLUTION
C      MOMENTUM EQUATION COEFFICIENTS
C
C      DO 10 N=2,IM
C      A1(N)=(AOBP(N)-VC(N))/AOB(N)
C      A2(N)=-BETA*FC(N)/AOB(N)
C      A3(N)=BETA/AOB(N)
C      A4(N)=-2.*XI*FC(N)/AOB(N)
C      CONTINUE
C      BC1=E1
C      BC2=FF
C      IF (KTSTTE.EQ.0) GO TO 20
C      BC1=1.D0
C      BC2=0.D0
C      CONTINUE
C      CALL SOLVE (FINN,FIN,F1,F2NN,F2N,F2,BC1,BC2,CRN1)
C      KF2=0
C      DO 30 N=2,IE
C      IF (F2(N).GT.1.0E-6) GO TO 30
C      KF2=1
C      F2(N)=1.0E-6
C      CONTINUE
C      IF (KF2.EQ.1) CALL DERIV3 (F2,XN,IE,1,F2N)
C      IF (KF2.EQ.1) CALL DERIV3 (F2N,XN,IE,1,F2NN)
C      IF (NC.NE.0) GO TO 40
C
C      DERIVATIVE CONVERGENCE TEST AT WALL
C
C      FPW=(F2(2)-F2(1))/XN(2)
C      DIFF=(FPW-FPW)/FPW

```

MOMO 330  
MOMO 340  
MOMO 350  
MOMO 360  
MOMO 370  
MOMO 380  
MOMO 390  
MOMO 400  
MOMO 410  
MOMO 420  
MOMO 430  
MOMO 440  
MOMO 450  
MOMO 460  
MOMO 470  
MOMO 480  
MOMO 490  
MOMO 500  
MOMO 510  
MOMO 520  
MOMO 530  
MOMO 540  
MOMO 550  
MOMO 560  
MOMO 570  
MOMO 580  
MOMO 590  
MOMO 600  
MOMO 610  
MOMO 620  
MOMO 630  
MOMO 640



AD-A074 972

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MCMO 650  
 MCMO 660  
 MCMO 670  
 MCMO 680  
 MCMO 690  
 MCMO 700  
 MCMO 710  
 MCMO 720  
 MCMO 730  
 MCMO 740  
 MCMO 750  
 MCMO 760  
 MCMO 770  
 MCMO 780  
 MCMO 790  
 MCMO 800  
 MCMO 810  
 MCMO 820  
 MCMO 830  
 MCMO 840  
 MCMO 850  
 MCMO 860  
 MCMO 870  
 MCMO 880  
 MCMO 890

```

40      FPMW=FPM
      IF (DIFF.GT.DIF) DIF=DIFF
      CONTINUE
      IF (K.GT.1) GO TO 60
      DC 50 N=1,IE
      F1(N)=F2(N)
      FIN(N)=F2N(N)
      FINN(N)=F2NN(N)
      CONTINUE
      IF (NC.EQ.0) GO TO 80
      DC 70 N=2,IE

      ALL POINTS CONVERGENCE TEST

      DIFF=ABS(1.0-FC(N)/F2(N))
      DIFM(N)=DIFF
      IF (DIFF.GT.DIF) DIF=DIFF
      CONTINUE
      CCCONTINUE
      DC 90 N=1,IE
      FCP(N)=(F2(N)-F1(N))/DS
      FCN(N)=F2N(N)*CRNI+FIN(N)*CCRN1
      FC(N)=F2(N)*CRNI+F1(N)*CCRN1
      RETURN
      END
90
70
80
C
C
C

```



```

SUBROUTINE PROFILE
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE PROFILE IS CALLED BY MAIN.

SUBROUTINE PROFILE GENERATES THE INITIAL VELOCITY PROFILE.

COMMON /ARRAY1/ AOB(101),AOBP(101),AI(101),A2(101),A3(101),A4(101)
1,CHI(101),DA(102),DR2(102),EPSG(101),EPSPL(101),F1(101),FIN(101),FPRF 10
21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(101)PRF 20
301),XN(102),XN2(102),Y(101),YCVDEL(101),YGVTH(101),YY(101)PRF 30
COMMON /COMWLL/ AIB,EI,FF,F2N1,VNPRF 40
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UER02,UESOPRF 50
COMMON /GEUME/ DS,CX,DX1,DXMAX,DXCLD,PNC,REFLEN,SCF,X,X1,X12,XIULDPRF 60
1,XJ,XJFAC,Z,ZDL,ROPRF 70
COMMON /INTGR/ IE,IIMAX,IM,IPENT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITPRF 80
13,NUSEPRF 90
COMMON /NMLCRD/ ADTEST,ETAINF,XKETAPRF 100
COMMON /REF/ PREF,RHOREF,UREFPRF 110
COMMON /CFPR/ CFPRF 120
COMMON /VSCSTY/ EPSVD,XK1,XK2PRF 130
COMMON /TVCURV/ TVC,BGDANG,FTVC(101),RCRW(101),ROPWSQ(101),RWPRF 140
COMMON /SPTVC/ RNCSEPRF 150
COMMON /WAK/ XKFACPRF 160
DATA YES/3HYES/PRF 170

EXP(X)=DEXP(X)PRF 180
FLCAT(M)=DFLOAT(M)PRF 190

DEVELOP INITIAL ETA GRIDPRF 200
PRF 210
PRF 220
PRF 230
PRF 240
PRF 250
PRF 260
PRF 270
PRF 280
PRF 290
PRF 300
PRF 310
PRF 320

```

```

10 IF (XKETA.EQ.1.0) DETAL=ETAINF/FLGAT(IE-1)
   IF (XKETA.NE.1.0) DETAL=ETAINF*(XKETA-1.0)/(XKETA**IM-1.0)
   DN(1)=DETAL
   XN(1)=0.00
   Y(1)=0.0
   XN(IE)=ETAINF
   DO 10 N=1,IE
     DN(N+1)=XKETA*DN(N)
     XN(N+1)=XN(N)+DN(N)
   CONTINUE
   YY(1)=1.00
   RW=1.00
   IF (XJFAC.GT.1.0-D-05.OR.XKFAC.GT.1.0-D-05) RW=RO
   RVC(1)=RW
   RORW(1)=1.00
   IF (XKFAC.GT.1.0-D-05) RORW(1)=C.00
   RORWSQ(1)=RORW(1)**2
   IF (NCSE.EQ.1) GO TO 20
   C
   C
   C
   SHARP NOSE
   RD=RW
   RDD=RW
   RDDD=RD
   IF (XKFAC.GT.1.0-D-04) RDDD=UE
   RT=1.00
   GO TO 30
   CONTINUE
   20 BLUNT NOSE
   C
   C
   C
   RD=RNCSE

```

PRFO 330  
 PRFO 340  
 PRFO 350  
 PRFO 360  
 PRFO 370  
 PRFO 380  
 PRFO 390  
 PRFO 400  
 PRFO 410  
 PRFO 420  
 PRFO 430  
 PRFO 440  
 PRFO 450  
 PRFO 460  
 PRFO 470  
 PRFO 480  
 PRFO 490  
 PRFO 500  
 PRFO 510  
 PRFO 520  
 PRFO 530  
 PRFO 540  
 PRFO 550  
 PRFO 560  
 PRFO 570  
 PRFO 580  
 PRFO 590  
 PRFO 600  
 PRFO 610  
 PRFO 620  
 PRFO 630  
 PRFO 640

```

RDD=1.00
RDD=RD
IF (XKFAC.GT.1.D-04) RDD=DUEDS
RT=0.00
CONTINUE
DEVELOP STRETCHED AND UNSTRETCHED COORDINATES FOR NO CURVATURE
CASES
CSOKW=1.00
IF (RW.GT.1.D-06) CSORW=DCOS(PODANG)/RW
XDOUG1=ETAINF/6.00
DO 50 N=1,IF
Y(N)=PNC*XN(N)
YY(N)=Y(N)*EPSVD
RCRW(N)=1.00
RCRWSQ(N)=1.00
RTVC(N)=RW
DEVELOP STRETCHED AND UNSTRETCHED COORDINATES FOR TVC CASES
IF (TVC.NE.YES) GO TO 40
YY(N)={-1.00+DSQRT(1.00+2.00*EPSVD*Y(N)*CSORW)}/CSORW
RDUM=RD+RDD*YY(N)*CSORW
RTVC(N)=RT*RDUM
RCRW(N)=RDUM/RDDC
RCRWSQ(N)=RCRW(N)**2
Y(N)=YY(N)/EPSVD
CONTINUE
USE ASSUMED VELOCITY PROFILE FOR INITIAL GUESS. VARIATION OF 1/6
POWER LAW.

```

30  
C  
C  
C  
C

C  
C  
C

40  
C  
C  
C

PRFO 650  
PRFO 660  
PRFO 670  
PRFO 680  
PRFO 690  
PRFO 700  
PRFO 710  
PRFO 720  
PRFO 730  
PRFO 740  
PRFO 750  
PRFO 760  
PRFO 770  
PRFO 780  
PRFO 790  
PRFO 800  
PRFO 810  
PRFO 820  
PRFO 830  
PRFO 840  
PRFO 850  
PRFO 860  
PRFO 870  
PRFO 880  
PRFO 890  
PRFO 900  
PRFO 910  
PRFO 920  
PRFO 930  
PRFO 940  
PRFO 950  
PRFO 960



PRF0 970  
 PRF0 980  
 PRF0 990  
 PRF01000  
 PRF01010  
 PRF01020  
 PRF01030  
 PRF01040  
 PRF01050  
 PRF01060  
 PRF01070  
 PRF01080  
 PRF01090  
 PRF01100  
 PRF01110  
 PRF01120  
 PRF01130  
 PRF01140  
 PRF01150  
 PRF01160  
 PRF01170  
 PRF01180  
 PRF01190

C  
 F1(N)=1.0-EXP(-XN(N)/XDOUG1)  
 FIN(N)=EXP(-XN(N)/XDOUG1)  
 IF (FIN(N).LE.1.0D-25) FIN(N)=0.0  
 FINN(N)=-FIN(N)  
 F2NN(N)=FINN(N)  
 FC(N)=F1(N)  
 FCN(N)=FIN(N)  
 FCP(N)=0.0  
 VC(N)=VW-XN(N)/XDOUG1  
 EPSPL(N)=0.0  
 F2(N)=F1(N)  
 YCVDEL(N)=0.0  
 YCVTHT(N)=0.0  
 CHI(N)=0.0  
 CONTINUE  
 F1(IE)=1.0  
 F2(IE)=1.0  
 FC(IE)=1.0  
 FIN(IE)=0.0  
 FINN(IE)=0.0  
 RETURN  
 END

```

SUBROUTINE READIN
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE READIN CALLS SUBROUTINES WRITE1 AND WRITE2.

SUBROUTINE READIN IS CALLED BY MAIN AND SUBROUTINE WRITE2.

SUBROUTINE READIN PROVIDES THE INPUT OF DATA FOR THE PROGRAM.

COMMON /ARRAY1/ AOB(101),AOBP(101),AI(101),A2(101),A3(101),A4(101)
1,CHI(101),DN(102),DN2(102),EPSU(101),EPSPL(101),FI(101),FIN(101),FREAO 100
21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(101)FREAO 110
301),XN(102),XN2(102),Y(101),YCVDEL(101),YOVTH(101),YY(101)FREAO 120
CC44ON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(101)FREAO 130
1101),RZ(501)FREAO 140
COMMON /CNVERG/ CONVRG,CCRN1,CRN1,DIF,DIFF,NCFREAO 150
IDSTARK,OSTARX,HAFCF,RETHET,REX,THETFREAO 160
IEFL,THODEL,THOREF,XGREFL,ZOREFLFREAO 170
COMMON /COEFF3/ CF1,SUM,SUM1,SUMT
COMMON /COMWLL/ A18,E1,FF,F2N1,VH
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UER02,UES0FREAO 180
COMMON /FRSTRM/ PFS,REINF,RHOFS,UFS
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXGLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLDREAO 190
1,XJ,XJFAC,Z,ZOL,ROFREAO 200
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITREAO 210
13,NOSEFREAO 220
COMMON /NTEGER/ I1,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,LREAO 230
1AMTR8,NITTOTFREAO 240
COMMON /NMLCRD/ ADTEST,ETAINF,XKETA

```

C  
C  
C  
C  
C  
C  
C

UU U UU UU UU



```

C
IF (IREAD.EQ.0) GO TO 10
CALL RESTAR
GO TO 50
10 IF (KHESS.EQ.0) GO TO 20
C
FOR RESTART CASE, READ IN STANDARD HESS INPUT
C
READ (5,260) HEDK,CASE,ICARD2,ICARD3,ICARD4,NN,IBDN
C
READ (5,210) BETAS,POMAX
20 READ (5,190) LABEL
C
      TITLE CARD
C
WRITE (6,200) LABEL
C
      READ (5,180) NCSE,LAMTRR,KVSLAW,KTRANS,KTRNSN,KONSET,KTE
      READ (5,160) NIT1,NIT2,NIT3,NC
      READ (5,140) IE,KEND,IIMAX
      READ (5,170) KADETA,KL,IPFL,IPRINT,IWT
      READ (5,210) CHICRT,XBAR,ATR
      READ (5,210) UFS,REINF,PFS,PSTAG,SCF,RNCSE
      READ (5,210) XK1,XK2,CONVRG,ADTEST
      READ (5,210) DX,CRNI,XKETA,ETAINF,REFLEN
      READ (5,150) XJFAC,XKFAC,TVC
      READ (5,220) OXMAX,XLOCA,OYDX,JSTA,NCPRFS
      READ (5,230) (IPR(J),J=1,IPRINT)
      READ (5,230) (IPRFL(J),J=1,IPFL)
      IWRTH=1
      J=0
      J=J+1
30

```

```

READ 650
READ 660
READ 670
READ 680
READ 690
READ 700
READ 710
READ 720
READ 730
READ 740
READ 750
READ 760
READ 770
READ 780
READ 790
READ 800
READ 810
READ 820
READ 830
READ 840
READ 850
READ 860
READ 870
READ 880
READ 890
READ 900
READ 910
READ 920
READ 930
READ 940
READ 950
READ 960

```

```

40 READ (5,240) ZA(J),RZ(J),XSTA(J),PZ(J),LSTC
50 IF (LSTC.EQ.LST) GO TO 40
    GC TO 30
    IIMAX=J
    J=IIMAX
    IF (KHESS.EQ.0) GO TO 100
    READ (18,250) (CP(I),I=1,J)
    C
    IF ON INITIAL ITERATION, SAVE INITIAL PRESSURE COEFF'S. FOR USE
    C IN REAO1050
    C DRAG CALCULATIONS.
    C
    DO 60 I=1,J
    60 CP(I)=CP(I)
    C
    DEVELOP PRESSURES FROM PRESSURE COEFF'S.
    C
    RHO=(PSTAG-PFS)*2/UFS**2
    DO 70 I=1,J
    70 PZ(I)=(PFS+CP(I)*0.5*RHC*UFS**2)/PSTAG
    IF (IREAD.NE.1) GO TO 90
    DO 80 I=1,J
    80 PZ(I)=PZ(I)*P10
    UEZ(I)=DSQRT(2.00*(P10-PZ(I)))
    WRITE (6,200) LABEL
    WRITE (6,110) P10
    WRITE (6,120) UE,PE
    CALL WRITEL
    RETURN
    90 CONTINUE
    IF (IREAD.EQ.1) RETURN
    100 CONTINUE
    IW=IWT-1

```

REAO 970  
 REAO 980  
 REAO 990  
 REAO1000  
 REAO1010  
 REAO1020  
 REAO1030  
 REAO1040  
 INREAO1050  
 REAO1060  
 REAO1070  
 REAO1080  
 REAO1090  
 REAO1100  
 REAO1110  
 REAO1120  
 REAO1130  
 REAO1140  
 REAO1150  
 REAO1160  
 REAO1170  
 REAO1180  
 REAO1190  
 REAO1200  
 REAO1210  
 REAO1220  
 REAO1230  
 REAO1240  
 REAO1250  
 REAO1260  
 REAO1270  
 REAO1280

```

110 IF (NIT1.EQ.0) NIT1=3
120 IF (NIT1.LT.0) NIT1=0
130 IF (NIT2.EQ.0) NIT2=6
    IF (NIT3.EQ.0) NIT3=9
    IF (KL.EQ.0) KL=2
    IF (ADTEST.EQ.0.0) ADTEST=0.0010
    IF (CONVRG.EQ.0.0) CONVRG=0.0010
    IF (ETAINF.EQ.0.0) ETAINF=100.0
    IF (XKETA.EQ.0.0) XKETA=1.09
    IF (LAMTRB.EQ.0) LAMTRB=1
    IF (NCSE.EQ.0) NCSE=1
    IF (XK1.EQ.0.0) XK1=0.40
    IF (XK2.EQ.0.0) XK2=0.01680
    IF (KTRNSN.GT.11MAX) KTRNSN=11MAX
    IF (KTRNSN.EQ.0) KTRNSN=11MAX
    IF (KTE.EQ.0) KTE=11MAX
    IF (KONSET.EQ.0) KONSET=11MAX
    RETURN
C
C
C
140 FORMAT (1H,,2X,4HP10=,D15.7)
150 FORMAT (9H,,UESO=,D15.7,9H,,PF50=,D15.7)
    FORMAT (60X,13HPROGRAM ICBL//60X,13HA PROGRAM FOR/21X,89H2-D AND REAO1520
    LAXISYMMETRIC INCOMPRESSIBLE, LAMINAR, TRANSITIONAL AND/OR TURBULENCEAO1530
    2TBUNDARY-LAYER/42X,47HFLOW INCLUDING EFFECTS OF TRANSVERSE CURVATUREAO1540
    3URE./66X,2HBY/45X,41HD.L. DWYER, C.H. LEWIS AND E.C. ANDERSON/47XREAO1550
    4,37HAEROSPACE AND OCEAN ENGINEERING DEPT./41X,51HVIRGINIA POLYTECHNICAO1560
    5NIC INSTITUTE AND STATE UNIVERSITY/56X,21HBLACKSBURG, VA. 24061/56REAO1570
    6X,22HPHONE - (703)-951-6126//)
    FORMAT (4(1X,13))
    FORMAT (2F12.6,4X,A3)
    REAO1580
    REAO1590
    REAO1600

```

```

REAO1290
REAO1300
REAO1310
REAO1320
REAO1330
REAO1340
REAO1350
REAO1360
REAO1370
REAO1380
REAO1390
REAO1400
REAO1410
REAO1420
REAO1430
REAO1440
REAO1450
REAO1460
REAO1470
REAO1480
REAO1490
REAO1500
REAO1510

```



REA01610  
 REA01620  
 REA01630  
 REA01640  
 REA01650  
 REA01660  
 REA01670  
 REA01680  
 REA01690  
 REA01700  
 REA01710  
 REA01720

160      FORMAT (6(8X,I2))  
 170      FORMAT (6(7X,I3))  
 180      FORMAT (3(8X,I2),4(7X,I3),9X,I1)  
 190      FORMAT (18A4)  
 200      FORMAT (1H0,30X,18A4////)  
 210      FORMAT (6F12.6)  
 220      FORMAT (3F12.6,2I3)  
 230      FORMAT (14I5)  
 240      FORMAT (4E12.6,A4)  
 250      FORMAT (12X,F12.6)  
 260      FORMAT (10A6,2X,A6/I3/I5/I1X,I4,I5/9X,I1)  
          END

```

SUBROUTINE RESTAR
  RESO 10
  RESO 20
  RESO 30
  RESO 40
  RESO 50
  RESO 60
  RESO 70
  RESO 80
  RESO 90
  RESO 100
  RESO 110
  RESO 120
  RESO 130
  RESO 140
  RESO 150
  RESO 160
  RESO 170
  RESO 180
  RESO 190
  RESO 200
  RESO 210
  RESO 220
  RESO 230
  RESO 240
  RESO 250
  RESO 260
  RESO 270
  RESO 280
  RESO 290
  RESO 300
  RESO 310
  RESO 320

  SUBROUTINE RESTAR WRITES A DATA TAPE AT THE RESTART POINT
  INCLUDING ALL VAGRIABLES THAT ARE NECESSARY FOR THE
  PROGRAM TO CALCULATE A NEW SOLUTION USING A PREVIOUS ITER-
  ATION SOLUTION.

  IMPLICIT REAL*8(A-H,O-Z)
  COMMON /APRAY1/ AOB(101),A0BP(101),A1(101),A2(101),A3(101),A4(101),FRESO 110
  1,CHI(101),DN(102),DN2(102),EPSQ(101),EPSPL(101),F1(101),F1N(101),FRESO 120
  21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(IRESO 130
  301),XN(102),XN2(102),Y(101),YCVDEL(101),YQVHT(101),YY(101)
  COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZAI(501),IPR(101),IPRFL(IRESO 150
  1101),RZ(501)
  COMMON /COEFF/ CFBAR,CFBREX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,RESO 160
  1DSTARK,DSTARX,HAFCF,RETHET,REX,THET
  COMMON /COEFF2/ DELORF,DELCX,DSAXCR,DSTODL,DSTORF,DSTGTH,DSTOX,RORRESO 170
  1EFL,THODEL,THCKEF,XCOREFL,ZOREFL
  COMMON /COEFF3/ CF1,SUM,SUM1,SUMT
  COMMON /COMWLL/ A1B,E1,FF,F2N1,VW
  COMMON /CFPR/ CF
  COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UEO2,UESO
  COMMON /FRSTRM/ PFS,REINF,RHOF,UFFS
  COMMON /GEUME/ DS,DX,OX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,X1,XI2,XIOLDRESO 260
  1,XJ,XJFAC,Z,ZOL,RO
  COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITRESO 280
  13,NUSE
  COMMON /NTEGER/ I1,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,LRESO 300
  1AMTRB,NITTUT
  COMMON /TRANS/ ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS,KONSET

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COMMON /VSCSTY/ EPSVD,XK1,XK2
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RORW(101),RORWSQ(101),RM
COMMON /LWALL/ UOUPLS(101),YPLUS(101),UDEF(101),UPLUS
COMMON /STAG/ P10,PSTAG,RHQ
COMMON /CNVERG/ CONVRG,CCRN1,CRNI,DIF,DIFF,NC
COMMON /NMLCRD/ ADTEST,ETAINF,XKETA
COMMON /REF/ PREF,RHOREF,UREF
COMMON /WTE/ IW,IWT
COMMON /TE/ KTE,KTSITE
COMMON /WAK/ XKFAC
COMMON /HESS/ IWRTH,ICARD2,ICARD3,ICARD4,NN,IBDN,HEDR(10),CASE,KHERES0
1SS
COMMON /INTACT/ BETAS
COMMON /DRAG/ CDV1,CDV2,XCP,XCP1,CP(501),CPI(501),ROMAX
COMMON /BDCORR/ ZDELST(501),RODELS(501),ZOLD(501),ROLD(501),MM
COMMON /STRTUP/ IREAD,IRSRT,KK
COMMON /APLDAT/ XLOCA,DYDX,JSTA,NCPRFS
IF (IREAD.EQ.1) GO TO 10
IF (IRSRT.GT.1) GO TO 30
GO TO 40
10
READ (20) AOB,AOBP,DN,EPSPL,F2,F2N,F2NN,FC,FCN,FCP,VC,XN,Y,YOVDEL,RES0
1YCVTHT,YY,CONVRG,CCRN1,CRNI,DIF,DIFF,NC,CFBAR,CFBEX,CFE,CFINF,CFRRES0
2ES,CFREY,DEL,DELST,DELTA,DSTARK,DSTORF,DSTOTH,DSTOCX,RCREFL,THODEL,THOREF,XGRRES0
3F,DELOX,DSAXOR,DSTODL,DSTORF,DSTOCX,RCREFL,THODEL,THOREF,XGRRES0
4EFL,ZORELF,CFL,SUM,AIB,E1,FF,F2N1,VW,CF,DUEDES,PE,PESO,PP,UE,UER02,RES0
5UESO,PFS,REINF,RHCFS,UFS,DS,DX,DX1,DXMAX,DXGLD
READ (20) PNC,RO,REFLEN,SCF,X,XI,XI2,XIGLD,XGLD,XJ,XJFAC,Z,ZOL,IE,RES0
1IIMAX,IM,IPRNT,ISTUP,KL,KVSLAW,NIT,NIT1,NIT2,NIT3,NIT3,NOSE,II,IPFL,IPRRES0
2INT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,LAMTRB,NITTOT,ADTEST,ETAINF,RES0
3XKETA,P10,PSTAG,ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS,EPSVD,XKRES0
41,XK2,HEDR,CASE,ICARD2,ICARD3,ICARD4,NN,IBDN,BETAS,XSTA,UJZ,PZ,ZA,RES0
5IPR,IPRFL,RZ,KHESS,PREF,RHOREF,UREF,IW,IWT,KTE,KTSITE,XKFAC,KONSETRES0
RES0 330
RES0 340
RES0 350
RES0 360
RES0 370
RES0 380
RES0 390
RES0 400
RES0 410
RES0 420
RES0 430
RES0 440
RES0 450
RES0 460
RES0 470
RES0 480
RES0 490
RES0 500
RES0 510
RES0 520
RES0 530
RES0 540
RES0 550
RES0 560
RES0 570
RES0 580
RES0 590
RES0 600
RES0 610
RES0 620
RES0 630
RES0 640

```





```

NIT=0
ISTOP=0
CALL DELTAS
UER02=UE
IF (XJFAC.GT.1.D-04) UER02=UE*RO**2
IF (XKFAC.GT.1.D-04) UER02=UE**3
CF1=2.D0*UE*A1B/PNC*EPSVD*DCOS(BODANG)
KKMX1=K+10
KK=K+1
RETURN

WRITE A TAPE WITH NEW SOLUTION DATA

WRITE (20) A0B,A0BP,UN,EPSPL,F2,F2N,F2NN,FC,FCN,FCP,VC,XN,Y,YOVDELRES01100
1,YOVHT,Y,Y,CONVRG,CCRN1,CRNI,DIF,DIFF,NC,CFBAR,CFBREX,CFE,CFINF,CFRES01110
2RES,CFREY,DEL,DELST,DELTA,DSTARK,DSTRAX,HAFCF,REIHT,REX,IHT,DELORES01120
3RF,DELGX,DSAXOR,DSTCOL,DSTORF,DSTICTH,DSTICX,ROREFL,THODEL,THOREF,XORES01130
4REFL,ZORELF,CF1,SUM,A1B,E1,FF,F2N1,VW,CF,DUEDES,PE,PESO,PP,UE,UER02RES01140
5,UESO,PFS,REINF,RHOFS,UFS,DS,DX,DX1,DXMAX,DXOLD
WRITE (20) PNC,RO,REFLEN,SCF,X,XI,XI2,XICLD,XGLD,XJ,XJFAC,Z,ZOL,IERES01160
1,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NIT3,NQSE,II,IPFL,IPRES01170
2RINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,LAMTRB,NITTUT,ADTEST,ETAINFRES01180
3,XKETA,P10,PSTAG,ATR,CHICRT,CHIMAX,GAMPA,XBAR,XIBAR,KTRANS,EPSVD,XRES01190
4K1,XK2,HEDR,CASE,ICARD2,ICARD3,ICARD4,NN,IBDN,BETAS,XSTA,UEZ,PZ,ZARES01200
5,IPR,IPRFL,RZ,KHESS,PREF,PHGREF,UREF,IM,IWT,KTE,KISTTE,XKFAC,KONSERES01210
6T,BETA,A1,A2,A3,A4,CHI,DN2,EPSC,F1,FIN,FINN,XN2,TVC,BODANG,RTVC,RORES01220
7RW,RCRWSQ,RW,UOUPLS,YPLUS,UDEF,UPLUS,KK,ZDELST,RODELS,CDV1,CDV2,XCRES01230
8P,XCP1,CP,CPI,SUM1,SUMT,ROMAX,RHC,MM,XLOCA,DYDX,JSTA,NOPRES
WRITE (6,70)
WRITE (6,80) X,XI,Z,RO,BETA,PP,K
WRITE (21,70)
WRITE (21,80) X,XI,Z,RO,BETA,PP,K

```

C  
C  
C  
30

RES01290  
RES01300  
RES01310  
RES01320  
RES01330  
RES01340  
RES01350  
RES01360  
RFS01370

40           RETURN  
  C  
50           FORMAT (10A6,2X,A6,/13/15/1X,I4,I5/9X,I1)  
60           FORMAT (2F12.6)  
70           FORMAT (10X,45HRESTART TAPE WRITTEN AT X,X1,Z,RO,BETA,PP,K =)  
80           FORMAT (10X,6F10.5,7X,I3)  
90           FORMAT (2F12.6)  
100          FORMAT (10A6,2X,A6/13/15/1X,I4,I5/9X,I1)  
            END





```

      B=(((-2.0+A1(N))*(DN(N)-DN(N-1)))/(DN(N)*DN(N-1))+A2(N))*CRNI+A4(N)/SOLO 330
10S      SOLO 340
      CC=(2.00+A1(N)*DN(N-1))/(DN(N)*(DN(N)+DN(N-1)))*CRNI      SOLO 350
      D=-(W1NN(N)+A1(N)*W1N(N)+A2(N)*W1(N))*(1.00-CRNI)-A3(N)+A4(N)*W1(NSOLO 360
1)/DS      SOLO 370
      F(N)=-CC/(B+A*E(N-1))      SOLO 380
      F(N)=(D-A*F(N-1))/(B+A*E(N-1))      SOLO 390
      W2(IE)=1.00      SOLO 400
      KCN=IM      SOLO 410
      DC 20 N=2,IE      SOLO 420
      W2(KON)=E(KON)*W2(KON+1)+F(KON)      SOLO 430
      KCN=KON-1      SOLO 440
      CALL DERIV3 (W2,XN,IE,1,W2N)      SOLO 450
      CALL DERIV3 (W2N,XN,IE,1,W2NN)      SOLO 460
      RETURN      SOLO 470
      END      SOLO 480

```

10

20





```

C
C
C
40
C
      ..... LINEARLY INTERPOLATE TO FIND CORRESPONDING VALUE OF Z .....
      TLU=Z(I-1)+(XSTAR-X(I-1))*(Z(I)-Z(I-1))/(X(I)-X(I-1))
      RETURN
      END
      TLU0 330
      TLU0 340
      TLU0 350
      TLU0 360
      TLU0 370
      TLU0 380
      TLU0 390

```

```

C
C
C
C
C
C
SUBROUTINE VELDAT
SUBROUTINE VELDAT WRITES OUT THE VELOCITY PROFILE AT THE UP-
STREAM EDGE OF THE NAVIER STOKES REGION TO BE USED AS BOUNDARY
CONDITIONS FOR THE APLNS PROGRAM.
IMPLICIT REAL*8(A-H,O-Z)
COMMON /APLOAT/ XLOCA,DYDX,JSTA,NOPRFS
COMMON /ARRAY1/ AOB(101),AOBP(101),A1(101),A2(101),A3(101),A4(101),VELO
1,CHI(101),DN(102),DN2(102),EPSO(101),EPSPL(101),F1(101),FIN(101),FVELO
21NN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(1VELO
301),XN(102),XN2(102),Y(101),YCVDEL(101),YOVTH(101),YY(101)
COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),Z(501),IPR(101),IPRFL(VELO
1101),RZ(501)
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UEO2,UESO
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLDVELO
1,XJ,XJFAC,Z,ZCL,RQ
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTOP,KL,KVSLAW,NIT,NIT1,NIT2,NITVELO
13,NOSE
COMMON /CCEFF/ CFBAR,CFBEX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,VELO
1DSTARK,DSTARX,HAFCF,RETHET,REX,THET
C
C
IF (X-LT.XSTA(JSTA)) RETURN
DO 10 I=JSTA,IIMAX
IF (X-EQ.XSTA(I)) GO TO 20
CONTINUE
RETURN
XBACK=1.0-XLOCA
DXI=XBACK/NOPRFS
DYI=DYDX*DXI
WRITE (7,40) DYDX,DYI,IE
10
20

```

VELO 330  
VELO 340  
VELO 350  
VELO 360  
VELO 370  
VELO 380  
VELO 390  
VELO 400

```
30      WRITE (7,50) DEL,UE  
      DO 30 I=1,IE  
      WRITE (7,50) YY(I),FC(I)  
      RETURN  
C  
40      FORMAT (2F12.6,13)  
50      FORMAT (2F12.6)  
      END
```



```

SUBROUTINE WRITE1
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE WRITE1 IS CALLED BY MAIN AND SUBROUTINE READIN.

THIS SUBROUTINE PROVIDES THE OUTPUT OF THE INPUT DATA AND THE
INITIALIZED DATA.

COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPFPL(
1101),RZ(501)
COMMON /CONVERG/ CONVRG,CCRN1,CCRN2,DIF,DIFF,NC
COMMON /CUMWLL/ A1B,E1,FF,F2N1,VW
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA,DUEDS,PE,PESO,PP,UE,UE02,UESO
COMMON /FRSTRM/ PFS,REINF,RHOF,UF5
COMMON /GEOME/ DS,DX,DX1,DXMAX,DXOLD,PNC,REFLEN,SCF,X,XI,XI2,XIOLD
1,XJ,XJFAC,Z,ZOL,RO
COMMON /INTGR/ IE,IIMAX,IM,IPRNT,ISTCP,KL,KVSLAW,NIT,NIT1,NIT2,NITWRCO
13,NGSE
COMMON /INTEGER/ II,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTCP,KTRNSN,LWRCO
1AMTRB,NITTOT
COMMON /NMLCRD/ ADTEST,FTAINF,XKETA
COMMON /REF/ PREF,RHOREF,UREF
COMMON /STAG/ P10,PSTAG
COMMON /TRANS/ ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS
COMMON /VSCSTV/ EPSVD,XK1,XK2
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RCRW(101),RORWSQ(101),RW
COMMON /TE/ KTE,KTSTTE
COMMON /WAK/ XKFAC
COMMON /STRTUP/ IREAD,IRSPT,KK,ITER
DATA YES/3HYES/

```

WRCO 10  
 WRCO 20  
 WRCO 30  
 WRCO 40  
 WRCO 50  
 WRCO 60  
 WRCO 70  
 WRCO 80  
 WRCO 90  
 WRCO 100  
 WRCO 110  
 WRCO 120  
 WRCO 130  
 WRCO 140  
 WRCO 150  
 WRCO 160  
 WRCO 170  
 WRCO 180  
 WRCO 190  
 WRCO 200  
 WRCO 210  
 WRCO 220  
 WRCO 230  
 WRCO 240  
 WRCO 250  
 WRCO 260  
 WRCO 270  
 WRCO 280  
 WRCO 290  
 WRCO 300  
 WRCO 310  
 WRCO 320

```

C
WRITE (6,180) ITER
IF (TVCEQ.YES) WRITE (6,170)
WRITE (6,20) NOSE,LAMTRB,KTRANS,KTRNSN,KTE
WRITE (6,30) NIT1,NIT2,NIT3,NC,IE,KEND,IIMAX
WRITE (6,40) KADETA,KL,IPFL,IPRINT,KVSLAW
WRITE (6,50) UFS,REINF
WRITE (6,60) PFS,RHCFS,PSTAG
WRITE (6,70) CHICRT,XBAR,ATR
WRITE (6,80) XK1,XK2
WRITE (6,90) CONVRG,ADTEST,CRNI,XKETA,ETAINF
WRITE (6,100) EPSVD,SCF,REFLEN
WRITE (6,110) XJFAC,XKFAC,BDDANG,DX1,DXMAX
WRITE (6,120) (IPR(J),J=1,IPRINT)
WRITE (6,130) (IPRFL(J),J=1,IPFL)
WRITE (6,140)
DC 10 J=1,IIMAX
WRITE (6,150) J,ZA(J),RZ(J),XSIA(J),PZ(J),UEZ(J)
CONTINUE
WRITE (5,160)
RETURN

10
C
C
C
20
30
40
50
60
FORMAT (1H0,2X,7HNOSE = ,11,11H, LAMTRB = ,11,11H, KTRANS = ,11,11H, KTRNSN = ,13,7H KTE = ,13)
FORMAT (1H0,2X,7HNIT1 = ,12,9H, NIT2 = ,12,9H, NIT3 = ,12,7H, NC = ,12,7H, IE = ,13,9H, KEND = ,13,10H, IIMAX = ,12)
FORMAT (1H0,2X,9HKADETA = ,11,7H, KL = ,11,9H, IPFL = ,13,11H, IPRWROO = ,11)
FORMAT (1H0,2X,6HUFPS = ,F12.6,10H, REINF = ,1PE14.7)
FORMAT (1H0,2X,6HHPFS = ,F12.4,10H, RHCFS = ,1PE13.6,10H, PSTAG = ,1PE14.7)

```

```

WROO 330
WROO 340
WROO 350
WROO 360
WROO 370
WROO 380
WROO 390
WROO 400
WROO 410
WROO 420
WROO 430
WROO 440
WROO 450
WROO 460
WROO 470
WROO 480
WROO 490
WROO 500
WROO 510
WROO 520
WROO 530
WROO 540
WROO 550
WROO 560
WROO 570
WROO 580
WROO 590
WROO 600
WROO 610
WROO 620
WROO 630
WROO 640

```

```

70      10PF12.4)
      FORMAT (1H0,2X,10HCHICRIT = ,F12.3,9H, XBAR = ,F12.6,8H, ATR = ,F1WROO 650
12.6)
      WROO 660
      WROO 670
80      FORMAT (1H0,2X,6HXX1 = ,F7.4,8H, XK2 = ,F9.6)
      WROO 680
90      FORMAT (1H0,2X,9HCUNVRG = ,F7.4,11H, ADTEST = ,F7.4,9H, CRNI = ,F7WROO 690
      WROO 700
100     1.4,10H, XKETA = ,F7.4,11H, ETAINF = ,F7.2)
      FORMAT (1H0,2X,8HEPSVD = ,F12.6,17H, SCALE FACTOR = ,F9.5,21H, REFWRROO 710
      WROO 720
110     IERENCE LENGTH = ,F9.4)
      FORMAT (1H0,2X,8HXJFAC = ,F7.4,2X,8HXKFAC = ,F7.4,10H, ANGLE = ,F9WROO 730
      WROO 740
120     1.6,7H DX = ,F7.4,10H, DXMAX = ,F7.4)
      WROO 750
130     FORMAT (1H0,3X,3HIPR,4X,2015,/(11X,2015/))
      WROO 760
140     FORMAT (1H0,3X,5HIPRFL,2X,2015,/(11X,2015/))
      WROO 770
      FORMAT (1H0,3X,14HAXIAL POSITION,14X,2HZA,13X,2HRZ,12X,4HXSTA,10X,WROO 780
      WROO 790
150     12HPZ,13X,3HUEZ/)
      WROO 800
160     FORMAT (9X,13,10X,5F15.6)
      WROO 810
170     FORMAT (1H0)
      WROO 820
180     FORMAT (43X,46HTHIS RUN INCLUDES TRANSVERSE CURVATURE EFFECTS////)WROO 830
      WROO 840
      END

```



```

SUBROUTINE WRITE2
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE WRITE2 CALLS SUBROUTINE READIN.

SUBROUTINE WRITE2 IS CALLED BY MAIN AND SUBROUTINE READIN.

THIS SUBROUTINE CONTROLS THE OUTPUT AFTER A CONVERGED SOLUTION IS
OBTAINED.
COMPLETE SOLUTIONS ARE WRITTEN ONLY AT SELECTED VALUES OF X,
I. E. AT X=XSTA(IPRFL), AND AT STATIONS INCREMENTED BY IMT.
ALL OTHER COMPUTED RESULTS ARE WRITTEN FOR EVERY VALUE OF X AT
WHICH A SOLUTION IS OBTAINED.

COMMON /ARPA1/ A08(101),A08P(101),A1(101),A2(101),A3(101),A4(101)
1,CHI(101),DN(102),DN2(102),EPSU(101),EPSPL(101),F1(101),FIN(101),FWRIO 10
21VN(101),F2(101),F2N(101),F2NN(101),FC(101),FCN(101),FCP(101),VC(1WRIO 20
301),XN(102),XN2(102),Y(101),YCVDEL(101),YDVTH(101),YY(101)
COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(WRIO 30
101),RZ(501)
COMMON /COEFF/ CFBAR,CFBEX,CFE,CFINF,CFRES,CFREY,DEL,DELST,DELTA,WRIO 210
10STAR, DSTARX, HAFCF, REIHET, REX, THET
COMMON /COEFF2/ DELGRF, DELGX, DSAXGR, DSTCOL, DSTORF, DSTOTH, DSTOX, RGRWRIO 230
1EFL, THUDEL, THOREF, XGREFL, ZGREFL
COMMON /COEFF3/ CFI, SUM, SUM1, SUMT
COMMON /COMWLL/ A19, EI, FF, F2N1, VM
COMMON /CFPR/ CF
COMMON /EDGPRP/ BETA, DUEDS, PE, PESO, PP, UE, UERO2, UESO
COMMON /GEOME/ DS, DX, DX1, DXMAX, DXOLD, PNC, REFLEN, SCF, X, XI, XI2, XIULDWRIO 300
1, XJ, XJFAC, Z, ZOL, RO
COMMON /INTGR/ IE, IIMAX, IM, IPRNT, ISTOP, KL, KVSLOW, NIT, NIT1, NIT2, NITWRIO 320

```

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

```

13,NOSE
COMMON /NTEGER/ II,IPFL,IPRINT,JJ,K,KADETA,KEND,KEP,KSTOP,KTRNSN,L
1AMTRB,NITTOI
COMMON /TRANS/ ATR,CHICRT,CHIMAX,GAMMA,XBAR,XIBAR,KTRANS
COMMON /VSCSTV/ EPSVD,XK1,XK2
COMMON /STAG/ P10,PSTAG,RHO
COMMON /REF/ PREF,RHOREF,UREF
COMMON /FRSTRM/ PFS,REINF,RHOFS,UFS
COMMON /TVCURV/ TVC,BODANG,RTVC(101),RORW(101),RORWSQ(101),RW
COMMON /WTE/ IW,IWT
COMMON /LWALL/ UOUPLS(101),YPLUS(101),UDEF(101),UPLUS
COMMON /TE/ KTE,KTSTTE
COMMON /HESS/ IWRTH,ICARD2,ICARD3,ICARD4,NN,IBDN,HEDR(10),CASE,KHEW
1SS
COMMON /BDLOOR/ ZDELST(501),RODELS(501),ZCLD(501),RCLD(501),MM
COMMON /STRUP/ IREAD,IRSRT,KK,ITER
COMMON /DRAG/ CDV1,CDV2,XCP,XCPI
COMMON /WKPRL/ RSTAR
C
DIMENSION TPR(102), XMAL(102), PITOT(101), PITOTR(101)
DIMENSION VORTI(101)
C
EQUIVALENCE (TPR(1),DN2(1))
EQUIVALENCE (XMAL(1),XN2(1)), (PITOT(1),EPSO(1)), (PITOTR(1),AI(1))
1)
C
ABS(X)=DABS(X)
C
IF (KHESS.EQ.0) GO TO 30
C
WF IS WEIGHTING FACTOR FOR DAMPING BODY COOR ITERATIONS
C

```

WRIO 330  
 WRIO 340  
 WRIO 350  
 WRIO 360  
 WRIO 370  
 WRIO 380  
 WRIO 390  
 WRIO 400  
 WRIO 410  
 WRIO 420  
 WRIO 430  
 WRIO 440  
 KHEW  
 WRIO 450  
 WRIO 460  
 WRIO 470  
 WRIO 480  
 WRIO 490  
 WRIO 500  
 WRIO 510  
 WRIO 520  
 WRIO 530  
 WRIO 540  
 WRIO 550  
 WRIO 560  
 WRIO 570  
 WRIO 580  
 WRIO 590  
 WRIO 600  
 WRIO 610  
 WRIO 620  
 WRIO 630  
 WRIO 640

```

10  WF=0.500
    IF (IWRTH.EQ.0) GO TO 30
    IF (K.GE.2) GO TO 10
    WRITE (3,290) HEDR,CASE,ICARD2,ICARD3,ICARD4,NN,IBDN
    MM=0
    THETA=BODANG
    MV=MM+1
    ROELS(MM)=RO+DELST*DCOS(THETA)
    ZDELST(MM)=Z-DELST*DSIN(THETA)
    IF (ITER.EQ.1) GO TO 20
    ZDELST(MM)=(1.00-WF)*ZOLD(MM)+WF*ZDELST(MM)
    ROELS(MM)=(1.00-WF)*ROLD(MM)+WF*ROELS(MM)
    WRITE (3,280) ZDELST(MM),ROELS(MM)
    IWRTH=0
    XBLANK=0.0
    WRITE (6,130) X,XI,Z,RO,BETA,PP,NIT,K
    WRITE (6,140) UE,PE,DUECS,CF,EPSVD,KFP,NITTOT
    WRITE (6,150) F2N(1),F2N(3),F2NN(1),F2NN(3),UPLUS
    IF (X.EQ.XSTA(1)) GO TO 60
    WRITE (6,160) CHIMAX,GAMMA,XIPAR
    WRITE (6,170) REX
    IF (KTSITE.GT.0) GO TO 40
    WRITE (6,180) CFE,CFINF,CFBAR,CFBRES,CFREY
    TAUW=CFINF*RHCF*UFS**2/2.0/144.0
    WRITE (6,190) HAFCF,TAUW
    CCNTINUE
    WRITE (6,200) XCREFL,ZCREFL,RUREFL,DELTX,DSTOX
    WRITE (6,210) THOKEF,DSTORF,DELORF,DSAXCR
    WRITE (6,220) THODEL,DSTODL,DSTOTH,DSTRAX
    WRITE (6,230) DSTARK,DELST,DEL,THET,RETHET
    ANG=BODANG
    BOYANG=ANG*180.000/DARCCS(-1.000)
20
30
40
    WRIO 650
    WRIO 660
    WRIO 670
    WRIO 680
    WRIO 690
    WRIO 700
    WRIO 710
    WRIO 720
    WRIO 730
    WRIO 740
    WRIO 750
    WRIO 760
    WRIO 770
    WRIO 780
    WRIO 790
    WRIO 800
    WRIO 810
    WRIO 820
    WRIO 830
    WRIO 840
    WRIO 850
    WRIO 860
    WRIO 870
    WRIO 880
    WRIO 890
    WRIO 900
    WRIO 910
    WRIO 920
    WRIO 930
    WRIO 940
    WRIO 950
    WRIO 960

```



```

WRITE (6,270) RDYANG
IF (KHESS.EQ.0) GO TO 50
WRITE (6,300) SUM,SUM1,SUMT,XCP,XCP1
IF (KTSTTE.LT.1) GO TO 60
WRITE (6,310) RSTAR
CONTINUE
REF=RO+DELST
IF (K.EQ.1) GO TO 30
DL 70 NM=1,IPRINT
IF (X.EQ.XSTA(IPRFL(NM))) GO TO 80
CONTINUE
IF (ABS(1.0-X/XSTA(KTRNSN)).LE.1.E-6) GO TO 80
IW=IW+1
IF (IW.LE.INT) GO TO 120
IW=1
CONTINUE
UFAC=UE*UFS
DO 90 N=1,IE
PITOT(N)=PI0+.500*UE**2*(F2(N)**2-1.00)
CONTINUE
WRITE (6,240)
DO 100 N=1,IE,KL
WRITE (6,250) XN(N),YY(N),YCVTHT(N),YQVDEL(N),FC(N),FCN(N),YPLUS(N)
1),UOUPLS(N),UDEF(N),EPSPL(N),PITOT(N),N
WRITE (6,260)
IF (X.LT.XSTA(N).OR.X.GT.XSTA(N)) GO TO 120
DO 110 I=1,IE
VORT1(I)=FIN(I)*RIVC(I)*UF**2/DSQRT(2.00*X1)
WRITE (10) (VORT1(I),YY(I),I=1,IE)
CONTINUE
IF (K.NE.1) IPRNT=IPRNT+1
IF (X.EQ.XSTA(IRSRT)) CALL RSTAR

```

WR10 970  
 WR10 980  
 WR10 990  
 WR101000  
 WR101010  
 WR101020  
 WR101030  
 WR101040  
 WR101050  
 WR101060  
 WR101070  
 WR101080  
 WR101090  
 WR101100  
 WR101110  
 WR101120  
 WR101130  
 WR101140  
 WR101150  
 WR101160  
 WR101170  
 WR101180  
 WR101190  
 WR101200  
 WR101210  
 WR101220  
 WR101230  
 WR101240  
 WR101250  
 WR101260  
 WR101270  
 WR101280

```

C
C
C
130  RETURN
      FORMAT (1H0,2X,3HS =,F10.5,1H,/16X,6H XI =,E10.4,5H, Z =,F9.5,6H,WRI01330
1 RO =,F8.5,8H, BETA =,F9.5,6H, PP =,F12.5,8H, NIT = ,13,5H, K =,13,WRI01340
2)
      WRI01350
140  FORMAT (1H0,2X,4HUE =,F8.5,6H, PE =,F11.5,9H, OUEDS =,F11.5,6H, CFWR01360
      WRI01370
150  1 =,F11.5,9H, EPSVD =,E13.6,7H, KEP =,13,10H, NITOT =,15)
      WRI01380
      FORMAT (1H0,2X,8HF2N(1) =,F12.6,10H, F2N(3) =,F12.6,11H, F2NN(1) =WPI01390
1, F12.6,11H, F2NN(3) =,F12.6,10H, UPLUS = ,E13.6)
      WRI01390
160  FORMAT (1H0,2X,8HCHIMAX =,1PE13.6,9H, GAMMA =,E13.6,9H, XIBAR =,E1WRI01400
13.6)
      WRI01410
170  FORMAT (1H0,2X,5HREX =,1PE12.5)
      WRI01420
180  FORMAT (1H0,2X,5HCFE =,1PE13.6,9H, CFINF =,E13.6,13H, CF(TOTAL) =,WPI01430
      IE13.6,19H, CFBAR*SQRT(REX) =,E13.6,19H, CFINF*SQRT(REX) =,E13.6) WRI01440
190  FORMAT (1H0,2X,9HCFINF/2 =,1PE13.6,8H, TAUW =,E13.6,7H P.S.I.) WRI01450
200  FORMAT (1H0,2X,10HX/REFLEN =,1PE13.6,12H, Z/REFLEN =,E13.6,13H, ROWRI01460
      I/REFLEN =,E13.6,11H, DELTA/X =,E13.6,12H, DELSTR/X =,E13.6) WRI01470
210  FORMAT (1H0,2X,14HTHETA/REFLEN =,1PE13.6,17H, DELSTR/REFLEN =,E13.WRI01480
16,16H, DELTA/REFLEN =,E13.6,20H, DELSTRAXI/REFLEN =,E13.6) WRI01490
220  FORMAT (1H0,2X,13HTHETA/DELTA =,1PE13.6,16H, DELSTR/DELTA =,E13.6,WRI01500
116H, DELSTR/THETA =,E13.6,13H, DELSTRAXI =,E13.6) WRI01510
230  FORMAT (1H0,2X,9HDELSTRK =,1PE12.5,10H, DELSTR =,E12.5,9H, DELTA =WRI01520
1,E12.5,9H, THETA =,E12.5,11H, RETHETA =,E12.5) WRI01530
240  FORMAT (1H0,75X,3HETA,8X,1HY,7X,7HY/THETA,4X,7HY/DELTA,5X,6HF=U/UEWRI01540
1,5X,5HFP(N),6X,5HYPLUS,6X,7HU/UPLUS,5X,4HUDEF,6X,4HEPS+,8X,5HPITOTWRI01550
2,6X,1HN/) WRI01560
250  FORMAT (F11.6,10F11.6,14)
260  FORMAT (1X,/)
270  FORMAT (1H0,2X,19HLCCAL BODY ANGLE = ,E12.6///)
280  FORMAT (2F12.6)

```

```
290  FORMAT (10A6,2X,A6/I3/I5/I1X,I4,I5/9X,I1)  
300  FCRMAT (3X,8H   CDF =,F12.6,8H   CDP =,F12.6,7H  
310  1 CP =,F12.6,8H   CPI =,F12.6)  
    FCRMAT (10X,7HRSTAR =,F12.6)  
    END  
WRI01610  
WRI01620  
WRI01630  
WRI01640  
WRI01650
```



```

SUBROUTINE ZR0 (JJ,X2,Z,R0)
IMPLICIT REAL*8(A-H,O-Z)

SUBROUTINE ZR0 CALLS SUBROUTINE INTER5

SUBROUTINE ZR0 IS CALLED BY SUBROUTINES BLUNT2 AND CONE2.

SUBROUTINE ZR0 CALCULATES FOR AXISYMMETRIC FLOW AN AXIAL DISTANCE
Z AND A RADIUS R0 CORRESPONDING TO A SURFACE DISTANCE X2.

COMMON /ARRAY2/ PZ(501),UEZ(501),XSTA(501),ZA(501),IPR(101),IPRFL(
101),RZ(501)

J=0
J=J+1
IF (X2.GT.XSTA(J)) GO TO 10
IF (J.LT.3) J=3
IF (J.GT.(JJ-2)) J=JJ-2
CALL INTER5 (X2,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),RZ
1(J-2),RZ(J-1),RZ(J),RZ(J+1),RZ(J+2),R0)
CALL INTER5 (X2,XSTA(J-2),XSTA(J-1),XSTA(J),XSTA(J+1),XSTA(J+2),Z
1(J-2),ZA(J-1),ZA(J),ZA(J+1),ZA(J+2),Z)
RETURN
END

```

TABLE 4.1 FIELD EXEC

```

&CONTROL ALL
GLOBAL TXLIB FORTLIB
FI 06 DISK HESS COORDATA B (LRECL 80 BLKSIZE 80 RECFM FB)
FI 07 TERM
FI 04 DISK INTER DATA B (LRECL 80 BLKSIZE 80 RECFM FB)
FI 05 DISK HESSLI DATA E (LRECL 80 BLKSIZE 80 RECFM FB)
FI 02 DISK HESS PARMDATA E (LRECL 80 BLKSIZE 80 RECFM FB)
LGAD DATFIELD (NO)MAP
START

```

TABLE 4.2 DEVELOP EXEC

```

&CONTROL ALL
GLOOP -LAREL &1
EXEC FIELD
EXEC HESSLI HESS COORDATA B

```

-LABEL &amp;CONTINUE

TABLE 4.3 DATFIELD FORTRAN

C	DIMENSION X(30,60), Y(30,60), HEDR(15), XB(501), YB(501)	DAT00010
C	READ IN DISPLACED BODY COORDINATES	DAT00020
C	READ (5,10) HEDR, CASE, ICARD2, ICARD3, ICARD4, NP, IBDN	DAT00030
C	READ(5,80)	DAT00040
C	DO 6 I=1, NN	DAT00050
	6 READ (5,20) XB(I),YB(I)	DAT00060
	DATA NB/1/,NNU/0/,NCF/0/,NAXI/1/,NOFF/1/,IGEOMF/0/,ISIGF/1/,ICURVDAT00090	DAT00070
	IN/J/,NONEWF/0/,IFCRMT/1/,IIBDN/0/,NNI/360/	DAT00080
C	WRITE OUT HESS DATA SET FOR EXECUTION WITH OFF BODY POINTS	DAT00100
C	WRITE (6,70) HEDR, CASE	DAT00110
C	WRITE (6,30) NB,NNU,NAXI,NCF,NOFF	DAT00120
	WRITE (6,30)	DAT00130
	WRITE (6,40) ICEOMF,ISIGF,ICURVN,NONEWF,IFORMT,NV	DAT00140
	WRITE (6,50) IBDN	DAT00150
	WRITE (6,20) (XB(I),YB(I),I=1,NN)	DAT00160
	WRITE (6,40) ICEOMF,ISIGF,ICURVN,NONEWF,IFORMT,NNI	DAT00170
	WRITE (6,50) IIBDN	DAT00180
		DAT00190
		DAT00200
		DAT00210



```

C      READ IN THE ITERATION DATA
C
C      READ (4,40) IHESI
C      READ (4,60) XLCCAT,DX,DY
C
C      M IS THE UPPER MOST ROW OF OFF BODY PCINTS
C      ITERATION. K IS THE BOTTOM MOST ROW.
C
C      M = IHESI*6
C      K = M-5
C      YS = DY*(K-1)
C      DO 1 I=K,M
C      XS = XLCCAT
C      DO 3 J=1,60
C      Y(I,J) = YS
C      X(I,J) = XS
C      WRITE (6,20) X(I,J), Y(I,J)
C      3 XS = XS+DX
C      1 YS = YS+DY
C      IHESI = IHESI+1
C
C      REWIND FILE WITH REPITI
C
C      REWIND 4
C      WRITE (4,40) IHESI
C      WRITE (4,60) XLCCAT,DX,DY
C      10 FORMAT (15A4,2X,A4/13/15/1X,I4,I5/9X,I1)
C      20 FORMAT (2F12.6)
C      30 FORMAT (5I1)
C      40 FORMAT (5I1,I5)
C      50 FORMAT (9X,I1)

```

```

DAT00220
DAT00230
DAT00240
DAT00250
DAT00260
DAT00270
DAT00280
DAT00290
DAT00300
DAT00310
DAT00320
DAT00330
DAT00340
DAT00350
DAT00360
DAT00370
DAT00380
DAT00390
DAT00400
DAT00410
DAT00420
DAT00430
DAT00440
DAT00450
DAT00460
DAT00470
DAT00480
DAT00490
DAT00500
DAT00510
DAT00520
DAT00530

```

DAT00540  
DAT00550  
DAT00560  
DAT00570  
DAT00580

60 FORMAT (3F12.6)  
70 FORMAT (15A4,2X,A4)  
90 FORMAT(/)  
STOP  
END

TABLE 5.1 APLNS EXEC

```

&CONTROL ALL
GLOBAL TXTLIB FORTXLIB
FI 5 DISK &1 &2 &3
FI 08 DISK STREAM DATA E (RECF4 FR BLOCK 87 LRECL 87
FI 11 DISK APLNS VELDATA1 E
TESTBAT
&RC = &RETCODE
&IF &RC EQ 0 FI 06 DISK APLNS OUTPUT E
&IF &RC NE 0 FI 06 PRINTER
LOAD NSTIDY PLTCAPLN ( CLEAR NOMAP
START

```

TABLE 5.2 APLNS FORTRAN

```

CALL DRFX6
STOP
END

```





```

*   EPG, THRUST
COMMON /ARRAYS/ PSI,XI,V,U,VA,UA,PSIB,XIB,XIW,EPA(60), UI(60),
*   UIO(60), PSIO(60)
COMMON /INTEGS/ L,L1,JDEL,M,M1,NTS,NFR,PSKP,IDIMY,JDIMY,JCI,IO
COMMON /IRRAYS/ LAR(60)
COMMON /LOGICS/ LSWH1, PRNT, GN, OFF, RSTART, SAVE, SWHFX,
*   ZSTART, CSTART
DIMENSIONS ARE SET UP FOR MAXIMUMS OF L=30, M=60, L1=15 & M1=15

DIMENSION PSI(60,30), PSIR(60,30), XI(60,30), V(60,30), U(60,30)
DIMENSION XIA(60,30), XIB(60,30), VA(60,30), UA(60,30)
DIMENSION A(1624,3), B(1624), XL(3248)
DIMENSION XIW(15), AA(30),BB(30),CC(30), YY(30,60)
DIMENSION UO(30), Y(30), X(60), FX(15), FXRHC(15), DFRDDR(15)
INTEGER TS, ITS, PSKP
COMMON INDR
INTEGER JHDR(6)
DATA JHDR / 'OPSI','O XI','O V','O U','OXIA','OXIB' /
DATA IPSIR /4HOPSR/
LOGICAL LSWH1, PRNT, GN, OFF, SWHFX
LOGICAL RSTART, SAVE, ZSTART, CSTART
DIMENSION PSWI(15,15), PSW(15), AI(15), AS(15,15)
EQUIVALENCE (A(1),AS(1))

DATA ZERO,ONE,TWO,THREE,FOUR/0.000,1.000,2.000,3.000,4.000/

DATA IA,IB,IDIMY,JDIMY / 1624, 1624, 60, 30 /
DATA IA,IB / 1624, 1624 /
DATA NLC,NUC, MB, IJCB / 1,1,1,0 /
DATA INCE / 0 /
DLOG2(X) = DLOG(X) / DLOG2

```

01021  
01022  
01023  
01024  
01025  
01026  
01027  
01028  
01029  
01030  
01031

01035  
01037  
01038

01039  
01041

C  
C

C  
C  
C

C

```

99 FORMAT(2X,1P10G12.4)
IF(INCE.EQ.1) GO TO 1000
PRINT 1
1 FORMAT('0**01/20/77   W O R K 6   WITH EPO')
INCE=1

C
C
EPO = 18.900D-05
PRINT 6, EPO
6 FORMAT(' EPO = ',1PG16.7)

C
C
DLG2 = DLOG(TWO)
MPI1 = M1+1
MM1 = M-1
MM2 = M-2
MM3 = M-3
LM1 = L-1
LM2 = L-2
LM3 = L-3
LIM1 = L1 - 1
LIM2 = L1 - 2
N = LM2*MM2
R = LM2
IDIMW = 2*LM2 + 4*MM2 + MM2*(DLOG2(R) + 1) + 1
43 FORMAT('HERE IS N, IDIMY AND IDIMW (MAX DIM FOR NW)',/318)
PRINT 43, N, IDIMY, IDIMW
DT2 = DT / TWO
DX2 = DX*DX
FDX2 = FOUR * DX2
DY2 = DY*DY
DY3 = DY2 * DY
RYX2 = DY2/DX2
RXY2 = DX2 / DY2

```

01040  
 01085  
 01086  
 01087  
 01088  
 01089  
 01090  
 01091  
 01092  
 01093  
 01094  
 01095  
 01096  
 01097  
 01098  
 01099  
 01100  
  
 01101  
 01102  
 01103  
 01104



01105  
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01110  
01135  
01136  
01137  
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01139  
01140

01141

\*/

```

TDY = TWO * DY
TDX = TWO * DX
DO 45 I=1,60
DO 45 J=1,30
XIA(I,J)=ZERO
XIB(I,J)=ZERO
PSIB(I,J)=ZERO
45 CONTINUE
DO 44 J=1,L
44 XIA(I,J)=XI(1,J) /* XI AT THE WALL FOR I=2 TO M1
XIW = 0;
DO 50 I=1,M1
50 XIW(I) = ZERO

C
C
DXT = DX2 / TDY
DO 51 J=1,LMI
T = DXT / Y(J+1)
AA(J) = RXY2 + T
CC(J) = RXY2 - T
51 BB(J) = -TWO * RXY2
AA(LMI) = AA(LMI) + CC(LMI)
CC(LMI) = ZERO

C
NS = JCI-2
IAS = 15
IDGT = 0
MIMI = MI-1
DO 40 I=2,MIMI
PRINT 2, I
2 FOR MAT(,OI= ,I4,, PSWI(K,I),K=2,MIMI)
DO 41 IP=1,LMI
DO 41 JP=1,MIM2

```

```

41      YY(IP,JP) = ZERO
      LJ = LAR(I)-1
      IF(LJ .LE. 0) GO TO 40
C
      YY(LJ,I-1) = ONE
      IHDR = MASK
C      IF(I .EQ. 4) CALL DMTD10(VY, LM1, MM2, L, M)
      CALL PCIS2(MM2,L,1,AA,BB,CC,JDIMY,VY,XL)
C      IF(I .EQ. 4) CALL DMTD10(VY, LM1, MM2, L, M)
C
      DO 42 K=2,MIM1
      LJ = LAR(K)-1
      IF(LJ .LE. 0) GO TO 40
      PSWI(K,I) = YY(LJ, K-1)
C      PRINT 99, (PSWI(K,I),K=2,MIM1)
      40 CONTINUE
      1000 CONTINUE
      NC = 0
      DO 88 J= 2,LM1
      DO 87 I=2,MM1
      EDD = EPA(I)/DX2
      EDC = (EPA(I+1)-EPA(I-1))/FDCX2
      LJ = LAR(I) + 1
      IF(I .LT. LJ) GO TO 87
      NC = NC+1
      A(NC,3) = U(I,J)/ TDY - EDD - EDC
      A(NC,2) = TWO/DT + (TWO*EPA(I))/DX2
      A(NC,1) = -U(I,J)/ TDY - EDD + EDC
      B(NC) = EPA(I)*((XI(I,J+1)-2*XI(I,J)+XI(I,J-1))/DY2
      *      + (XI(I,J+1)-XI(I,J-1))/TDY/V(J)-XI(I,J)/Y(J)**2)
      *      - V(I,J) * (XI(I,J+1)-XI(I,J-1))/TDY
      *      + XI(I,J) / DT2 + V(I,J) * XI(I,J) / Y(J)

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```

C      B(NC) = B(NC) - (EPA(I+1)-EPA(I-1))/TDX * (
1      (V(I,J+1) - TWO*V(I,J) + V(I,J-1))/DY2 +
2      (V(I,J+1) - V(I,J-1)) / TDY / Y(J) +
3      (V(I+1,J) - TWO*V(I,J) + V(I-1,J))/DX2 - V(I,J)/Y(J)**2) -
4      (EPA(I+1) - TWO*EPA(I) + EPA(I-1))/DX2 * (
5      (U(I,J+1)-U(I,J-1))/TDY + (V(I+1,J)-V(I-1,J))/TDX )
C
C      ***** FOR EPS( Y ) *****
C      IF(EPO .EQ. ZERO) GO TO 93
C      IF( I .GT. M1) GO TO 93
C      IF( J .NE. LJ) GO TO 93
C
C      B(NC) = B(NC) + (EPA(I)-EPO)/TDY * ( (U(I,J+1)-TWO*U(I,J)+
1      U(I,J-1))/DY2 + (U(I,J+1)-U(I,J-1))/TWO/DY2/(LJ-1) +
2      (U(I+1,J)-TWO*U(I,J)+U(I-1,J))/DX2 +
3      (XI(I,J+1)-XI(I,J-1))/TDY
4      ) +
5      (EPA(I)-TWO*EPA(I)+EPO)/DY2 *
6      ( (U(I,J+1)-U(I,J-1))/TDY + (V(I+1,J)-V(I-1,J))/TDX )
7      + (EPO-EPA(I))/DY/DX *
8      ( (U(I+1,J)-U(I-1,J))/TDX - (V(I,J+1)-V(I,J-1))/TDY )
93 CONTINUE
C
C      DETERMINATION OF THE LOCATION OF THE PROPELLER(S)
C
C      IF((I.NE.M1).AND.(I.NE.M1P1)) GO TO 94
C      IF(I.NE.M1) GO TO 94
C      IF(J .LE. L1) B(NC) = B(NC) + DFRCOR(J)
94 IF(I .NE. 2) GO TO 95
C      ALONG AB
C      B(NC) = B(NC) - A(NC,1)*XI(1,J)
01291
01292
01293

```



```

          A(NC,1) = ZERO
95 CONTINUE
  IF( I .NE. MM1) GO TO 86
  C      ALONG      CD
          A(NC,1) = A(NC,1) - A(NC,3)
          A(NC,2) = A(NC,2) + TWO*A(NC,3)
          A(NC,3) = ZERO
36 CONTINUE
  IF( I .GT. M1) GO TO 87
  IF( J .NE. LJ) GO TO 87
  C      ALONG      EF
          B(NC) = B(NC) - A(NC,1)*XI(1,J)
          A(NC,1) = ZERO
87 CONTINUE
88 CONTINUE
  C
  N=NC
  CALL LEQTB(A,N,NLC,NUC,IA,B,MB,IB,IJOB,XL,IER)
  C
  IF( IER .NE. 0) PRINT 22, IER
22 FORMAT('O***ERROR 1ST LEQTB: IER= ',I5)
  NC = 0
  DO 96 J= 2,LM1
  C      XIA(1,J) = XI(1,J)
  DO 89 I=2,MM1
  LJ = LAR(I)+1
  IF( J .LT. LJ) GO TO 89
  NC = NC + 1
  XIA(1,J) = B(NC)
89 CONTINUE
96 CONTINUE
  C

```

\*\*\*DONE UP ABOVE

01294  
0129501297  
01298  
0129901300  
0130101302  
01303  
01304  
01305  
0130601310  
01311  
01312

```

01313      DC 97 I=1,M
          LJ=LAR(I)
          XIA(I,LJ) = XI(I,LJ)
          XIA(I,L) = ZERO
          97 CONTINUE
          C
          NEW ALONG CD -->
          DC 98 J=2,LM1
          98 XIA(M,J) = 2*XIA(MM1,J) - XIA(MM2,J)
          IHDR = JHDR(5)
          -----
          C
          C
          IF (TS .GT. 1) GO TO 175
          FOR TS=1
            DTA = DT
            DO 170 I=1,M
            DO 170 J=1,L
              UA(I,J) = U(I,J)
              VA(I,J) = V(I,J)
            CONTINUE
          170 GO TO 200
          C
          FOR TS NOT 1
          175 CONTINUE
              TMP = DT/(DTA*TWO)
              DO 180 I=1,M
              DO 180 J=1,L
                JA(I,J) = UA(I,J) + (U(I,J)-UA(I,J)) * TMP
                VA(I,J) = VA(I,J) + (V(I,J)-VA(I,J)) * TMP
              CONTINUE
          180
          C
          200 CONTINUE
              NC=0
              DC 110 I=2,MM1

```

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```

EOD = EPA(I)/DY2
LJ = LAR(I)+1
DG 110 J=LJ,LM1
NC = NC+1
T = EPA(I) / TDY / Y(J)
A(NC,3) = VA(I,J)/ TDY - EOD - T
A(NC,2) = TWO/DT + (TWC*EPA(I))/DY2
A(NC,1) = -VA(I,J)/ TDY - EOD + T

C
B(NC) = EPA(I)*((XIA(I+1,J)-2*XIA(I,J)+XIA(I-1,J))/DX2
* - XIA(I,J)/Y(J)**2)
* - UA(I,J) * (XIA(I+1,J)-XIA(I-1,J))/TDX
* + XIA(I,J) / DT2 + VA(I,J) * XIA(I,J) / Y(J)

C
B(NC)=B(NC)+(EPA(I+1)-EPA(I-1))/TDX *(XIA(I+1,J)-XIA(I-1,J))/TDX
1 - (EPA(I+1)-EPA(I-1))/TDX * (
2 (VA(I,J+1) - TWO*VA(I,J) + VA(I,J-1))/DY2 +
3 (VA(I,J+1) - VA(I,J-1)) / TDY / Y(J) +
4 (VA(I+1,J) - TWO*VA(I,J) + VA(I-1,J))/DX2 - VA(I,J)/Y(J)**2) -
5 (EPA(I+1) - TWO*EPA(I) + EPA(I-1))/DX2 * (
6 (UA(I,J+1)-UA(I,J-1))/TDY + (VA(I+1,J)-VA(I-1,J))/TDX )

C
***** FOR EPS( Y ) *****
IF(EPO .EQ. ZERO) GO TO 193
IF( J .NE. LJ) GO TO 193
IF( I .GT. M1) GO TO 193
A(NC,1) = A(NC,1) + (EPA(I)-EPO)/4.0D0/DY2
A(NC,3) = A(NC,3) - (EPA(I)-EPO)/4.0D0/DY2
B(NC) = B(NC) + (EPA(I)-EPO)/TDY * ( (UA(I,J+1)-TWO*UA(I,J)+
1 UA(I,J-1))/DY2 + (UA(I,J+1)-UA(I,J-1))/TWC/DY2/(LJ-1) +
2 (UA(I+1,J)-TWO*UA(I,J)+UA(I-1,J))/DX2 ) +
5 (EPA(I)-TWO*EPA(I)+EPO)/DY2 *

```

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```

6      ( (UA(I,J+1)-UA(I,J-1))/TDY + (VA(I+1,J)-VA(I-1,J))/TDX )
7      + (EPO-EPA(I))/DY/DX *
8      ( (UA(I+1,J)-UA(I-1,J))/TDX - (VA(I,J+1)-VA(I,J-1))/TDY )
C
193 CONTINUE
C
C      IF((I.NE.M1).AND.(I.NE.M1P1)) GO TO 102
C      IF(I.NE.M1) GO TO 102
C      IF(J.LE.L1) B(NC) = B(NC) + DFRCDR(J)
C
102 CONTINUE
C      IF( J.NE. LJ) GO TO 104
C      B(NC) = B(NC) - A(NC,1) * XIA(I,LJ-1)
C      A(NC,1) = ZERO
C
104 CONTINUE
C      IF(J.NE. LM1) GO TO 106
C      B(NC,1) = B(NC,1) - A(NC,1) * 0.3      IE TOP WALL
C      A(NC,3) = ZERO
C      */
C
106 CONTINUE
110 CONTINUE
C
N = NC
CALL LEQT18(A,N,NLC,NUC,IA,B,MB,IB,IJCP,XL,IER)
C
IF(IER.NE.0) PRINT 46,IER
46 FORMAT('O***ERROR ***2ND LEQT18:  IER= ',I4)
C
NC = 0
DO 120 I=2,MM1
LJ = LAR(I)+1
XIB(I,LJ-1) = XI(I,LJ-1)
DO 120 J=LJ,LM1
NC = NC+1

```

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01375  
01376  
01377

01380

```

      XIB(I,J) = B(NC)
120 CONTINUE
C
      DO 122 I=1,M
122 XIB(I,L) = ZERO
      DO 124 J=1,L
124 XIB(I,J) = XI(I,J)
      NOW ALONG CD-->
      DO 126 J=2,LM1
126 XIB(M,J) = TWO*XIB(MM1,J) - XIB(MM2,J)
      XIB(M,1) = ZERO
C
      IHDR = JHDR(6)
C
C -----
C DEL_SQUARE PSI = XI(X,Y) A LA EHRlich IE. CD
C FIRST SOLVE ALONG THE RHS OF THE REGION.
C BUT NOT THE END POINTS
C
      DO 205 J=1,LM2
      T = DY/TWO/Y(J+1)
      A(J,3) = ONE - T
      A(J,2) = -TWO
      A(J,1) = ONE + T
      B(J) = DY2 * XIB(M,J+1) * Y(J+1)
205 CONTINUE
C
      T = DY / TWO / Y(LM1)
      A(1,1) = ZERO
      A(LM2,2) = -ONE - T
      A(LM2,3) = ZERO
      B(LM2) = (DY2*XIB(M,LM1) - U1(M)*DY*(CNE-T)) * Y(LM1)

```

\$

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 01399  
 01400  
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 01412  
 01413

```

C      CALL LEQT1B(A,LM2,NLC,NUC,IA,B,M3,IB,IJC3,XL,IER)
C
C      IF(IER.NE.0) PRINT 24,IER
24  FORMAT('O***ERROR ***MID LEQT1B:  IER= ',I4)
C      DO 130 J=1,LM2
C      PSIB(M,J+1) = B(J)
130  CONTINUE
C
C      MUST "INTERCHANGE I AND J FOR POIS2 USE HERE"
C      (I,J) MAPS INTO (J',I') AND YY(30,60)
C
C      ---- STEP 2 ----
C      DO 135 I=1,LM1
C      DO 135 J=1,MM2
C      LJ = LAR(J+1)-1
C      YY(I,J)=ZERO
C      IF(I.GT.LJ) YY(I,J) = XIB(J+1,I+1)*DX2 * Y(I+1)
135  CONTINUE
C
C      ALONG L.H.SIDE
C      LJ=JCI-1
C      DO 136 I=LJ,LM1
136  YY(I,1) = YY(I,1) - PSI(1,I+1)
C      ALONG R.H.SIDE
C      DO 2137 I=1,LM1
2137 YY(I,MM2) = YY(I,MM2) - PSI(M,I+1)
C
C      DO 137 J=1,MM2
C      ALONG THE BOTTOM
C      YY(1,J) = YY(1,J) - ZERO
C      ALONG THE TOP

```

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01439



[illegible]

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01459  
01460

```

DC 142 I=1,M1M1
LJ = LAR(I)+1
142 XIW(I) = TWO*(PSIB(I,LJ)/DY2 + PSIB(I+1,LJ-1)/DX2) / Y(LJ-1)
XIW(M1) = THREE * PSIB(M1,2)/DY3
C
C *PPINT 99, (XIW(I),I=1,M1)
C PRINT 99, (XIW(I),I=1,M1)
C
C IF( ONE .EQ. 1.0D0) STOP
C RETURN
C END

```

01464  
01464  
01465  
01466





```

* ZSTART, CSTART
COMMON /PLOTZ/ SL,SU,SLI,SKEY(30)
DIMENSIONS ARE SET UP FOR MAXIMUMS OF L=30, M=60, LI=15 & MI=15

DIMENSION PSI(60,30), PSIB(60,30), XI(60,30), V(60,30), U(60,30)
DIMENSION XIW(15), XIB(60,30), VA(60,30), UA(60,30)
DIMENSION UO(30), Y(30), X(60), FX(15), FXRHU(15), DFRQDR(15)
DIMENSION DUMA(15)
INTEGER TS, TIS, PSKP
COMMON IHDR
INTEGER JHDR(6)
DATA JHDR / 'OPSI','O XI','O V','O U','OXIA','OXIB' /
LOGICAL LSWHL, PKNT, ON, OFF, SWHFX
LOGICAL RSTART, SAVE, ZSTART, CSTART

DATA ZERO,ONE,TWO,THREE,FCUR/0.000,1.000,2.000,3.000,4.000/

ON = .TRUE.
OFF = .FALSE.
LSWHL = OFF
PRINT 6
6 FORMAT(' 12/30/76 CORNER AXI-SYM **6**')
IA = IB = (L-2)*(M-2)
THE DIM OF A AND B ARE N AND XL IS TWICE THAT
IA = 1624
IB = 1624
IDIMY = 60
JDIMY = 30
ONE = 1.000

C READ INITIAL DATA

```

01021

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```

C      CALL PUTING6
      MM1 = M-1
      MM2 = M-2
      LM1 = L-1
      MPI = MI+1
C      SET UP INITIAL BOUNDARY CONDITIONS
C      CALL INTAL6
C      IF (TRAMP .EQ. ZERO) TRAMP=ONE
C
C      THE FIRST TIME STEP
C      "IT" IS ACTUAL STEP COUNTER; IT IS ONLY UPDATED WHEN TIME IS.
C      IT=0
C      FOR THIS RUN, THAT IS.
C      TS = 1
C      TTS = PSKP
C      PRNT = GN
C      TIME = ZERO
C      IF ( .NOT. ZSTART) GO TO 10
C      GET BETTER START FROM **10**
C      REWIND 10
C      READ(10) DUM1,DUM2,DUM3,DUM4,IDUM
C      READ(10) DUMA
C      READ(10) PSI,XI,V,U
C      CALL DUICAL
C      CALL EPSCA6( IT )
C      GO TO 887
10 IF ( .NOT. RSTART) GO TO 887
      REWIND 9

```

01230

01232  
01233  
01234  
01235

01236  
01237



```

01238      READ(9)  TIME,DT,DT2,DIA, TS
01239      READ(9)  DFRQDR
01240      READ(9)  PSI,XI,V,U
01241      READ(9)  VA,UA
01242      CALL DUICAL
01243      CALL EPSCA6( IT )
01244
01245      C
01246      C WANT TO MAKE ANY CHANGES?
01247      C
01248      C 887 IF( CSTART) CALL CHANG5( TIME, TS )
01249
01250      C
01251      C TIME_STEP LOOP:
01252      C 898 CONTINUE
01253      C PRINT 1, TIME
01254      C 1 FORMAT('O TIME = ',F12.5)
01255      C IF(TS .LE. NTS) GO TO 700
01256      C 13 FORMAT('O *****TIME_STEP LOOP*****
01257      C 131*** IT = ',I4)
01258      C PRINT 13, IT
01259      C IF(IT .EQ. 0) GO TO 402
01260      C IF(TS .GE. NTS) GO TO 400
01261      C GO TO 402
01262
01263      C 400 CONTINUE
01264      C IHDR = JHDR(1)
01265      C CALL DMTOIO(PSI, M, L, IDIMY, JDIMY)
01266      C IHDR = JHDR(2)
01267      C CALL DMTOIO(XI, M, L, IDIMY, JDIMY)
01268      C IHDR = JHDR(3)
01269      C CALL DMTOIO( V, M, L, IDIMY, JDIMY)
01270      C IHDR = JHDR(4)
01271      C CALL DMTOIO( U, M, L, IDIMY, JDIMY)
01272      C 402 CONTINUE

```

```

C
C
C
PRNT = OFF
PRINT XI CONTOUR PLOT
CONTOUR PLCT FOR XI(1)
PRINT 87
87 FORMAT(11,111111,10
CALL PIXER( XI )
4 FORMAT(111)
PRINT 4
C
666 CONTINUE
IF(15 .LT. 115) GO TO 700
SAVE FOR A LATER RESTART
IF( .NOT. SAVE) GO TO 699
PRINT 2, 10
2 FORMAT(10 DATA SAVED ON UNIT 1,15)
REWIND 10
WRITE(10) TIME,DT,DT2,DTA, 15
WRITE(10) DFRGDR
WRITE(10) PSI,XI,V,U
WRITE(10) VA,UA
C 699 STOP
699 RETURN
700 CONTINUE
IF( .NOT. PRNT) GO TO 701
PRINT 87
CALL PIXER( XI )
PRINT 4
701 CONTINUE
C
C
C
THE ITERATION LOOP

```

```

DO 777 ITER=1,NER
PRINT 21, ITER
21 FORMAT( '///, ' ITER = ',I4, '
CALL WORK6(TIME, TS, ITS )
C
C
C
TEST CONVERGENCE
C
C
C
XMAX = ZERO
DO 147 I=2,M1
J = JCI+1-I
PRINT 3, I,J,XI(I,J),XIW(I)
3 FORMAT('0I,J,XI(I,J),XIW ARE ',2I6,1P2G20.10)
IF(XI(I,J) .EQ. ZERO) GO TO 1313
XAB = DABS((XI(I,J)-XIW(I))/XI(I,J))
XMAX = DMAX1(XMAX,XAB)
147 CONTINUE
PRINT 31, XMAX
31 FORMAT('0 XMAX = ', 1PE12.4)
IF(XMAX .LT. TOL ) GO TO 555
C
C
C
IF XMAX< IS GREATER THAN TOL SET XI=(XIW+XI)/2
DO 146 I=2,M1
J=JCI+1-I
XI(I,J) = (XI(I,J)+XIW(I))/TWO
XI8(I,J) = XI(I,J)
146 CONTINUE
777 CONTINUE
END OF LOOP ON ITER-----
C
C
C/**** NOT KNOWING WHAT TO DO..... */
1313 CONTINUE

```

01274  
01275  
01276

01467

01468  
01469

DEBUG  
DEBUG

01471  
01474  
01475  
01476  
01477

01478  
01479  
1498  
1499  
1500



```

1501 PRNT=ON
1502 PRINT 32
1503 32 FORMAT('OFINISHED THE LOOP AND DONT KNOW WHAT TO DO.')
1504 STOP BUT FIRST PRINT OUT WHAT YOU GET
1505 SAVE = OFF
1506 TS = NTS+1
1507 OUT_OF_LOOP
1508
1509 555 CONTINUE
1510 DO 556 I=2,M1
1511 J=JCI+1-I
1512 XI(I,J) = XIW(I)
1513 XI8(I,J) = XIW(1)
1514 556 CONTINUE
1515 TIME = TIME + DT
1516 IT = IT + 1
1517
1518 DC 35 J=1,L1
1519 DFRCDR(J) = FXRHC(J)
1520 IF (TIME .LT. TFAMP) DFRCDR(J) = FXRHC(J)*TIME/TRAMP
1521 35 CONTINUE
1522 9 FORMAT('O DFRCDR:')
1523 99 FORMAT(2X,1PLOG12.4)
1524 PRINT 9
1525 PRINT 99, (DFRCDR(I),I=1,L1)
1526
1527 DTA = DT
1528 IF (ITER .GT. 3) DT = DT/R1
1529 IF (ITER .LT. 3) DT = DT*R1
1530 300 CONTINUE
1531 PRINT 33, ITER, TS

```

1515  
1516  
1517  
1518  
1519

33 FORMAT('O ITER AND TS ARE ',2I8)  
DT2 = DT / TWO  
PRINT 34, DT  
34 FORMAT('O DT IS ',F12.6)  
TS = TS + 1

C  
C DEFINE THE GRID STREAM FUNCTION AND DU/DY DISTRIBUTION  
C BASED ON THE FINAL RESULTS FROM WORK6  
C

1520  
1521  
1522  
1523  
1524

DO 150 I=1,M  
DO 150 J=1,L  
XI(I,J) = XIB(I,J)  
PSI(I,J) = PSIB(I,J)  
150 CONTINUE

C  
C CALCULATE U AND V FOR THE REGION AHEAD OF THE TRAILING EDGE  
C

DO 155 I=2,M1  
JL = JCI+2-I  
DO 155 J=JL,L41  
U(I,J) = (PSI(I,J+1) - PSI(I,J-1))/TDY/Y(J)  
V(I,J) = -(PSI(I+1,J)-PSI(I-1,J))/TDX /Y(J)  
155 CONTINUE

1527  
1528  
1529

C  
C CALCULATE U AND V FOR THE WAKE REGION  
C

DO 5155 I=MIP1,M1  
DO 5155 J=2,L41  
U(I,J) = (PSI(I,J+1) - PSI(I,J-1))/TDY/Y(J)  
V(I,J) = -(PSI(I+1,J)-PSI(I-1,J))/TDX /Y(J)  
5155 CONTINUE

1530

C

```

C      RECALCULATE U(I,1) = D(PST)/DY FOR MPI1 TO M      1531
C
      DO 160 I=MPI1, M      1532
      160 U(I,1) = TWO*PSI(I,2)/DY2      1533
C
C      CALCULATE U FOR THE DOWNSTREAM BOUNDARY
C
      DO 162 J=2,LM1      1534
      U(M,J) = (PSI(M,J+1)-PSI(M,J-1)) / TDY/Y(J)      1535
      V(M,J) = -(PSI(MM2,J) - FOUR*PSI(MM1,J) + THREE*PSI(M,J))/TDX/Y(J)      1536
      162 CONTINUE      1537
C
C      CALCULATE U(M,L)
C
C      U(M,L) = U1(M)      1538
C      CALCULATE V(M,L)      1539
C
      V(1,L) = -(PSI(MM2,L) - FOUR*PSI(MM1,L) + THREE*PSI(M,L))/TDX/Y(L)      1540
C
C      CALCULATE V ALONG THE UPSTREAM BOUNDARY
C
      DO 166 I=2,MM1      1541
      166 V(I,L) = -(PSI(I+1,L) - PSI(I-1,L)) / TDX /Y(L)      1542
C
      IF(MOD(IT,PSKP) .EQ. 0) CALL DUICAL      1543
      IF(MOD(IT,PSKP) .EQ. 3) CALL EPSCA6( IT )
C
      PRINT = ON
      IF ( TS .GE. NTS ) GO TO 888
      IF ( TS .LE. 2 ) GO TO 888
      PRINT = OFF
      1545
      1546
      1547
      1548

```



1549  
1550  
1551  
1552  
1553  
1554  
1555

TTS = TTS - 1  
IF ( TTS .GT. 0) GO TO 888  
PRNT = CN  
TTS = PSKP  
GO TO 888  
GO TO TIME\_STEP;  
END

C

## SUBROUTINE PUTING6

THIS SUBROUTINE IS RESPONSIBLE FOR READING IN THE DATA FOR  
DRFAX6. THE BODY SHAPE IS DEFINED IN THE LAR ARRAY AND ANY  
QUANTITIES THAT NEED BE INITIALIZED ARE SET IN THIS ROUTINE  
AND INTAL6.

```

IMPLICIT REAL*8 (A-H,O-Z)
REAL*8 K1, KM, KL, KU
COMMON /REALS/ R1,C7,DX,DY,DT,U2,RHC,EPS,FX,FXRHD,X,Y,UO,
* DT2,DTA,TDY,TDX,DY2, DFRDR, TRAMP,TCL, K1, KM, KL, KU,
* EPO, THRUST
COMMON /ARRAYS/ PSI,XI,V,U,VA,UA,PSIB,XIB,XIW, EPA(60), U1(60),
* U10(60), PS10(60)
COMMON /INTEGS/ L,L1,JDEL,M,M1,NTS,NER,PSKP,IDIMY,JDIMY,JCI,IC
COMMON /IRRAYS/ LAR(60)
COMMON /LOGICS/ LSWH1, PRNT, ON, OFF, RSTART, SAVE, SWHFX,
* ZSTART, CSTART
COMMON /PLGTZ/ SL,SU,SLL,SKEY(30)
DIMENSIONS ARE SET UP FOR MAXIMUMS OF L=30, M=60, L1=15 & M1=15

DIMENSION PSI(60,30), PSIB(60,30), XI(60,30), V(60,30), U(60,30)
DIMENSION XIW(15), XIB(60,30), VA(60,30), UA(60,30)
DIMENSION UO(30), Y(30), X(60), FX(15), FXRHU(15), DFRDR(15)
INTEGER PSKP
COMMON IHDR
LOGICAL LSWH1, PRNT, CN, OFF, SWHFX
LOGICAL SWH
LOGICAL RSTART, SAVE, ZSTART, CSTART

DATA ZERO,ONE /0.0D0,1.0D0 /

```

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```

C
NAMELIST /ILIST/ L,L1,M,M1,PSKP,NER,NTS,JDEL,JCI,IO
NAMELIST /RLIST/ CX,DY,DT, RHO,EPS,TCL,C7,TRAMP,KU,K1,KM,KL,EPO
NAMELIST /LLIST/ SWHFX,RSTART,SAVE,ZSTART,CSTART
01042

C
PRINT 87
87 FORMAT('O PUTIN6 01/20/77 MAKE PLOT * 7',//)
01051

C
TWO = 2.000/ONE
THREE = 3.000
FOUR = 4.000
R1 = 1.10
01053
01078
01079

C
14 FORMAT('O**** A RESTART ****')
15 FORMAT('O**** SAVE FOR A PESTAPT AFTER NTS TIME_STEPS. ****')
5 FORMAT('O****NEW START. GET GOOD GUESS FROM UNIT 10****')

C
SWHFX = .TRUE. IMPLIES "NOT" TO COMPUTE A NEW FX CURVE IN SUB
INITIAL
C
ZSTART=ON IMPLIES THIS IS A NEW START AND GET A GOOD GUESS FROM
DATA LN UNIT 10
C
CSTART = ON IMPLIES A CALL TO SUB CHANGE TO MAKE SOME CHANGES
BEFORE ACTUALLY STARTING.
C
TRAMP = 0.100
1000 CONTINUE
C
INPUT PARAMETERS
READ (5, ILIST)
READ (5, RLIST)
READ (5, LLIST)
C
TDX = TWO*DX
TDY = TWO*DY
C
WRITE(6, ILIST)
01080
01081

```



```

C
WRITE(6, RLIST)
WRITE(6, LLIST)

IF( (JCI+2 .LT. JDEL) .AND. (JCI .LE. M1) ) GO TO 20
PRINT 4
4 FORMAT('*****ERROR IN JCI & JDEL')
STOP
20 CONTINUE

C
C DEFINING THE LAR ARRAY
C
DO 21 I=1,M
21 LAR(I)=1

C
DO 22 I=1,M1
J = JCI+1 - I
LAR(I) = J
IF(J.EQ.1) GO TO 23
22 CONTINUE
23 PRINT 6, LAR
6 FORMAT('0THE LAR ARRAY',/(5X,20I3) )

C
IF( RSTART ) PRINT 14
IF( SAVE ) PRINT 15
IF( ZSTART ) PRINT 5
PRINT 2, L, L1, M, M1, DX, DY, DT, KU, RHO, EPS, NER, NTS, JDEL
2 FORMAT('0HERE IS L, L1, M, M1, DX, DY, DT, KU, RHO, EPS, NER, NTS, JDEL',
2*,/(4I6,/1P6G14.5/) )

C
PRINT 111, TOL
111 FORMAT('0 TOL = ', F12.5)
PRINT 1, TRAMP

```

01076  
01077  
01082  
01083  
01084  
01117

```

1 FORMAT('O FOR GRAD PROP, TRAMP =',F8.2)
DO 53 I=1,LI
53 FX(I) = ZERO
C
IF(JDEL .LE. 1) READ 3, (FX(I),I=1,LI)
3 FORMAT(8F10.0)
C
SL = -7.939282907351564D0
SL1 = -5.732802153593751D0
SU = 1.35D0
SKEY(1) = SL
SKEY(2) = SL1
DPY = SL1 - SL
SWH = OFF
C
DO 35 I=3,30
IF(SKEY(I-1)) 30,31,31
30 DPY = DPY / SU
GO TO 32
31 IF(SWH) DPY = DPY * SU
SWH = ON
32 SKEY(I) = SKEY(I-1) + DPY
IF( DABS(SKEY(I)) .LE. 1.0D-5) SKEY(I)=0.0D0
35 CONTINUE
DO 80 I=1,30
SKEY(I) = 7.0D0 * SKEY(I)
80 CONTINUE
C
RETURN
END

```

```

01111
01112
01113
01115
01116
01118

```

## SUBROUTINE DUCAL

THIS SUBROUTINE CALCULATES A D(U1) WHICH IS ADDED TO THE INITIAL  
VALUE COMPUTED IN INTAL6. THE VALUE OF D(U1) IS UPDATED DURING  
THE ITERATION SEQUENCE TO MODIFY THE INITIAL BOUNDARY CONDITIONS.

```

IMPLICIT REAL*8 (A-H,O-Z)
REAL*8 K1, KM, KL, KU
COMMON /REALS/ R1,C7,DX,DY,DT,U2,RHC,EPS,FX,FXRHC,X,Y,UO,
* DT2,DIA,TDY,IDX,DY2, DFRODR, TRAMP,TOL, K1, KM, KL, KU,
* EPO, THRUST
COMMON /ARRAYS/ PSI,XI,V,U,VA,UA,PSIB,XIB,XIW, EPA(60), U1(60),
* U10(60), PSIO(60)
COMMON /INTEGS/ L,L1,JDEL,M,M1,NTS,NER,PSKP,IDIMY,JCI,IO
COMMON /IRRAVS/ LAR(60)
COMMON /LOGICS/ LSWH1, PRNT, ON, OFF, RSTART, SAVE, SWHFX,
* ZSTART, CSTART
DIMENSION PSI(60,30), PSIB(60,30), XI(60,30), V(60,30), U(60,30)
DIMENSION XIW(15), XIB(60,30), VA(60,30), UA(60,30)
DIMENSION UO(30), Y(30), X(60), FX(15), FXRHO(15), DFRODR(15)
INTEGER PSKP
LOGICAL LSWH1, PRNT, ON, OFF, SWHFX
LOGICAL RSTART, SAVE, ZSTART, CSTART

DIMENSION DPSI(60), DDU1(60)

1 FORMAT(' DUCAL 09/01/76')
2 FORMAT('0 I U1(I) DDU1(I) U10(I) PSIO')
3 FORMAT('15,1P4G15.5')
PRINT 1
MM1=M-1
RT=(L-1)*DY

```

01023

01027

01033

C

C



```

RT2 = RT**2
ZC=0.000
T*U=2.000
DDU1(I)=ZC
DPSI(M) = ZC

C
DO 10 I=1,M*1
DPSI(I) = PSI(I+1,L) - PSI(I,L) - PSIO(I+1) + PSIO(I)
10 CONTINUE

C
PRINT 2
DC 30 I=2,M
XT = (I-1)*DX
DDU1(I)=ZC
DO 20 K=1,M*1
XK=(K-1)*DX + DX/140
XTK = XT-XK
R2 = TWO * (RT2 + XTK**2)
BETA = DATAN2( RT, XTK )
DV = DPSI(K) / R2
DDU1(I) = DDU1(I) + DV*DCOS( BETA )
20 CONTINUE
U1(I) = U10(I) + DDU1(I)
PRINT 3, I, U1(I), DDU1(I), U10(I), PSIO(I)
30 CONTINUE
DC 40 I=1,M
40 U(I,L) = U1(I)
RETURN
END

```

## SUBROUTINE INTAL6

```

C
C THIS SUBROUTINE SOLVES FOR THE INITIAL INVISCID FLOWFIELD
C AND SETS THE INITIAL BOUNDARY CONDITIONS FOR THE AXISYM-
C METRIC CASE. THE STREAM FUNCTION FOR THE INVISCID FLOWFIELD
C IS SOLVED FOR USING A SOURCE-SINK DISTRIBUTION ALONG THE
C BODY AXIS. THIS DISTRIBUTION IS FED INTO THE SUBROUTINE
C FROM SUBROUTINE SINK.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*8 KI, KM, KL, KU
      COMMON /REALS/ RI,C7,DX,DY,DT,U2,RHC,EPS,FX,FXRHC,X,Y,UO,
*      DT2,DTA,TDY,TDX,DY2, DFRDR, TRAMP,TCL, KI, KM, KL, KU,
*      EPO, THRUST
      COMMON /ARRAYS/ PSI,XI,V,U,VA,UA,PSIB,XIB,XIW, EPA(60), UI(60),
*      UIO(60), PSIO(60)
      COMMON /INTEGS/ L,L1,JDEL,M,M1,NTS,NER,PSKP,IDIMY,JCI,IC
      COMMON /IRRAYS/ LAR(60)
      COMMON /LOGICS/ LSWH1, PRNT, ON, OFF, RSTART, SAVE, SWHFX,
*      ZSTART, CSTART
      DIMENSIONS ARE SET UP FOR MAXIMUMS OF L=30, M=60, L1=15 & M1=15
C
      DIMENSION PSI(60,30), PSIB(60,30), XI(60,30), V(60,30), U(60,30)
      DIMENSION XIW(15), XIB(60,30), VA(60,30), UA(60,30)
      DIMENSION UIO(30), Y(30), X(60), FX(15), FXRHO(15), DFRDR(15)
      INTEGER PSKP
      COMMON IHDR
      LOGICAL LSWH1, PRNT, ON, OFF, SWHFX
      LOGICAL RSTART, SAVE, ZSTART, CSTART
C
      DATA ZERO,ONE,TWO,THREE,FOUR/0.000,1.000,2.000,3.000,4.000/
C

```

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```

PRINT 1
1 FORMAT(' INTAL6 02/09/77')
JCI = JCI+1
JC2 = JCI + 2
FX0 = ZERO
PI4 = DATAN(ONE)
TDY = TWO*DY
LM1 = L-1
LIM1 = L1-1
LIM2 = L1-2
L13 = L1-3
L14 = L1-4
MIP1 = M1+1

C
DO 52 I=1,M
52 X(I) = (I-1)*DX
DC 54 I=1,L
U0(I) = ZERO
Y(I) = (I-1) * DY
54 CONTINUE

C
DO 60 I=1,M1
DC 60 J=1,M1
PSI(I,J) = ZERO
XI(I,J) = ZERO
V(I,J) = ZERO
U(I,J) = ZERO
60 CONTINUE
DO 60 I=1,M
J1 = LAR(I)
XP = K1 + (I-1)*DX
DO 600 J=J1,L

```

01114  
01119  
01120  
01121  
  
01122  
01126



```

IF(J .GT. J1) GO TO 30
V(I,J)=ZERO
U(I,J)=ZERO
PSI(I,J)=ZERO
GO TO 600
30 CONTINUE
RB = (J-1)*DY
2  FORMAT(1P8G15.5)
3  FORMAT(18,1P4G15.5)
C
C BEGIN SOLVING FOR THE INVISCID FLOWFIELD
C
      THETA = DATAN(RB/XP)
      R = DSQRT(RB**2 + XP**2)
      CT = DCOS(THETA)
      ST2 = ONE - CT**2
      ST = DSQRT(ST2)
      RKL = R/KL
C
      DS = DSQRT(RKL**2 + ONE - TWO*RKL*CT)
C
C CALCULATE STREAM FUNCTION (PSI)
C
      PSI(I,J) = -KM*CT + KM*(RKL - DS) + KU*R**2*ST2/TWO
      VRU = KM/KU/R**2 - KM/KU/KL**2/(RKL*DS) + CT
      VTU = -KM/KU/KL**2/(RKL*ST) * (ONE-(RKL-CT)/DS) - ST
C
      VTOT = KU * DSQRT(VRU**2 + VTU**2)
      ALPHA = DATAN(VTU/VRU)
C
      U(I,J) = VTOT * DCOS(THETA+ALPHA)
      V(I,J) = VTOT * DSIN(THETA+ALPHA)

```

```

600      CONTINUE
      U1(I) = U(I,L)
      U10(I) = U1(I)
      PS10(I) = PSI(I,L)
601      CONTINUE
      DO 602 I=M1P1,M
      XP = K1 + (I-1)*DX
      U(I,1) = KU*(CNE+KM/KU/KL**2*(ONE/XP**2-CNE/XP/(XP-ONE)))
602      CONTINUE
C
      V(M1,2) = V(M1P1,2)
      V(M1-1,3) = V(M1,3)
      DO 603 J=2,L
603      U(M1,J) = U(M1P1,J)
C
      YBOT = Y(JDEL) - Y(JCI)
      U2 = U(1,JDEL)
      PRINT 10, Y(JDEL), YBOT, U2
10      FORMAT('0 Y(JDEL) = ', IPG20.10, ' Y(JDEL)-Y(JCI) = ', IPG20.10,
10*      U2 = ', IPG20.10)
      JDELM1 = JDEL-1
C
C      CALCULATE THE VELOCITY PROFILE AT THE FRONT EDGE OF THE REGION
C
      DO 56 I=JCI,JDELM1
      U0(I) = U2 * ( (Y(I)-Y(JCI))/YBOT )**C7
      U(1,I) = U0(I)
56      CONTINUE
C
C      SWITCH TO COMPUTE FX'S OR LET THEM BE ZERC.
C
      IF(SWHFX) GO TO 59
01133
01134
01145

```

```

C C FIRST: INTEGRAL OF (U0*(U2-U0)*Y)DY FROM Y(JCI) TO Y(JDEL)
C C SU0 = ZERO
C C DG 57 I=JCI,JDELM1
C C 57 SU0 = SU0 + U0(I)*(U2-U0(I))*Y(I)
C C SU0 = SU0 * DY
C C FX0 = TWO * SU0 / Y(L1)**2 / DX
C C SU0 = 0.00
C C FX0 = 259.000
C C PRINT 12, SU0, FX0
C C 12 FORMAT('OINT OF U0*(U2-U0)*Y FROM Y(JCI) TO Y(JDEL) AND FX0 ARE'
C C 12*,/1P2G20.10)
C C DO 58 I=1,L1
C C 58 FX(I) = FX0
C C DC 580 I=L13,L1
C C 580 FX(I) = FX0/TWO * (ONE + DCOS((Y(I)-Y(L14))*PI4/DY))
C C 59 CONTINUE
C C PRINT 4, (FX(I),I=1,L1)
C C 4 FORMAT('HERE IS FX(1:L1) =',/, (1P10E13.4) )
C C PSI IS INTEGRAL (Y(JCI) TO Y(J)) OF Y*U(Y) DY (SANS 2*PI)
C C AND XI IS DU/DY
C C HH = DY/TWO
C C XI(1,JCI) = (-THREE*U(1,JCI)+FOUR*U(1,JCI)-U(1,JC2)) / TDY
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00 64 J=JCI,L
PSI(I,J) = PSI(I,J-1) + HM*(U(I,J)+U(I,J-1)) * Y(J)
IF( J .NE. L) XI(I,J) = (U(I,J+1)-U(I,J-1))/TDY
64 CONTINUE
XI(I,L) = ZERO
C
C IFIEPS .GT. ZERO) GO TO 65
C THE END POINTS OF THE INTEGRAND ARE ASSUMED TO BE ZERO
C PLANAR DSTAR FOR EPS
C THE FOLLOWING WAS REMOVED 2/9/77
C DELSR2 = 0.5D0
C DO 62 I=JCI,JDELM1
C 62 DELSR2 = DELSR2 + ONE-UO(I)/U2
C DELSR2 = DELSR2 * DY
C EPS = 0.018D0 * DELSR2 * U2
C 2/9/77
C DELSR2 = (Y(JDEL)-Y(JCI)) / (CNE/C7+ONE)
C EPS = 0.0168D0 * DELSR2 * U2
C PRINT 11, DELSR2, EPS
11 FORMAT('0 DELSR2 AND EPS ARE ', 1P2G17.8)
65 CONTINUE
DC 27 I=1,M
27 EPA(I) = EPS
C -----
C NOW FILL IN...
K15 = L - JCI
DO 40 I=2,M1
LJ = LAR(I)
DO 41 K=1,K15
J = LJ+K-1
XI(I,J) = XI(I-1,J+1)
41 CONTINUE

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```

J1 = J+1
DO 42 K=J1,L
  XI(I,K) = XI(I,J)
CONTINUE
42 CONTINUE
C
DO 66 I=M1P1,M
DO 66 J=1,L
  XI(I,J) = XI(M1,J)
66 CONTINUE
C  ALONG ED-->
DO 78 I=M1P1,M
  PSI(I,1) = ZERO
78 XI(I,1)=ZERO
C  ALONG THE WALL
DO 79 I=1,M1
  J = LAR(I)
  U(I,J)=ZERO
  V(I,J)=ZERO
  PSI(I,J)=ZERO
  IF(I.EQ.1) GO TO 79
  PSI(I,J+2) = TWO*PSI(I,J+3)/THREE
  PSI(I,J+1) = PSI(I,J+3) / THREE
  U(I,J+2) = TWO* U(I,J+3)/THREE
  U(I,J+1) = U(I,J+3) / THREE
  V(I,J+2) = TWO* V(I,J+3)/THREE
  V(I,J+1) = V(I,J+3) / THREE
79 XI(I,J) = XI(I,JCI)
C
DO 80 J=1,L1
  FXRHO(J) = ZERO
80 DFRDR(J) = ZERO

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```

C      NCW ONLY E      IE.      I=M1, J=2 TO L1-1
C      ASSUMING FXRHO IS ZERO INITIALLY
      DO 82 J=L13,L1
C      82 FXRHO(J) = -FX0 * PI4/TDY * DSIN((Y(J)-Y(L14))*PI4/DY)

C      99 FCRMAT(2X,1PIOG12.4)

C      5 FCRMAT('O      UO')
      PRINT 5
      PRINT 99, (UO(I),I=1,L)
C      7 FCRMAT('O      Y ')
      PRINT 7
      PRINT 99, (Y(I),I=1,L)
C      8 FCRMAT('O      X ')
      PRINT 8
      PRINT 99, (X(I),I=1,M)
C      9 FCRMAT('O      FXRHO')
      PRINT 9
      PRINT 99, (FXRHO(I),I=1,L1)

C      RETURN
C      END

```

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SUBROUTINE EPSCA6 ( ID )

THIS SUBROUTINE CALCULATES THE EDDY VISCOSITY LAW AS DESCRIBED IN THE ACCOMPANYING REPORT. AS AN ADDITIONAL REFERENCE, SEE THE SCHETZ-FAVIN PAPER CONCERNING THE DEVELOPMENT OF THE PROBLEM TITLED " NUMERICAL SOLUTION FOR THE NEAR WAKE OF A BODY WITH PROPELLER".

```

IMPLICIT REAL*8 (A-H,O-Z)
REAL*8 K1, KM, KL, KU, I1, I2
COMMON /REALS/ P1,C7,DX,DY,DT,U2,RHO,EPS,FX,FXRHC,X,Y,UO,
* DT2,DTA,TDY,TDX,DY2, DFRDR, TRAMP,IOL, K1, KM, KL, KU,
* EPO, THRUST
COMMON /ARRAYS/ PSI,XI,V,U,VA,UA,PSIB,XIB,XIW,EPA(60), U1(60),
* U10(60), PS10(60)
INTEGER PSKP
COMMON /INTEGS/ L,L1,JDEL,M,M1,NTS,NER,PSKP,IDIMY,JCI,I0
COMMON /IRRAYS/ LAR(60)
COMMON /LOGICS/ LSWH1, PRNT, CN, OFF, RSTART, SAVE, SWHFX,
* ZSTART, CSTART
DIMENSIONS ARE SET UP FOR MAXIMUMS OF L=30, M=60, L1=15 & M1=15

DIMENSION PSI(60,30), PSIB(60,30), XI(60,30), V(60,30), U(60,30)
DIMENSION XIW(15), XIB(60,30), VA(60,30), UA(60,30)
DIMENSION DU(30), DUY(30), I1(60), I2(60), D11(60), DB(60), B(60)
DIMENSION DU1(60), RI(60)
DIMENSION UO(30), Y(30), X(60), FX(15), FXRHO(15), DFRDR(15)
LOGICAL LSWH1, PRNT, CN, OFF, SWHFX
LOGICAL RSTAPT, SAVE, ZSTART, CSTART

DATA IDSV / -1 /
IF(ID .EQ. 0) IDSV=-1

```

```

C
IF(ID .EQ. IDSV) RETURN
IF(ID .NE. 0) IDSV=ID

Z0 = 0.000
ONE = 1.000
TWO = 2.000

C
EPA(1) = EPS
PRINT 3, EPS
3 FORMAT(' EPS=',1PG20.10)
CUT = 0.00100 * XI(1,JCI)
PRINT 425, CUT
425 FORMAT(' CUT IS ',1PG20.8)
IF(CUT .GT. 0.0500) GO TO 421
GO TO 420
421 IF(CUT .LT. 100.000) GO TO 422
420 CUT = 0.0500
422 CONTINUE
PRINT 426, CUT
426 FORMAT(' CUT USED IS ',1PG20.8)
PRINT 1
C
1 FORMAT('1 EPSCA6 02/09/77 WITH A2 = 2.33 & C2=0.03',
1 FORMAT('1 EPSCA6 04/06/77 WITH A2 = 2.00 & C2=0.035',
* /,8X,'B',11X,'I1',10X,'I2',10X,'DB',10X,
11 'DII',9X,'F1',10X,'F2',10X,'F3',10X,'EPN',9X,'EPA')
C
4 FORMAT(' I=',16,' XI(1,J)',/10(6X,1P10G12.4,/))
C
IF(EPS .GT. 0.000) RETURN
LM2 = L-2
DO 100 I=1,M
LI = LAR(I)
RI(I) = DY*(LI-1)
PUT IN IF D U M M Y

```

```

      LII = LI + 1
      DO 20 J=1,LI
        DU(J) = Z0
        DUY(J) = Z0
      DO 99 J=LII,LM2
        DU(J) = (U(I,J+1)-U(I,J-1)) / TDY
        DUY(J) = Y(J) * DU(J)**2
      CONTINUE
      IF(I .LT. M1) DU(LI) = (4.000*U(I,LII)-U(I,LI+2))/TDY
      IF(I .EQ. M1) DU(LI) = 3.000*PSI(M1,2)/DY**3
      IF(I .LE. M1) DUY(LI) = Y(LI) * DU(LI)**2
C
C
C
C
      5 FORMAT(1P6G16.5)

      DU 10 K=2,LM2
      J = L-K
      JP = J+1
      IF(UBABS(XI(I,J)) .GE. CUT) GO TO 30
      CONTINUE
10  PRINT 13, I
13  FORMAT(' ***ERROR** I =',I5)
C  SOME GUESS
      JP=JDEL
      GO TO 39
C  STOP
30  CONTINUE
      IF(JP .LE. LI) JP=JDEL
      IF(JP .GE. LM2) JP=JDEL
      IF(I .EQ. 1) GO TO 39
      IF(IABS(JP-LJP) .LE. 2) GO TO 39

```



```

C      OK, BUT LET IT JUMP BY 2 ONLY
      IF(JP-LJP) 34, 39, 35
34 JP = LJP-2
   GO TO 30
35 JP = LJP+2
   GO TO 30
39 CONTINUE
C
      LJP = JP
      B(I) = Y(JP)
      I1(I)=Z0
      I2(I)=Z0
      JPI = JP-1
      DO 40 J=L11,JPI
      I1(I) = I1(I) + U(I,J)*Y(J)
      I2(I) = I2(I) + DUY(J)
40
C      I1(I) = I1(I) + U(I,JP)*Y(JP)/TWO
      I2(I) = I2(I) + DUY(JP)/TWO + DUY(L1)/TWO
C
      I1(I) = DY * I1(I) / U1(I) / (B(I)-RI(I))**2
      I2(I) = DY * I2(I) / U1(I) / U1(I)**2
100 CONTINUE
C
C      MM1 = M-1
      DO 200 I=2,MM1
      DI1(I) = (DLOG(I1(I+1))-DLOG(I1(I-1))) / TOX
      DI2(I) = (DLOG( B(I+1))-DLOG( B(I-1))) / TOX
      DUI(I) = (U1(I+1)-U1(I-1)) / TOX
200 CONTINUE
C

```

```

C
D11(1) = (DLOG(I1(2))- DLOG(I1(1))) / DX
DB(1) = (DLOG( B(2))- DLOG( B(1))) / DX
DU1(1) = (U1(2)-U1(1))/DX

DB(M) = (DLOG( B(M)) - DLOG( B(M-1))) / DX
D11(M) = (DLOG(I1(M)) - DLOG(I1(M-1))) / DX
DU1(M) = (U1(M)-U1(M-1))/DX

C2 = 0.03500
A2 = 2.00D0

C
DO 300 I=1,M1
RB = RI(I)/B(I)
BA = (ONE-RB)**2
CON1 = C2**2 * U1(I) / TWC
CON2 = -A2*((ONE-RB**2)/BA**2) / (4.0D0*U1(I)*C2)
F1 = CON1 * I2(I) / I1(I)
F2 = CON2 * EPA(I)**2 / B(I)**2 / I1(I)
F3 = EPA(I) * (DB(I)/I1(I))/TWC/BA - D11(I)/TWC
F4 = -EPA(I) * DU1(I)/TWC/U1(I)

EPA = EPA(I) + DX*(F1+F2+F3+F4)

C
PRINT 2, I,B(I),I1(I),I2(I),DB(I),D11(I),F1,F2,F3,EPN,EPA(I)
IF(EPN .LE. Z0) EPN = EPS
EPA(I+1) = EPN
300 CONTINUE
PRINT 2, M,B(M),I1(M),I2(M),DE(M),D11(M),F1,F2,F3,EPN,EPA(M)
2 FORMAT(14,1P0G12.4)
RETURN
END

```

```

SUBROUTINE CHANG5(TIME, TS)
  IMPLICIT REAL*8 (A-H,O-Z)
  COMMON /REALS/ RI,C7,DX,DY,DT,U2,RHO,EPS,FX,FXRHC,X,Y,UO,
  * DT2,DTA,TDY,TDX,DY2, DFRDDR, TRAMP,TOL, KI, KM, KL, KU
  COMMON /ARKAYS/ PSI,XI,V,U,VA,UA,PSIB,XIB,XIW,EPA(60), UI(60),
  * UIO(60), PSIO(60)
  COMMON /INTEGS/ L,L1,JDEL,M,M1,NTS,NER,PSKP,JOIMY,JCI,IG
  COMMON /IRRAYS/ LAR(60)
  COMMON /LOGICS/ LSWH1, PRNT, CN, OFF, RSTART, SAVE, SWHFX,
  * ZSTART, CSTART
  DIMENSIONS ARE SET UP FOR MAXIMUMS OF L=30, M=60, L1=15 & M1=15

  DIMENSION PSI(60,30), PSIB(60,30), XI(60,30), V(60,30), U(60,30)
  DIMENSION XIW(15), XI6(60,30), VA(60,30), UA(60,30)
  DIMENSION UO(30), Y(30), X(60), FX(15), FXRHO(15), DFRDDR(15)
  INTEGER TS, PSKP
  LOGICAL LSWH1, PRNT, CN, OFF, SWHFX
  LOGICAL RSTART, SAVE, ZSTART, CSTART
  COMMON /PLOIZ/ SL,SU,SLI,SKEY(30)
  PRINT 6
  6 FORMAT(' 5/13/76 DUMMY CHANG5')
  RETURN
END

```

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 01022  
 01023  
 01027  
 01033

C C



```

SUBROUTINE PIXER( U )
IMPLICIT REAL*8 (A-H,O-Z)
COMMON /PLOTZ/ SL,SU,SL1,SKEY(30)
DIMENSION U(60,30)
INTEGER B(15),XK, CC(8)
INTEGER ONCE
INTEGER ONCE
LOGICAL*1 C(32), A(132)
EQUIVALENCE (A(1),B(1)), (C(1),CC(1))
DATA CC /'-ABC','DEFG','HIJK','LMNO','PQRS','TUVW','XYZ+',',++ '//
DATA CC /'-765','4321','OABC','DEFG','HIJK','LMNO','PQRS',',++ '//
DATA ONCE / 1 /

C
IF(ONCE .EQ. 0) GO TO 100
ONCE = 0
PRINT 35
35 FORMAT('O' KEY TO PLOTS')
DO 30 K=1,28
30 PRINT 33, SKEY(K), C(K), SKEY(K+1)
33 FORMAT(5X,1PG12.3,1X,1A1,1PG12.3)
34 FORMAT(1H1)
PRINT 34
100 CONTINUE
C
DO 10 K=1,30
J=31-K
DO 20 I=1,60
XK=1
IF(U(I,J) .LT. SKEY(2)) GO TO 19
XK=28
IF(U(I,J) .GE. SKEY(28)) GO TO 19

```

```

DC 18 L=2,28
XK=29-L
IF(U(I,J) .GE. SKEY(XK)) GO TO 19
18 CONTINUE
C
IF(XK .LE. 0) XK=1
IF(XK .GT. 28) XK=28
19 CALL PLTC(A, I, C(XK), I)
20 CONTINUE
10 PRINT 2, J, (A(M),M=1,60)
PRINT 4
PRINT 3
2 FORMAT(13,1X,60(1A1,1X))
4 FCRMAT(4X,1,17X,1,5(19X,1))
3 FCRMAT(4X,1,17X,10,18X,20,18X,30,18X,40,18X,50,18X,
3*60,/)
RETURN
END

```

```

SUBROUTINE POIS2(N,M,A,B,C, IDIMY,Y,W)
IMPLICIT REAL*8 (A-H,O-Z)
REAL*8   Y(IDIMY,1),A(1),B(1),C(1),W(1)

```

```

THIS SUBROUTINE SOLVES THE LINEAR SYSTEM OF EQUATIONS

```

```

      A(I)*X(I-1,J) + B(I)*X(I,J) + C(I)*X(I+1,J) +
      X(I,J-1) - 2*X(I,J) + X(I,J+1) = Y(I,J) ,

```

```

      FOR I = 1,2, . . . , M , AND
      J = 1,2, . . . , N ,

```

```

WHERE

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      X(I,0) = X(I,N+1) = 0 FOR ALL I, AND
      X(0,J) = X(M+1,J) = 0 FOR ALL J.

```

```

* * * * * RESTRICTIONS * * * * *

```

```

M AND N MUST BE GREATER THAN 1.

```

```

W MUST BE DIMENSIONED AT LEAST 2*N + 4*M + M*(LOG2(N)+1).

```

```

* * * * *

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```

PI (MACHINE DEPENDENT CONSTANT) DEFINED IN POSGN2 AND COSGEN.

```

```

I1 = 2*N + 1
I2 = I1 + M
I3 = I2 + M
I4 = I3 + M
I5 = I4 + M
DO 100 I=1,M

```



```
100 W(I4+I-1) = B(I) - 2.D0  
CALL POSGN2(N,M,A,W(I4),C,IDIMY,Y,W(1),W(11),W(12),W(13),W(15))  
RETURN  
END
```

```

SUBROUTINE PGSGN2(N,M,BA,BB,BC,IDIMQ,Q,TCOS,B,D,W,P)
IMPLICIT REAL*8 (A-H,O-Z)
REAL*8 Q(IDIMQ,1),BA(1),BB(1),BC(1),TCOS(1),B(1),D(1),W(1),P(1)
PI = 3.14159265358979D0
IDGGBR = 0
IDGCCR = 0
IP = 0
DO 100 I=1,M
100 P(I) = 0.D0
NUN = N
JST = 1
JSP = N
IRREG = 1
C IRREG = 1 WHEN NO IRREGULARITIES HAVE OCCURRED, OTHERWISE IT IS 2.
200 L = 2*JST
NODD = 2 - 2*((NUN+1)/2) + NUN
C NODD = 1 WHEN NUN IS ODD, OTHERWISE IT IS 2.
GO TO (220,210),NODD
210 JSP = JSP - L
GO TO 230
220 JSP = JSP - JST
IF (IRREG .NE. 1) JSP = JSP - L
230 CONTINUE
C REGULAR REDUCTION
DO 300 I=1,JST
300 TCOS(I) = 2.D0*DCOS(DFLCAT(2*I-1)*PI/DFLCAT(L))
IF (L .GT. JSP) GO TO 400
DO 380 J=L,JSP,L
IF (JST .NE. 1) GO TO 330
DO 310 I=1,M
8(I) = 2.D0*Q(I,J)
310 Q(I,J) = Q(I,J-1) + Q(I,J+1)

```

```

CALL TRIX(JST,O,M,BA,BB,BC,B,TCOS,D,W)
DO 320 I=1,M
320 Q(I,J) = Q(I,J) + B(I)
GO TO 380
330 DO 340 I=1,M
  T = Q(I,J) - Q(I,J-JSH) - Q(I,J+JSH) + Q(I,J-JST) + Q(I,J+JST)
  B(I) = T + Q(I,J) - Q(I,J-3*JSH) - Q(I,J+3*JSH)
340 Q(I,J) = T
CALL TRIX(JST,O,M,BA,BB,BC,B,TCOS,D,W)
DO 350 I=1,M
350 Q(I,J) = Q(I,J) + B(I)
380 CONTINUE
C
  REDUCTION FOR LAST UNKNOWN
400 GO TO (410,470),NODD
410 GO TO (540,420), IRREG
420 JSP = JSP + L
  J = JSP
429 DO 430 I=1,M
430 B(I) = .500*(Q(I,J-JSH)+Q(I,J-3*JSH)-Q(I,J-JST)) + P(IP*M+ I) - Q(I,J)
432 CALL TRIX(JST,O,M,BA,BB,BC,B,TCOS,D,W)
  IP = IP + 1
DO 431 I=1,M
  P(IP*M+I) = .500*(Q(I,J-JSH)+Q(I,J+JSH)-Q(I,J)) + B(I)
431 B(I) = Q(I,J+JST) - P(IP*M+I)
CALL COSGEN(JSTSAV,IDEGBR,IDEGCR,TCOS)
KK = JSTSAV*(IDEGBR+IDEGCR)
DO 440 I=1,JST
440 TCOS(KK+I) = 2.00*DCOS(DFLOAT(2*I-1))*PI/DFLOAT(L)
CALL TRIX(IDEGBR*JSTSAV,IDEGBR*JSTSAV+JST,M,BA,BB,BC,B,TCOS,D,W)
DO 460 I=1,M
460 Q(I,J) = Q(I,J-JST) + B(I) - P(IP*M+I)
  IDEGCR = IDEGBR

```



```

IDG8R = IDEG8R + 2*JST/JSTSAV
GO TO 540
470 JSP = JSP + L
J = JSP
IP = IP + 1
GO TO (480,500),IRREG
480 IRREG = 2
JSTSAV = JST
IDEG = JST
IDG8R = 2
IF (JST .NE. 1) GO TO 483
DO 482 I=1,M
482 B(I) = Q(I,J)
GO TO 528
483 DO 485 I=1,M
B(I) = Q(I,J) + .500*(Q(I,J-JST)-Q(I,J-JSH)-Q(I,J-3*JSH))
485 P(M*(IP-1)+1) = .500*(Q(I,J-JSH)+Q(I,J+JSH)-Q(I,J))
GO TO 528
500 CALL COSGEN(JSTSAV, IDEG8R, IDEGCR, TCOS)
IDEG = IDEG8R*JSTSAV
IDG8R = IDEG8R + JST/JSTSAV
DO 505 I=1,M
505 B(I) = Q(I,J) + .500*(Q(I,J-JST)-Q(I,J-JSH)-Q(I,J-3*JSH))
528 CALL TRIX(IDEG, IDEGCR*JSTSAV,M,BA,BB,BC,B,TCOS,D,W)
DO 530 I=1,M
P(M*IP+1) = P(M*(IP-1) + 1) - B(I)
530 Q(I,J) = Q(I,J-JST) - P(M*IP+1)
540 NUN = NUN/2
JSH = JST
JST = 2*JST
550 IF (NUN .GE. 2) GO TO 200
J = JSP

```

```

        DO 610 I=1,M
        610 B(I) = Q(I,J)
        GO TO (620,630),IRREG
        620 DO 625 I=1,JST
        625 TCOS(I) = 2.00*DCOS(DFLCAT(2*I-1)*PI/DFLOAT(2*JST))
        IDEG = JST
        GO TO 634
        630 IDEGBR = IDEGCR + JST/JSTSAV
        CALL COSGEN(JSTSAV,IDEGBR,IDEGCR,TCOS)
        IDEG = JSTSAV*IDEGBR
        634 CONTINUE
        CALL TRIX(IDEGBR,IDEGCR*JSTSAV,M,BA,BB,BC,B,TCOS,O,W)
        GO TO (635,637),IRREG
        635 DO 636 I=1,M
        636 Q(I,J) = .500*(Q(I,J-JSH)+Q(I,J+JSH)-Q(I,J)) - B(I)
        GO TO 655
        637 DO 650 I=1,M
        650 Q(I,J) = P(IP*M+1) - B(I)
        IP = IP - 1
        655 CONTINUE
        JST = JST/2
        JSH = JST/2
        NUN = 2*NUN
        IF (NUN .GT. N) GO TO 760
        DO 750 J=JST,N,L
        IF (J .GT. JST) GO TO 670
        DO 660 I=1,M
        660 B(I) = Q(I,J) - Q(I,J+JST)
        GO TO 710
        670 IF (J+JST .LE. N)GO TO 690
        DO 680 I=1,M
        680 B(I) = Q(I,J) - Q(I,J-JST)

```

```

IF (JST .LT. JSTSAV) IRREG = 1
GO TO (710,720), IRREG
690 DO 700 I=1,M
700 B(I) = Q(I,J) - Q(I,J-JST) - Q(I,J+JST)
710 DC 715 I=1,JST
715 TCOS(I) = 2.00*DCOS(DFLCAT(2*I-1)*PI/DFLCAT(L))
IDEG = JST
JDEG = 0
GO TO 721
720 IF (J+L .GT. N) IDEGCR = IDEGCR - JST/JSTSAV
IDEGCR = JST/JSTSAV + IDEGCR
CALL COSGEN(JSTSAV, IDEGCR, IDEGCR, TCOS)
IDEG = IDEGCR*JSTSAV
JDEG = IDEGCR*JSTSAV
721 CONTINUE
CALL TRIX(IDEG, JDEG, M, BA, BB, BC, B, TCOS, D, W)
IF (JST .GT. 1) GO TO 723
DC 722 I=1,M
722 Q(I,J) = -B(I)
GO TO 750
723 IF (J+JST .GT. N) GU TC 730
725 DO 724 I=1,M
724 Q(I,J) = .500*(Q(I,J-JSH)+Q(I,J+JSH)-Q(I,J)) - B(I)
GO TO 750
730 GO TO (725,739), IRREG
739 DC 740 I=1,M
740 Q(I,J) = P(IP*M+I) - B(I)
750 CONTINUE
IP = IP - 1
755 L = L/2
GO TO 655
760 RETURN
END

```



```

SUBROUTINE TRIX(IDEGBR, IDEGCR, M, A, B, C, Y, TCOS, D, W)
IMPLICIT REAL*8 (A-H, O-Z)
REAL*8 A(1), B(1), C(1), Y(1), T COS(1), D(1), W(1)

```

C  
C  
C

```

SUBROUTINE TO SOLVE TRIDIAGONAL SYSTEMS

```

```

MM1 = M - 1
DELT C = DFLOAT(IDEGBR+1)/DFLOAT(IDEGCR+1)
L = DELT C
LINT = 1
DO 300 K=1, IDEGBR
X = TCOS(K)
IF (K .NE. L) GO TO 90
XX = TCOS(IDEGBR + LINT) - X
DO 20 I=1, M
W(I) = Y(I)
20 Y(I) = XX*Y(I)
90 CONTINUE
D(1) = C(1)/(X - B(1))
Y(1) = Y(1)/(X - B(1))
IM1 = 1
DO 100 I=2, M
Z = X - B(I) - A(I) *D(I-1)
D(I) = C(I)/Z
100 Y(I) = (Y(I) + A(I)*Y(I-1))/Z
DO 200 IP=1, MM1
I = M - IP
200 Y(I) = Y(I) + D(I)*Y(I+1)
IF (K .NE. L) GO TO 300
DO 250 I=1, M
250 Y(I) = Y(I) + W(I)
LINT = LINT + 1

```

```
C      L = (LINT*(IDGCR+1.))/(IDGCR+1.)  
      L = DFLOAT(LINT*(IDGCR+1))/DFLOAT(IDGCR+1)  
300 CONTINUE  
      RETURN  
      END
```

```

SUBROUTINE COSGEN(N,M1,M2,TCOS)
IMPLICIT REAL*8 (A-H,O-Z)
REAL*8    TCOS(1)
PI = 3.14159265358979D0
KK = 0
DO 200 K=1,N
  DO 100 I=1,M1
    X = DFLOAT(K) - DFLOAT(I)/DFLOAT(M1+1)
    100 TCOS(KK+I) = 2.D0*DCOS(X*PI/DFLOAT(N))
    200 KK = KK + M1
  IF (M2 .EQ. 0) GO TO 500
  DO 400 K=1,N
    DO 300 I=1,M2
      X = DFLOAT(K) - DFLOAT(I)/DFLOAT(M2+1)
      300 TCOS(KK+I) = 2.D0*DCOS(X*PI/DFLOAT(N))
      400 KK = KK + M2
    500 RETURN
  END

```



```

SUBROUTINE DMT010(A,NR,NC,NRDM,NJDIM)
COMMON IHDR
5 FORMAT(1A4)
PRINT 10 COLUMNS PER ROW WITH G12.4 FORMAT

THIS FORTRAN IV SUBROUTINE WRITES A DOUBLE PRECISION MATRIX IN A
READABLE FORMAT WITH ROW AND COLUMN IDENTIFICATION.

THE ARGUMENTS IN THE CALLING STATEMENT ARE:
A THE MATRIX TO BE WRITTEN (SPECIFIED DOUBLE PRECISION),
NR THE NUMBER OF ROWS OF A TO BE WRITTEN,
NC THE NUMBER OF COLUMNS OF A TO BE WRITTEN,
NRDM THE NUMBER OF ROWS OF A IN THE DIMENSION STATEMENT OF THE
CALLING PROGRAM.

DOUBLE PRECISION A(NRDM,NJDIM)
NCD8 = NC/10
NCRM = MOD(NC,10)
IF (NCD8 .LE. 0) GO TO 2
DO 1 I=1,NCD8
PRINT 5, IHDR
18 = I*10
18M7 = 18-9
WRITE(6,100)(JCOL,JCOL=18M7,18)
100 FORMAT(4H ROW,3X,4HCOL ,13, 9(5X,4HCOL ,13))
DO 1 IROW=1,NR
WRITE(6,101) IROW,(A(IROW,JCOL),JCOL=18M7,18)
101 FORMAT(1H ,13,1P10G12.4)
1 CONTINUE
2 IF (NCRM .LE. 0) GO TO 4
PRINT 5, IHDR
NCMNCR = NC-NCRM+1

```

00000010  
00000020  
00000030  
00000040  
00000050  
00000060  
00000070  
00000080  
00000090  
00000100  
00000110  
00000120

00000210

00000240  
00000250

00000260

00000270  
00000280  
00000290  
00000300  
00000310  
00000320

```
WRITE(6,100) (JCOL,JCOL=NCMNCR,NC)
DO 3 IROW=1,NR
WRITE(6,101) IROW,(A(IROW,JCOL),JCOL=NCMNCR,NC)
3 CONTINUE
4 RETURN
END
```

AD-A074 972

VIRGINIA POLYTECHNIC INST AND STATE UNIV BLACKSBURG --ETC F/6 20/4  
USER'S GUIDE FOR A SYSTEM OF COMPUTER PROGRAMS TO PREDICT FLOWS--ETC(U)  
NOV 78 M C HYMAN, S C HOULIHAN, J A HILL

UNCLASSIFIED

VPI-AERO-096

NL

4 OF 4

ADA  
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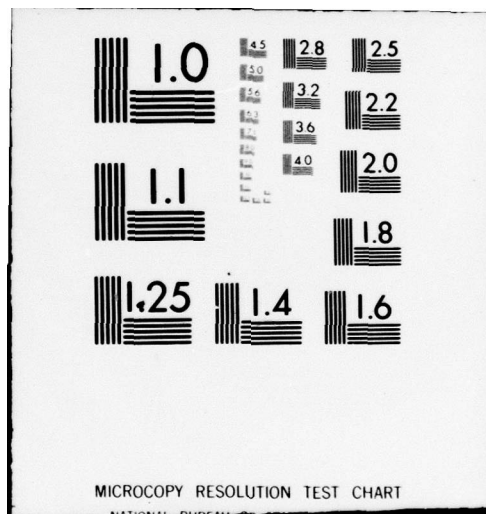
NO  
FILE

END  
DATE  
FILMED

10 -79

DDC







## APPENDIX B

SAMPLE DATA SETS FOR EXECUTION  
OF TEST CASE TWO

TABLE 1.1

## COORD DATA

0	
90	15115
0.0	0.0
0.006667	0.023329
0.013333	0.032712
0.020000	0.039717
0.026667	0.045457
0.033333	0.050366
0.040000	0.054670
0.046667	0.058501
0.053333	0.061947
0.060000	0.065070
0.066667	0.067914
0.073333	0.070513
0.080000	0.072893
0.086667	0.075075
0.093333	0.077075
0.100000	0.078909
0.106667	0.080586
0.113333	0.082117
0.120000	0.083509



0.126667	0.084770
0.133333	0.085905
0.140000	0.086919
0.146667	0.087816
0.153333	0.088601
0.160000	0.089275
0.166667	0.089841
0.173333	0.090302
0.180000	0.090659
0.186666	0.090913
0.193333	0.091065
0.200000	0.091116
0.240747	0.091116
0.281494	0.091116
0.322241	0.091116
0.362988	0.091116
0.403735	0.091116
0.444482	0.091116
0.485230	0.091116
0.525977	0.091116
0.566724	0.091116
0.607471	0.091116
0.614013	0.091115
0.620555	0.091106
0.627097	0.091084
0.633639	0.091042
0.640182	0.090974
0.646724	0.090874
0.653266	0.090738
0.659808	0.090560
0.666350	0.090337
0.672892	0.090063

0.679434	0.089736
0.685977	0.089352
0.692519	0.088909
0.699061	0.088402
0.705603	0.087831
0.712145	0.087192
0.718687	0.086484
0.725230	0.085706
0.731772	0.084856
0.738314	0.083932
0.744856	0.082934
0.751398	0.081862
0.757940	0.080715
0.764482	0.079492
0.771025	0.078193
0.777567	0.076820
0.780000	0.076281
0.793300	0.074000
0.800000	0.070583
0.810000	0.064683
0.820000	0.059265
0.830000	0.054290
0.840000	0.049722
0.850000	0.045528
0.860000	0.041677
0.870000	0.038140
0.880000	0.034893
0.890000	0.031912
0.900000	0.029174
0.910000	0.026661
0.920000	0.024352
0.930000	0.022233

0.940000	0.020287
0.950000	0.018500
0.960000	0.016859
0.970000	0.015353
0.980000	0.013969
0.990000	0.012699
1.000000	0.011533

TABLE 1.2

SEPARA DATA

1
71 90
0

TABLE 1.3

HESS PAPMOATA



NSRDC SUB(L/D = 10.975) WITH ELLIPTIC FCREBODY

101

1001 101  
1

TABLE 2.4

HESSBLI DATA

NSRDC SUB(L/D = 10.975) WITH ELLIPTIC FCREBODY

101

0  
1001 100  
1

0.0	0.0
0.006667	0.023329
0.013333	0.032712
0.020000	0.039717
0.026667	0.045457
0.033333	0.050366
0.040000	0.054670
0.046667	0.058501
0.053333	0.061947
0.060000	0.065070

0.066667	0.067914
0.073333	0.070513
0.080000	0.072893
0.086667	0.075075
0.093333	0.077075
0.100000	0.078909
0.106667	0.080586
0.113333	0.082117
0.120000	0.083509
0.126667	0.084770
0.133333	0.085905
0.140000	0.086919
0.146667	0.087816
0.153333	0.088601
0.160000	0.089275
0.166667	0.089841
0.173333	0.090302
0.180000	0.090659
0.186666	0.090913
0.193333	0.091065
0.200000	0.091116
0.240747	0.091116
0.281494	0.091116
0.322241	0.091116
0.362988	0.091116
0.403735	0.091116
0.444482	0.091116
0.485230	0.091116
0.525977	0.091116
0.566724	0.091116
0.607471	0.091116
0.614013	0.091115

0.620555	0.091106
0.627097	0.091084
0.633639	0.091042
0.640182	0.090974
0.646724	0.090874
0.653266	0.090738
0.659808	0.090560
0.666350	0.090337
0.672892	0.090063
0.679434	0.089736
0.685977	0.089352
0.692519	0.088909
0.699061	0.088402
0.705603	0.087831
0.712145	0.087192
0.718687	0.086484
0.725230	0.085706
0.731772	0.084856
0.738314	0.083932
0.744856	0.082934
0.751398	0.081862
0.757940	0.080715
0.764482	0.079492
0.771025	0.078193
0.777567	0.076820
0.780000	0.075371
0.790000	0.074053
0.800000	0.071857
0.810000	0.069693
0.820000	0.067561
0.830000	0.065459
0.840000	0.063389



0.850000	0.061348
0.860000	0.059336
0.870000	0.057354
0.880000	0.055401
0.890000	0.053476
0.900000	0.051579
0.910000	0.049710
0.920000	0.047867
0.930000	0.046052
0.940000	0.044263
0.950000	0.042500
0.960000	0.040762
0.970000	0.039050
0.980000	0.037362
0.990000	0.035699
1.000000	0.034060
1.009999	0.032445
1.019999	0.030853
1.029998	0.029285
1.039997	0.027739
1.049996	0.026216
1.059996	0.024715
1.069995	0.023235
1.079994	0.021777
1.089993	0.020341
1.099993	0.018925
1.109992	0.017529
1.119991	0.016154
1.129991	0.014799
1.139990	0.013464
1.149989	0.012148
1.159988	0.010851

1.169988	0.009573
1.179987	0.008313
1.189986	0.007072
1.199986	0.005849
1.209985	0.004643
1.219984	0.003455
1.229983	0.002285
1.239983	0.001131
1.249982	-0.000006

TABLE 2.5

WAKE COORDATA

11

1.020000
1.050000
1.100000
1.200000
1.300000
1.400000
1.500000
1.600000
1.700000
1.800000

1.900000

TABLE 2.6

SUMDS DATA

0.0	0.0
0.006667	0.024474
0.013333	0.036000
0.020000	0.045676
0.026667	0.054476
0.033333	0.062757
0.040000	0.070693
0.046667	0.078383
0.053333	0.085888
0.060000	0.093250
0.066667	0.100499
0.073333	0.107654
0.080000	0.114733
0.086667	0.121748
0.093333	0.128708
0.100000	0.135623
0.106667	0.142497
0.113333	0.149337
0.120000	0.156148
0.126667	0.162933
0.133333	0.169695



0.140000	0.176439
0.146667	0.183166
0.153333	0.189878
0.160000	0.196579
0.166667	0.203270
0.173333	0.209952
0.180000	0.216629
0.186666	0.223300
0.193333	0.229968
0.200000	0.236636
0.240747	0.277383
0.281494	0.318129
0.322241	0.358876
0.362988	0.399623
0.403735	0.440370
0.444482	0.481117
0.485230	0.521865
0.525977	0.562612
0.566724	0.603359
0.607471	0.644106
0.614013	0.650648
0.620555	0.657190
0.627097	0.663732
0.633639	0.670274
0.640182	0.676817
0.646724	0.683360
0.653266	0.689904
0.659808	0.696448
0.666350	0.702994
0.672892	0.709541
0.679434	0.716092
0.685977	0.722646

0.692519	0.729203
0.699061	0.735764
0.705603	0.742331
0.712145	0.748904
0.718687	0.755485
0.725230	0.762074
0.731772	0.768671
0.738314	0.775278
0.744856	0.781895
0.751398	0.788525
0.757940	0.795166
0.764482	0.801822
0.771025	0.808492
0.777567	0.815178
0.780000	0.818010
0.790000	0.828096
0.800000	0.838335
0.810000	0.848566
0.820000	0.858791
0.830000	0.869009
0.840000	0.879221
0.850000	0.889427
0.860000	0.899628
0.870000	0.909822
0.880000	0.920011
0.890000	0.930195
0.900000	0.940373
0.910000	0.950546
0.920000	0.960715
0.930000	0.970878
0.940000	0.981037
0.950000	0.991191

0.960000	1.001341
0.970000	1.011486
0.980000	1.021627
0.990000	1.031764
1.000000	1.041897
1.009998	1.052024
1.019999	1.062150
1.029998	1.072271
1.039996	1.082388
1.049995	1.092502
1.059996	1.102613
1.069995	1.112721
1.079993	1.122825
1.089993	1.132926
1.099993	1.143025



TABLE 3.1 UNIT 5 DATA (APLNS DATA)

```
&LLIST  
NTS=70,PSKP=5,NER=40,L=30,LI=12,M=60,M1=15,IO=9,  
&END  
&RLIST  
DT=0.1D-02,RHD=0.7535D-01,EPS=0.0,TOL=0.02D0,TRAMP=.1D0,EPO=0.0D0,  
SCALE1=10.0D0,SCALE2=1.0D0,  
&END  
&LLIST  
SWHFX=F,SAVE=F,  
&END
```

TABLE 3.2 UNIT 8 DATA (APLNS VELDATA)

0.100000	0.006000101
0.0	0.0
0.0	0.0
0.000000	0.000091
0.000000	0.000190
0.000000	0.000297
0.000000	0.000415
0.000000	0.000543
0.000000	0.000683
0.000001	0.000835
0.000001	0.001001
0.000001	0.001181
0.000001	0.001378
0.000001	0.001593
0.000001	0.001827
0.000001	0.002082
0.000002	0.002360
0.000002	0.002663
0.000002	0.002993
0.000002	0.003352

0.000003	0.003744
0.000003	0.004171
0.000003	0.004637
0.000004	0.005144
0.000004	0.005697
0.000005	0.006299
0.000005	0.006955
0.000005	0.007670
0.000006	0.008449
0.000007	0.009297
0.000007	0.010222
0.000008	0.011229
0.000009	0.012326
0.000010	0.013521
0.000011	0.014822
0.000012	0.016240
0.000013	0.017784
0.000014	0.019465
0.000015	0.021295
0.000017	0.023288
0.000018	0.025458
0.000020	0.027819
0.000022	0.030390
0.000024	0.033187
0.000026	0.036230
0.000029	0.039541
0.000031	0.043143
0.000034	0.047059
0.000037	0.051318
0.000041	0.055947
0.000044	0.060977
0.000048	0.066442



TABLE 3.3 UNIT 11 DATA (STREAM DATA)

1	0.903550	0.0	0.977568	0.0	0.977568	0.0	0.0
2	0.909980	0.0	0.975612	0.0	0.975612	0.0	0.0
3	0.916410	0.0	0.973802	0.0	0.973802	0.0	0.0
4	0.922840	0.0	0.972125	0.0	0.972125	0.0	0.0
5	0.929270	0.0	0.970569	0.0	0.970569	0.0	0.0
6	0.935700	0.0	0.969122	0.0	0.969122	0.0	0.0
7	0.942130	0.0	0.967772	0.0	0.967772	0.0	0.0
8	0.948560	0.0	0.966509	0.0	0.966509	0.0	0.0
9	0.954990	0.0	0.965324	0.0	0.965324	0.0	0.0
10	0.961420	0.0	0.964206	0.0	0.964206	0.0	0.0
11	0.967850	0.0	0.963145	0.0	0.963145	0.0	0.0
12	0.974280	0.0	0.962134	0.0	0.962134	0.0	0.0
13	0.980710	0.0	0.961163	0.0	0.961163	0.0	0.0
14	0.987140	0.0	0.960222	0.0	0.960222	0.0	0.0
15	0.993570	0.0	0.959300	0.0	0.959300	0.0	0.0
16	1.000000	0.0	0.958387	0.0	0.958387	0.0	0.0
17	1.006429	0.0	0.957469	0.0	0.957469	0.0	0.0
18	1.012857	0.0	0.956531	0.0	0.956531	0.0	0.0
19	1.019287	0.0	0.955554	0.0	0.955554	0.0	0.0
20	1.025718	0.0	0.954512	0.0	0.954512	0.0	0.0
21	1.032146	0.0	0.953369	0.0	0.953369	0.0	0.0

22	1.038576	0.0	0.952079	0.0	0.952079	0.0	0.0
23	1.045007	0.0	0.950572	0.0	0.950572	0.0	0.0
24	1.051435	0.0	0.948750	0.0	0.948750	0.0	0.0
25	1.057865	0.0	0.946452	0.0	0.946452	0.0	0.0
26	1.064296	0.0	0.943439	0.0	0.943439	0.0	0.0
27	1.070724	0.0	0.939352	0.0	0.939352	0.0	0.0
28	1.077154	0.0	0.933695	0.0	0.933695	0.0	0.0
29	1.083585	0.0	0.925982	0.0	0.925982	0.0	0.0
30	1.090014	0.0	0.916524	0.0	0.916524	0.0	0.0
31	1.096443	0.0	0.908230	0.0	0.908230	0.0	0.0
32	1.102874	0.0	0.906467	0.0	0.906467	0.0	0.0
33	1.109303	0.0	0.912748	0.0	0.912748	0.0	0.0
34	1.115732	0.0	0.922815	0.0	0.922815	0.0	0.0
35	1.122163	0.0	0.932782	0.0	0.932782	0.0	0.0
36	1.128592	0.0	0.941273	0.0	0.941273	0.0	0.0
37	1.135021	0.0	0.948203	0.0	0.948203	0.0	0.0
38	1.141452	0.0	0.953836	0.0	0.953836	0.0	0.0
39	1.147882	0.0	0.958454	0.0	0.958454	0.0	0.0
40	1.154310	0.0	0.962290	0.0	0.962290	0.0	0.0
41	1.160741	0.0	0.965524	0.0	0.965524	0.0	0.0
42	1.167171	0.0	0.968282	0.0	0.968282	0.0	0.0
43	1.173599	0.0	0.970663	0.0	0.970663	0.0	0.0
44	1.180030	0.0	0.972740	0.0	0.972740	0.0	0.0
45	1.186460	0.0	0.974568	0.0	0.974568	0.0	0.0
46	1.192888	0.0	0.976189	0.0	0.976189	0.0	0.0
47	1.199319	0.0	0.977638	0.0	0.977638	0.0	0.0
48	1.205749	0.0	0.978940	0.0	0.978940	0.0	0.0
49	1.212177	0.0	0.980117	0.0	0.980117	0.0	0.0
50	1.218608	0.0	0.981186	0.0	0.981186	0.0	0.0
51	1.225038	0.0	0.982162	0.0	0.982162	0.0	0.0
52	1.231466	0.0	0.983056	0.0	0.983056	0.0	0.0
53	1.237897	0.0	0.983878	0.0	0.983878	0.0	0.0

54	1.244327	0.0	0.984637	0.0	0.984637	0.0	0.0
55	1.250755	0.0	0.985339	0.0	0.985339	0.0	0.0
56	1.257186	0.0	0.985990	0.0	0.985990	0.0	0.0
57	1.263616	0.0	0.986596	0.0	0.986596	0.0	0.0
58	1.270044	0.0	0.987161	0.0	0.987161	0.0	0.0
59	1.276475	0.0	0.987690	0.0	0.987690	0.0	0.0
60	1.282905	0.0	0.988184	0.0	0.988184	0.0	0.0
61	0.903550	0.001670	0.977565	0.000264	0.977566	0.015468	0.0
62	0.909980	0.001670	0.975610	0.000245	0.975610	0.014372	0.0
63	0.916410	0.001670	0.973800	0.000227	0.973800	0.013349	0.0
64	0.922840	0.001670	0.972123	0.000211	0.972123	0.012409	0.0
65	0.929270	0.001670	0.970567	0.000196	0.970567	0.011550	0.0
66	0.935700	0.001670	0.969120	0.000182	0.969120	0.010762	0.0
67	0.942130	0.001670	0.967770	0.000170	0.967770	0.010047	0.0
68	0.948560	0.001670	0.966508	0.000159	0.966508	0.009437	0.0
69	0.954990	0.001670	0.965323	0.000150	0.965323	0.008897	0.0
70	0.961420	0.001670	0.964204	0.000142	0.964204	0.008412	0.0
71	0.967850	0.001670	0.963145	0.000135	0.963145	0.008032	0.0
72	0.974280	0.001670	0.962134	0.000129	0.962134	0.007705	0.0
73	0.980710	0.001670	0.961162	0.000125	0.961162	0.007444	0.0
74	0.987140	0.001670	0.960221	0.000121	0.960221	0.007241	0.0
75	0.993570	0.001670	0.959300	0.000120	0.959300	0.007148	0.0
76	1.000000	0.001670	0.958387	0.000119	0.958387	0.007121	0.0
77	1.006429	0.001670	0.957469	0.000121	0.957469	0.007219	0.0
78	1.012857	0.001670	0.956532	0.000124	0.956532	0.007454	0.0
79	1.019287	0.001670	0.955555	0.000131	0.955555	0.007869	0.0
80	1.025718	0.001670	0.954513	0.000142	0.954513	0.008506	0.0
81	1.032146	0.001670	0.953372	0.000157	0.953372	0.009443	0.0
82	1.038576	0.001670	0.952082	0.000180	0.952082	0.010834	0.0
83	1.045007	0.001670	0.950578	0.000214	0.950578	0.012877	0.0
84	1.051435	0.001670	0.948758	0.000264	0.948758	0.015916	0.0
85	1.057865	0.001670	0.946464	0.000339	0.946464	0.020492	0.0

TABLE 3.3 has been appended from 180 to 85 lines.